

# **UT GeoFluids 2020 Research Plan**

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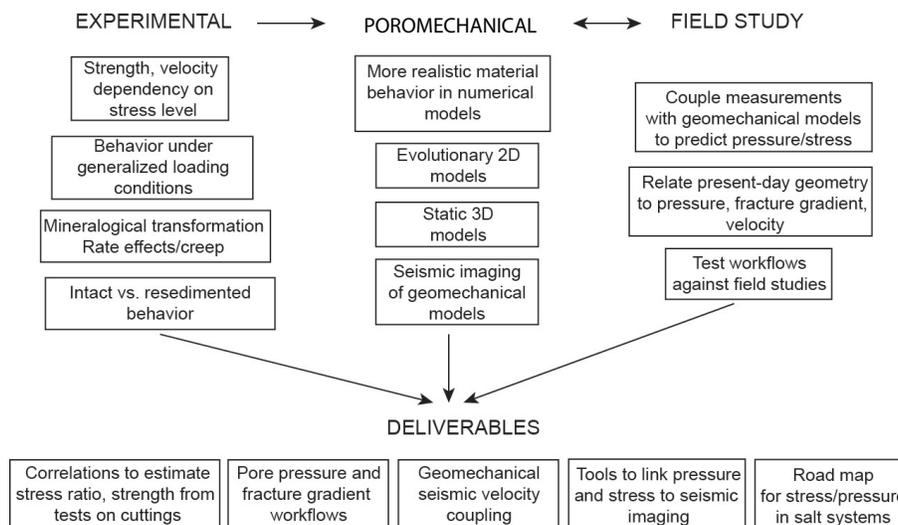
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## **1 Executive summary**

The UT GeoFluids 2020 Industrial Associates Program will study the state and evolution of pressure, stress, deformation and fluid flow through experiments, theoretical analysis, and field study. The Institute for Geophysics (UTIG) at the Jackson School of Geosciences will partner with the Dept. of Civil and Environmental Engineering at Tufts University. The cost will be \$50,000 and will increment at 2%/yr. The first payment will be due in May 2019. Our research will focus on the following.

- Develop and deliver pore pressure and fracture gradient workflows.
- Link poromechanics with pressure prediction and express in whole earth stress models.
- Include stress dependency and material anisotropy in poromechanical models.
- Develop synthetic seismic models of poromechanical models.
- Study material behavior under complex stress paths representative of geologic conditions.
- Examine the role of creep in mudstones at geological stresses.
- Compare material behavior of resedimented mudstone with intact material.
- Perform field studies and build geomechanical models to predict pressure during unloading in unconventional basins

We aim to develop a unified approach that incorporates stress dependency, creep, mineralogical transformation, and loading path to illuminate the state and evolution of pressure and stress in basins. We already see evidence that this unified approach can improve well design and provide insight into a range of geological processes. These approaches will result in two and three-dimensional whole earth models that improve well design, real-time drilling, borehole stability, and reservoir simulation.



*Figure 1. Interdependence of experimental, poromechanical, and field study variables.*

## 2 UT GeoFluids Plan

We produce innovative concepts that couple geology, mudrock rheology, and fluid flow to predict pressure and stress in the subsurface. Applications include pore pressure and stress prediction, the design of stable and safe drilling programs, and the study of hydrocarbon migration and entrapment. We study the state and evolution of pressure, stress, deformation and fluid migration through experiments, models, and field study:

1. **Experimental:** We analyze fabric, acoustic, electrical, hydraulic, and material properties of mudrocks: 0.1-100 MPa.
2. **Poromechanical Modeling:** We couple sedimentation, porous fluid flow, geologic and tectonic loading to predict pore pressure and the full stress tensor.
3. **Field Study:** We analyze pore pressure, stress, and deformation in conventional and unconventional basins.

### 2.1 Experimental

#### 2.1.1 Overview

We will characterize and quantify stress level dependence, anisotropy, and time dependence. Our goal is to better interpret field observations, calibrate numerical simulations, and provide a database to develop new models of mudrock behavior. During the past decade, we focused primarily on the stress dependent aspects of behavior during uniaxial and triaxial loading conditions and under constant loading rates. This has included various subthemes (temperature, salinity, type of mudrock, mineral transformation, etc.) but the central focus has been stress level. The next phase of the research will expand to compare intact to resedimentated behavior, the effects of loading direction, and the effects of creep.

#### 2.1.2 Validate/calibrate resedimented behavior against intact behavior

**Challenge:** We have spent a decade developing material models for mudstones of different lithologies based on the resedimentation process. We will reconcile these systematic measurements against intact core samples. Does resedimented material behave similarly to intact material; if not, is there a systematic mapping that we can use to transfer insights from resedimented to intact mudrock behavior?

**Research Plan:** We will work with industry sponsors to acquire intact core samples of unlithified mudrocks and associated material. We will compare the material behavior of intact vs. resedimented material. We will perform laboratory experiments (uniaxial compression, undrained triaxial shear, velocity, etc.) on the intact core and the companion resedimented specimens and we will perform our typical suit of physical property tests.

We will systematically compare the resedimented behavior with the intact behavior (Figure 2), and with our resedimentation database. We will produce an approach, if possible, to integrate the intact and resedimentation database to develop generalized intact behavior. The results will allow our experimental work to more effectively be applied to subsurface problems.

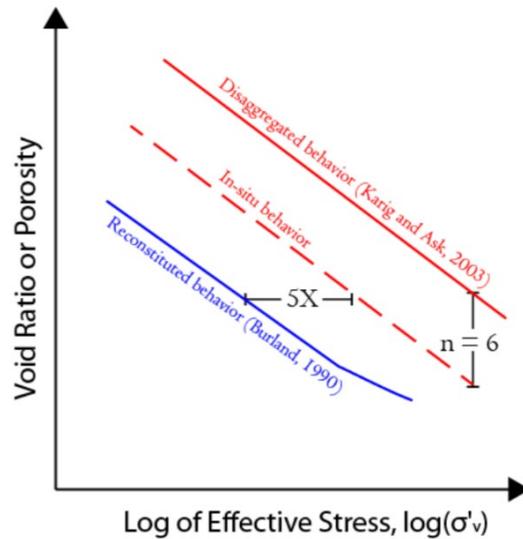


Figure 2. The relationship between material properties of intact core and resedimented material is unclear. Karig and Ask (2003) suggest that at given effective stress, an intact mudrock is more compacted than a synthetic specimen of identical composition. In contrast, Burland (1990) suggests that the in-situ mudrock is less compacted than the synthetic material. We will compare measurements (e.g. stress-strain behavior under shear, undrained strength, friction angle, velocities, etc.) of resedimented behavior against intact behavior.

### 2.1.3 Poromechanical behavior under generalized load conditions.

**Challenge:** Mudrocks in many basins undergo complex stress histories. For example, sediment deposited outside a thrust belt under uniaxial strain ( $K_0$ ) conditions is ultimately exposed to a large lateral stress as it is consumed into the thrust belt (Figure 3a). Alternately, sediment adjacent to a salt diapir may undergo extreme lateral stresses (Figure 3b).

Most mathematical models for geological applications use relatively simple descriptions of material behavior. For example, we use the Modified Cam Clay model or Rockfield's SR3 model, which are based on yield surfaces that are symmetric about the horizontal (mean stress) axis and remain as such regardless of the loading path. However, yield surfaces rotate and align with the loading axis (Figure 4b). A critical question is what is the shape of the yield surface and how does it evolve during loading? This form of the yield surface at any given loading increment controls the amount of pore pressure generated.

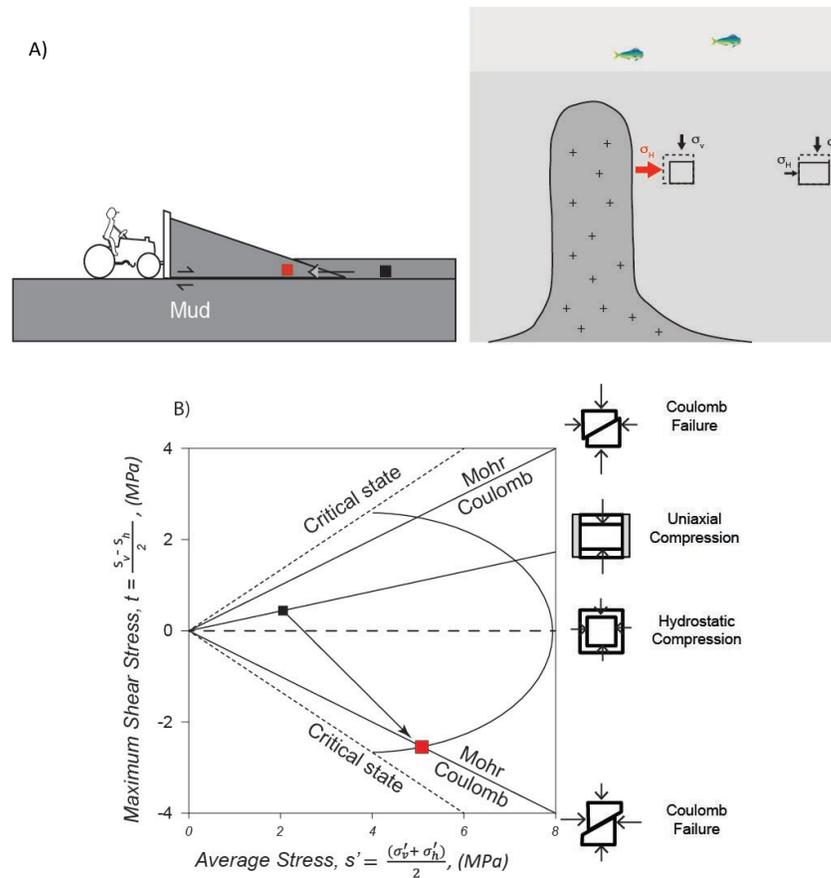


Figure 3: Basin sediments commonly undergo complex stress histories. In either a thrust belt (a) or a salt system (b), the stress path may shift from initial deposition along the  $K_0$  trend (black square), where the horizontal stress is less than the vertical, to compressional failure (red square), where the lateral stress exceeds the vertical stress.

### Research Plan:

Initially, we will investigate the shape of the yield surface at different stress levels, up to 100MPa, using our conventional triaxial apparatus (cylindrical specimens). We will also study yield surface rotation under compressional loading (horizontal major principal stress). We will next develop a 3-axis testing device capable of large normal strains in order to decouple the intermediate principal stress from the direction of loading. Such devices have been used for very low stress testing (<1 MPa) in geotechnical engineering and for rock testing at high stress, but with limited strain capability (<5%). This will be a major advancement in technology that will allow investigation of compression and shear behavior as the material transitions from a  $K_0$  state of stress to the more general stress conditions found around salt features or within thrust belts.

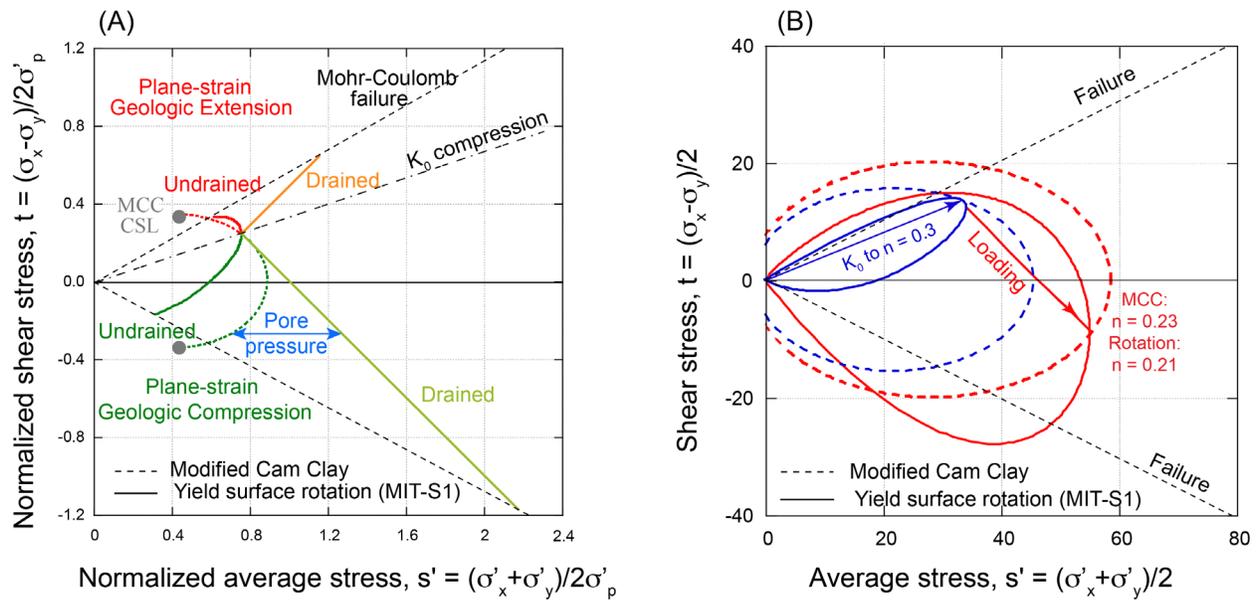


Figure 4: A) Example loading paths following uniaxial compression for plane-strain conditions, predicted by Modified Cam Clay (dashed lines) and MIT-S1 (yield-surface rotation; solid lines). B) Compressional loading after uniaxial compression: iso-volumetric surface at the end of each loading predicted by MCC (symmetric with respect to x-axis) and MIT-S1 (asymmetric and rotating; Pestana et al, 2002).

#### 2.1.4 Wave Velocity Characterization:

**Challenge:** Wave velocities are a function of the elastic modulus and density of the material. Most sedimentary materials are considered to be cross-anisotropic (one symmetry axis) resulting in five independent elastic parameters. Anisotropy in the sedimentary section must be corrected for us to properly image the subsurface and to estimate subsurface properties (Nihei et al., 2011). We are developing complex forward poromechanical models and we wish to understand how they would be imaged in the subsurface. To do so, we need to determine the five elastic constants and how they vary with stress state and stress level.

**Research Plan:** We will measure the compressional ( $P$ ) and shear ( $S$ ) wave velocity anisotropy as a function of stress up to 100 MPa. The measured velocities will be used to compute the elements of the stiffness matrix, which are then used to determine the velocity in any direction (e.g. Figure 5). Velocity measurements require specific technologies designed for each stress level range. We have recently developed technology up to 10 MPa which allows measurement of a)  $P$  and  $S$  waves in the axial dimension (surface mounted piezoceramic crystals in the end caps); b)  $P$  and  $S$  waves across the specimen diameter (crystals mounted directly on the specimen under the membrane) and c) one inclined  $P$  wave (side of specimen to end cap). Our next technology increment will be developing a similar capability in the triaxial cell having a capacity of 100 MPa.

Elastic anisotropy (Young's modulus, Shear modulus, and Poisson's ratio) varies with stress level during  $K_0$  consolidation and is also dependent on the general stress state (non- $K_0$

conditions and proximity to the failure envelop). We will explore these velocities during different compression paths ( $K_0$ , isostatic, etc.) as well as during undrained shearing.

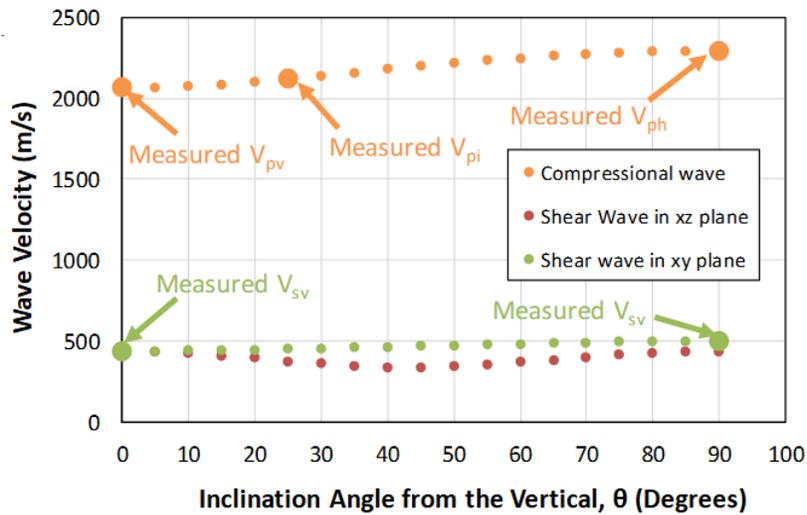


Figure 5. Compressional and shear wave velocity as a function of angle based on measurements of five independent velocities on a specimen uniaxially consolidated to 5.8 MPa

### 2.1.5 Visco-plastic behavior:

**Challenge:** Deeper, hotter, and older mudrocks are often more compacted than mudrocks at the same effective stress in the shallow section. It is also common for laboratory-measured of resedimented specimens to have a higher porosity than intact samples at the same stress level. We have ruled out the effects of pore fluid salinity, elevated temperature, and illitization. While unloading (reduction in effective stress) may account for some cases, it is unlikely to explain the ubiquitous behavior observed. We will now focus on creep as a cause for these effects.

All particulate materials experience time-dependent deformations (volumetric and shear) under constant effective stress conditions. Mesri (1974) found that the rate of creep was uniquely related to the slope of the compression curve and coined this "the 4<sup>th</sup> law of soil mechanics". Relaxation is the reduction in the stress state at fixed deformation, which is a closely related time-dependent behavior to creep. Creep is often referred to as secondary compression, drained creep, and undrained creep. In the lab, creep follows primary consolidation. However, since rates of consolidation scale with the square of the drainage distance, field consolidation times are millions of times slower than the laboratory scale. It is unclear if creep occurs after primary consolidation or if it coexists with primary consolidation. This can lead to very different deformation and potentially different pore pressure predictions.

Creep under uniaxial loading has been studied extensively in the laboratory using both an incremental oedometer and constant strain rate compression testing. Creep deformations follow a linear log-time relationship. Figure 6 illustrates the potential effect of creep on compression behavior for different time scales up to 10 million years. While the numbers are approximate and based on lab measurements, Figure 6 clearly illustrates that creep may be an important factor in assessing field porosities. For example, at a 5% creep rate, a 10 m.y. old rock under a load of

100 MPa (14,500 psi) would compact 0.08 additional porosity units relative to a material recently deposited (solid red vs. dashed black lines, Figure 6).

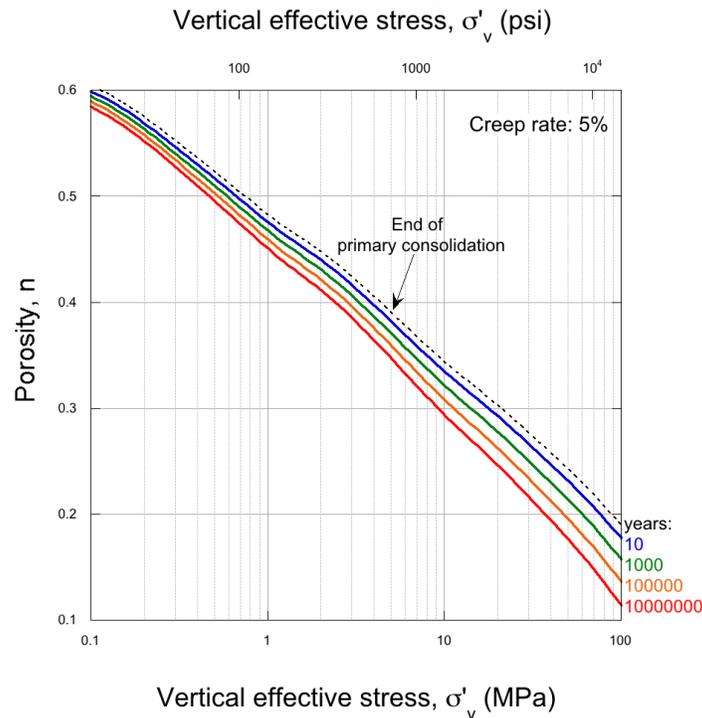


Figure 6. Effect of creep on compression behavior for different time scales up to 10 million years. End of primary consolidation (dashed black line) based on laboratory tests. Creep rate 5%.

**Research Plan:** We will perform uniaxial compression tests under varying strain rates as well as constant axial effective stress conditions (incremental loading) to characterize the creep rate and variation in the lateral stress ratio as a function of time and stress level. We will use rigid wall and triaxial devices to vary the drainage height and provide lateral stress measurements. The output of this study will be an understanding of how compression curves vary with strain rate. It will form the basis of a rate dependent mudrock model. We will also investigate how relaxation may alter the state of stress during uniaxial compression with a particular focus on how lateral stress ( $K_0$ ) values change as a function of relaxation.

## 2.2 Poromechanical

### 2.2.1 Overview

The motivation of the poromechanical program is to study stress, pressure and deformation in complex geologic settings using field geometries and realistic material description. Our goals are to: a) estimate pore pressure and the full stress tensor under complex geologic loading; b) identify hazardous zones for drilling; c) advance our fundamental understanding of the interaction between pressure, stress, and deformation in basins; and d) develop a technical approach to address geological systems where large strains, pore fluids, and sedimentation interact. We will develop material models that describe the behavior observed in our experimental program (e.g., stress dependency, yield-surface rotation) and we will implement

these models into numerical simulations. In addition, we will build 3-dimensional models of complex geologic systems and develop workflows to relate poromechanical results to velocity fields.

### 2.2.2 Incorporate more realistic material behavior within numerical models

**Challenge:** It is necessary to include this stress and path dependence in our poromechanical models to more accurately describe earth behavior. Simple critical state soil models assume a constant frictional strength, are insensitive to the rate of loading, and do not depend on the direction of loading. Our recent experimental work has demonstrated a systematic dependence of frictional strength, undrained strength, and lateral stress ratio on stress level. For example, the predicted stresses are fundamentally different when the material properties are strength dependent (Figure 7, right) relative to when they are not (Figure 7, left). We also observe a dependence of the yield surface and iso-volumetric surfaces on stress level and loading direction.

**Research plan:** We will develop an enhanced critical state model that will incorporate 1) the asymmetry (rotation) and evolution of the yield surface under complex geologic loading and high stress levels, 2) stress-level dependency of frictional angle, undrained strength, and stress ratio, 3) strain rate sensitivity. We will couple this new formulation with evolutionary numerical models.

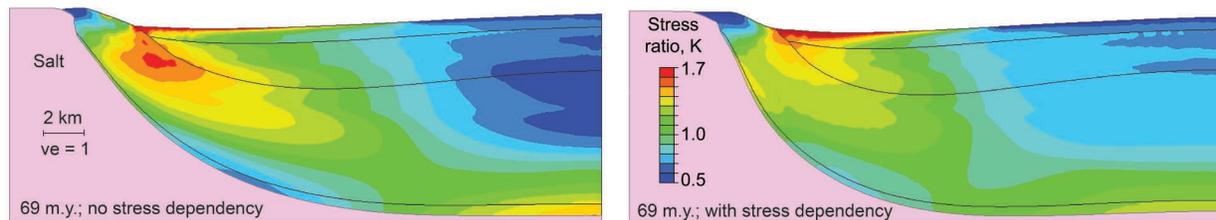


Figure 7. Preliminary study of the effect of stress dependency on a salt system. Decrease in the frictional strength with confining stress leads to a more uniform stress state near salt.

### 2.2.3 3-D models of complex salt systems

**Challenge:** We will extend model results to three dimensions to explore under what conditions it is appropriate to extrapolate 2D results to 3D systems (Figure 8). A plane strain model can over-predict stresses relative to an axisymmetric model (Figure 9). Thus, while plane-strain and axisymmetric models may predict qualitatively similar behavior, the plane-strain approach predicts much higher values, because no deformation is allowed in the out-of-plane direction. At the same time, the axisymmetric model may under-predict stresses, because it cannot account for constraints in the circumferential (hoop) direction. Hence, neither approach fully represents the three-dimensional geometry of salt systems.

**Research plan:** We will develop 3-dimensional models and study the effect of complex geometries to stress and pressure near salt. We will compare our results with plane-strain or axisymmetric models and provide criteria and guidelines for investing in a 3-dimensional study. We will work with industry to obtain real salt geometries, predict pressure and stress and compare with field data.

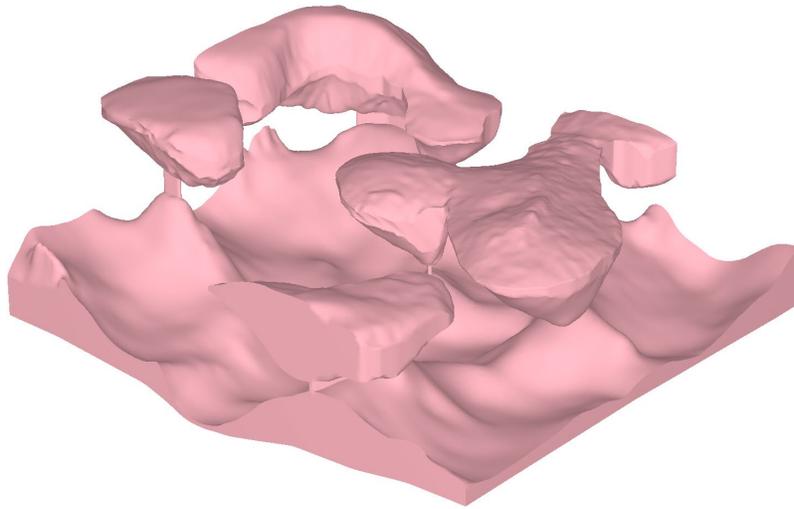


Figure 8. Salt system offshore West Africa, (courtesy of Repsol) illustrating the complexity of the 3D salt geometry.

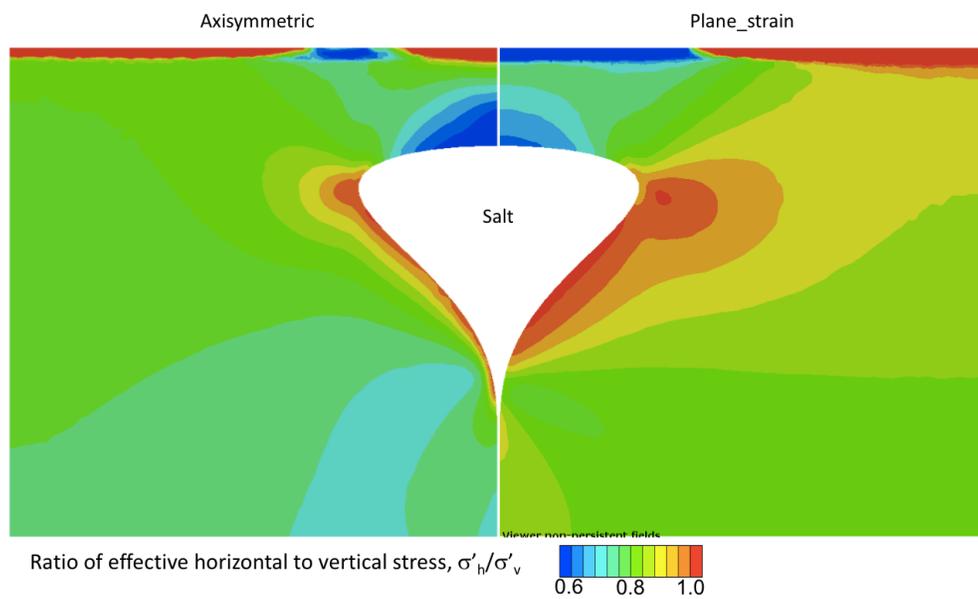


Figure 9. Axisymmetric vs. plane strain salt model. Both models predict qualitatively similar behavior; however, the plane-strain model predicts much higher stress values.

#### 2.2.4 Synthetic Seismic of Poromechanical Models

**Challenge:** Our poromechanical models provide the full effective and total stress tensors, porosity and pore pressure predictions. We will develop seismic models of our poromechanical models to understand how pressure and stress are recorded in seismic data. The results may improve seismic imaging and ultimately allow inversion of pressure and stress from seismic data.

**Research plan:** We will couple poromechanical modeling, laboratory measurements, and seismic anisotropic-model building to develop the next generation of seismic analysis tools.

We will generate synthetic seismic data and images based on computed stresses (Figure 10A) and material properties from our poromechanical models. We will build anisotropic velocity models (Figure 10B) using published, and lab-measured, empirical and theoretical relations. We will use anisotropic models to create synthetic seismic shot gathers (Figure 10C) using the derived stiffnesses. A necessary intermediate step is the derivation of a rock-physics model to translate stresses to seismic velocities or elastic stiffnesses. Because the stress model is transversely isotropic (TI), the more convenient quantities to work in are the elastic stiffnesses. Initially, we will calculate directional-dependent velocities from the stiffnesses. Each cell in the TI model requires five independent stiffnesses. In this example (Figure 10), the rock-physics used relates the effective stresses to the velocities. To derive this model, first, the well-log velocities are considered relative to the maximum principal stress along the deviated wellbore. The well deviation angle and the maximum principal stress angle dictate which anisotropic, angle-dependent velocity is measured along the wellbore. Once this is done, the range of fast and slow P-wave velocities expected throughout the model are known. The empirically derived rock-physics model relates the effective-stress components to elastic stiffnesses. It then transforms the poromechanical stresses to TI elastic stiffnesses at all locations (Figure 10B). The maximum principal stress direction determines the orientation of the fast and slow velocities.

For application to field data, we will use our effective stiffnesses for imaging using TTI reverse time migration. Resulting image gathers will be flat, which can be used for subsequent AVO analysis. Note that we estimate NMO velocity and  $\eta$  from anisotropic velocity analysis. These will be used together with velocity data (e.g., Figure 10) for quantitative interpretation (AVO analysis) and depth imaging of field gathers. Furthermore, we will develop inversion methods for directly estimating parameters other than NMO velocity and  $\eta$ , directly from field seismic data. We envision coupling modeling, lab measurements, and seismic anisotropic-model building to develop the next generation of seismic analysis tools.

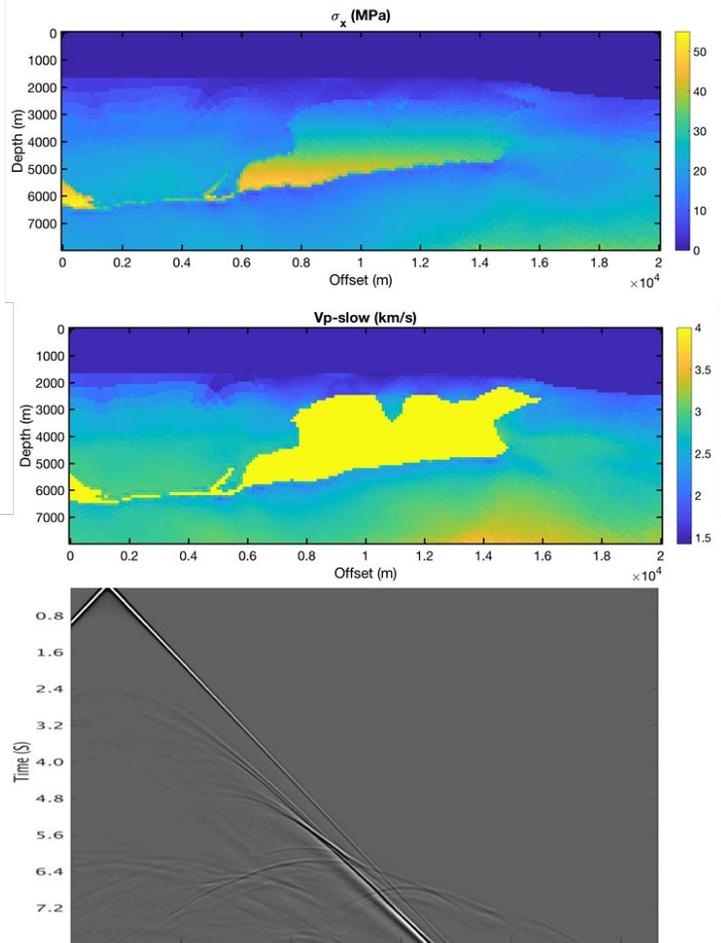


Figure 10. A) Stress field (in-plane horizontal stress) from geomechanical model; B) slow quasi-P wave velocity from (A); C) Synthetic seismic shot gather computed by finite differences using (B). Shot gathers will be processed/studied for AVO and anisotropic velocity analysis.

### 2.2.5 Geomechanical response to unloading

**Challenge:** In unconventional basins, secondary pressure mechanisms (e.g. hydrocarbon generation) and/or erosion often unload the system (the present effective stress is less than the maximum effective stress in the past). Traditional effective stress approaches to pressure prediction do not hold in these environments (e.g. Couzens-Schultz et al. 2013). The challenge is to develop a quantitative physics-based understanding of how unloading impacts the stress field and pore pressure prediction.

**Research plan:** We will develop geomechanical models to describe pore pressure and stress response to unloading. We will specifically include the effect of the full stress tensor on pore-pressure and porosity changes during unloading. In addition, we will consider the effect of a hydrocarbon source term and the presence of multiple phases in the pore space. We will begin with the development of simple, one dimensional models and will evolve to considering two dimensional models. We will integrate our geomechanical understanding with field observations to develop a process understanding of the evolution of pressure in unconventional basins.

## 2.3 Field studies

### 2.3.1 Overview

We will continue to perform field studies in the Gulf of Mexico and elsewhere. In particular, we will expand our studies to include analysis of unconventional basins. Analysis of field data tests the effectiveness, approaches, and insights that we develop through our experimental and modeling work. It also trains the next generation of quantitative geoscientists.

### 2.3.2 Validation of poromechanical predictions with field measurements

**Challenge:** We have developed evolutionary poromechanical models that couple sedimentation with porous fluid flow and salt flow. We have also developed transient evolutionary models of fold-and-thrust belts. These models provide specific predictions regarding the state of stress, pressure, and deformation in complex systems. We will deliberate target data sets to test these predictions with field measurements.

**Research plan:** We will work with our industry members to obtain stress and pressure measurements in salt systems and in thrust belts. We will mine MDT and leak-off measurements from public databases. We will augment our estimate of stress state and pressure from borehole image logs. We will compare these field studies with poromechanical model predictions. This research will be instrumental in creating a road map that links porosity, overpressure, stress ratio, and mudrock strength with geometric features of salt systems.

### 2.3.3 Validation of pressure prediction workflows

**Challenge:** We have developed pressure prediction workflows that couple poromechanical modeling with seismic velocities. We have applied the workflow in a 2D transect in the Gulf of Mexico with limited well data. We will validate and test these approaches with analysis of field measurements in areas we apply these workflows.

**Research plan:** We will work with industry sponsors and service companies to release seismic data and pressure and stress data over specific fields with geometries that reflect our poromechanical model simulations. We will take advantage of newly released 3D seismic data available across the Gulf of Mexico. We will build static poromechanical models from present-day geometry and couple them with velocity data. We will validate our workflow by comparing pressure and stress predictions with available well measurements. We will use 2D and 3D poromechanical models and predict pressure across transects and across a three-dimensional area of interest. We will evaluate the relative benefits of investing into three-dimensional workflows.

### 2.3.4 Pressure prediction in unconventional basins

**Challenge:** Pore pressures are impacted by erosional unloading and hydrocarbon maturation in many unconventional basins. As a result, effective-stress–pore-pressure prediction techniques used in conventional basins may not be successful (Couzens et al., 2013). The challenge is to develop a process understanding of how pore pressure evolves in unconventional basins and then apply this understanding to predict pressure in new locations.

**Research plan:** We will work with industry sponsors and service companies to obtain log and pressure data over several unconventional basins. We are considering the Powder River Basin of Wyoming and the Permian Basin of West Texas and two companies are eager to provide data to support this effort. We will first build a pore pressure database from kicks, connection gases, DFITs and production data (Ewens et al., 2012; Jones et al., 2014; Kozlowski et al., 2018). We will then study the petrophysical response of velocity (shear and density) and resistivity logs. We will integrate geologic information to understand the history of deposition and erosion, the organic content, and the timing of maturation. We will then link our observations of pressure to predictions from geomechanical models and develop a process understanding of the evolution of pressure in unconventional basins.

We wish to address the following. Can we develop a systematic approach for predicting pressure in unconventional basins and how different is this approach from workflows used in conventional basins? Does overpressure generation followed by subsequent exhumation, therefore a reduction in confining stress and cooling, enhance or reduce overpressure? What can logs tell us about the state of stress and pressure in a basin, given a known amount of erosion?

## 2.4 Deliverables

- 1) Cuttings Protocol: We will deliver a protocol for on-site (on-rig) cleaning and testing of cuttings. We will provide correlations between liquid limits/clay fraction and stress ratio, friction angle, and undrained strength. This tool will allow quick estimation of least principal stress and strength during drilling.
- 2) Salt Pressure-Stress Atlas: We will build an atlas that relates salt geometry to pressure and stress predictions. This atlas will qualitative insights to estimate stress, pressure, and hazardous zones near salt.
- 3) Road Map for Intact vs. Resedimented Behavior: We will build a database that compares intact with resedimented behavior.
- 4) Online Experimental Database: We will provide an online database containing our experimental measurements for use by the sponsors for internal evaluations.
- 5) Poromechanical Model Results: We will communicate and distribute poromechanical model results in standard industry software format and in excel spreadsheets.
- 6) Online Software: We build online software to communicate the concepts we are developing.
- 7) Workflows: We will continue to develop our workflow to couple seismic models with poromechanical models to predict pressure and stress.
- 8) Synthetic Seismic Images: We will deliver tools and workflows to generate synthetic seismic datasets from our poromechanical models.

## 3 Logistics

The first payment will in May of 2019. The initial annual fee will be \$50,000 and this will increment at 2%/yr. There will be no penalty for withdrawing from the consortium. Members who choose to join after the first year will be required to pay the previous year's consortium cost.

### 3.1.1 Current industrial associates

Industrial Associates which are currently members of the GeoFluids consortium under the [Industrial Associate Agreement](#) will need to sign an Amendment.

### 3.1.2 Prospective industrial associates

Industrial Associates interested in joining the GeoFluids consortium will need to sign a new Agreement that reflects the original Agreement and the Amendment.

## 4 References

- Burland JB (1990). On the compressibility and shear strength of natural clays. *Geotechnique* 40:329-378, doi:10.1680/geot.1990.40.3.329.
- Couzens-Schultz, B. A., et al. (2013). Pore Pressure Prediction in Unconventional Resources. International Petroleum Technology Conference. Beijing, China, International Petroleum Technology Conference: 11.
- Ewens, S. D., Idorenyin, E. H., apos, Donnell, P., Brunner, F., and Santo, M., 2012, Executing Minifrac Tests and Interpreting After-Closure Data for Determining Reservoir Characteristics in Unconventional Reservoirs, SPE Canadian Unconventional Resources Conference: Calgary, Alberta, Canada, Society of Petroleum Engineers, p. 14.
- Jones, R. S., Jr., Pownall, B., and Franke, J., 2014, Estimating Reservoir Pressure From Early Flowback Data, Unconventional Resources Technology Conference: Denver, Colorado, USA, Unconventional Resources Technology Conference, p. 16.
- Karig DE, Ask MVS (2003). Geological perspectives on consolidation of clay-rich marine sediments. *Journal of Geophysical Research* 108:2197, doi:2110.1029/2001JB000652.
- Kozlowski, K., Da Silva, M., Brown, D., Taylor, J., Willems, H., Watson, T., Burch, D., Hutton, T., Christensen, C., and Manohar, M., 2018, The Importance of Overburden and Pore Pressure on Horizontal Stress Magnitude Determination; an Example From the Delaware Basin, SPE/AAPG/SEG Unconventional Resources Technology Conference: Houston, Texas, USA, Unconventional Resources Technology Conference, p. 15.
- Mesri G, Rokhsar A (1974). Theory of consolidation for clays. *Journal of the Geotechnical Engineering Division, Proceedings of the American Society of Civil Engineers* 100:889-904.
- Nihei K, Nakagawa, S., Reverdy, F., Myer, L., Duranti, L. (2011). Phased array compaction cell for measurement of the transversely isotropic elastic properties of compacting sediments. *Geophysics* 76:WA113-WA123.
- Pestana JM, Whittle AJ, Gens A (2002). Evaluation of a constitutive model for clays and sands: Part II Clay behavior. *International Journal for Numerical and Analytical Methods in Geomechanics* 26:1123-1146.