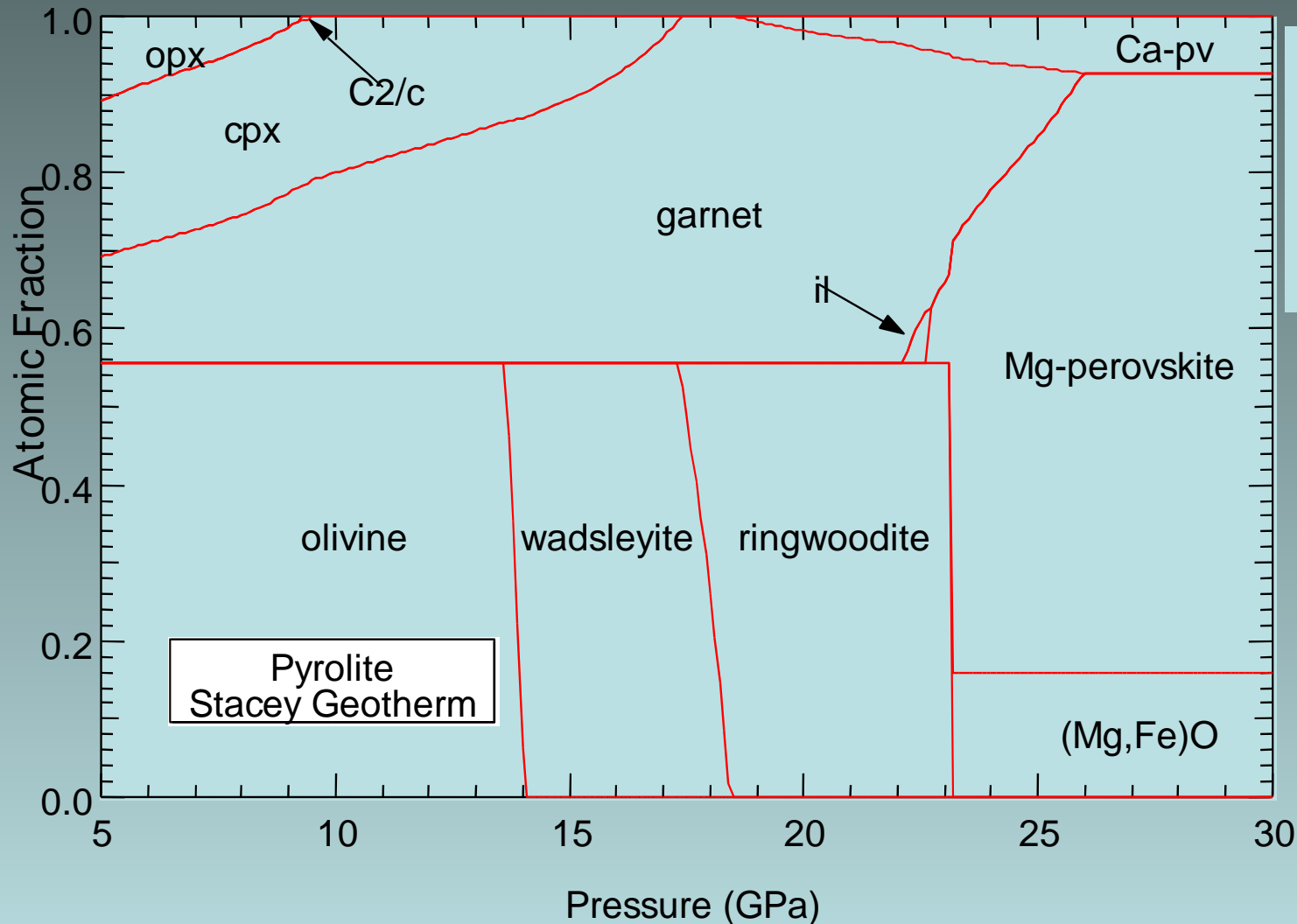


# Interpreting Geophysical Data for Mantle Dynamics

Wendy Panero

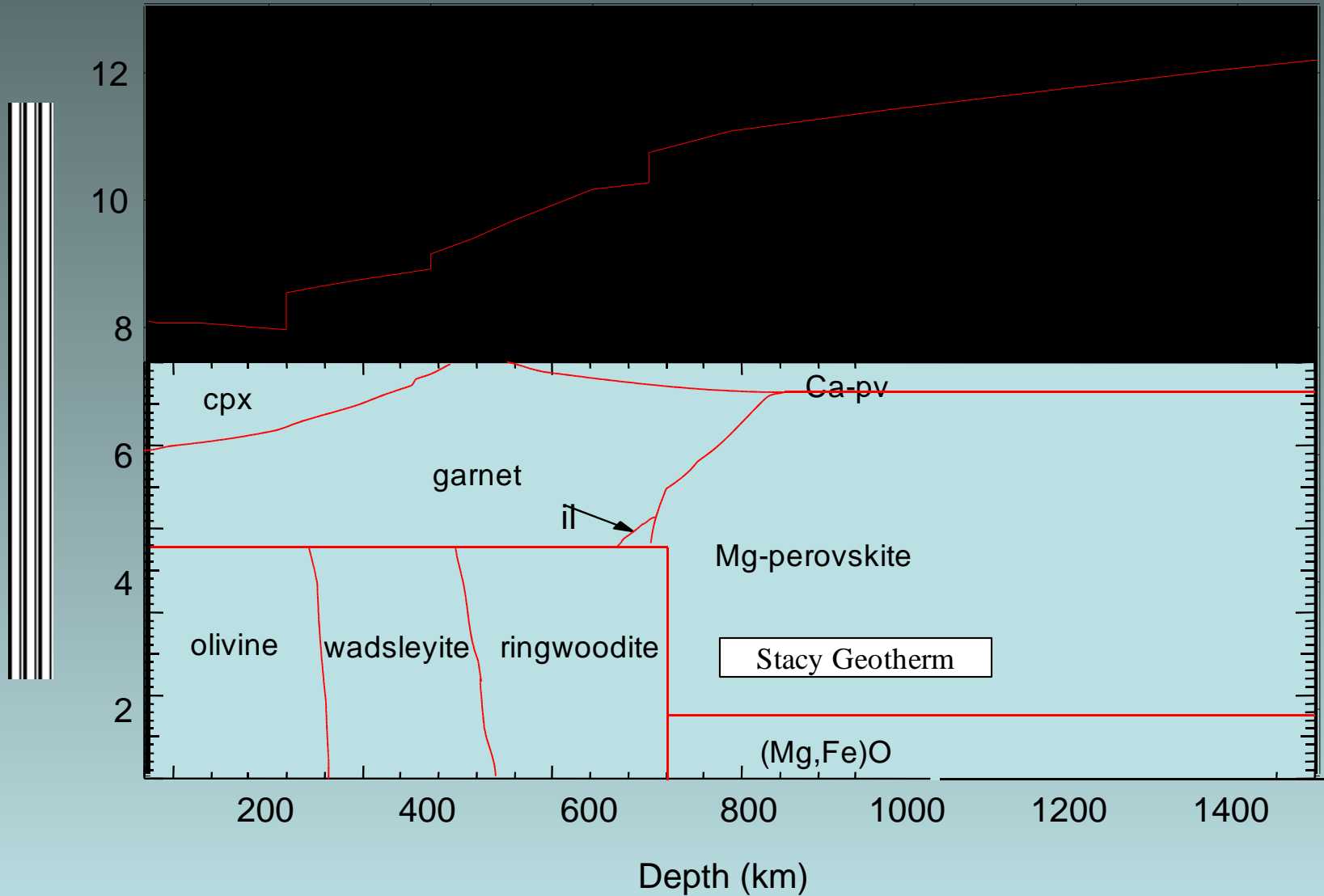
University of Michigan

# Chemical Constraints on Density Distribution

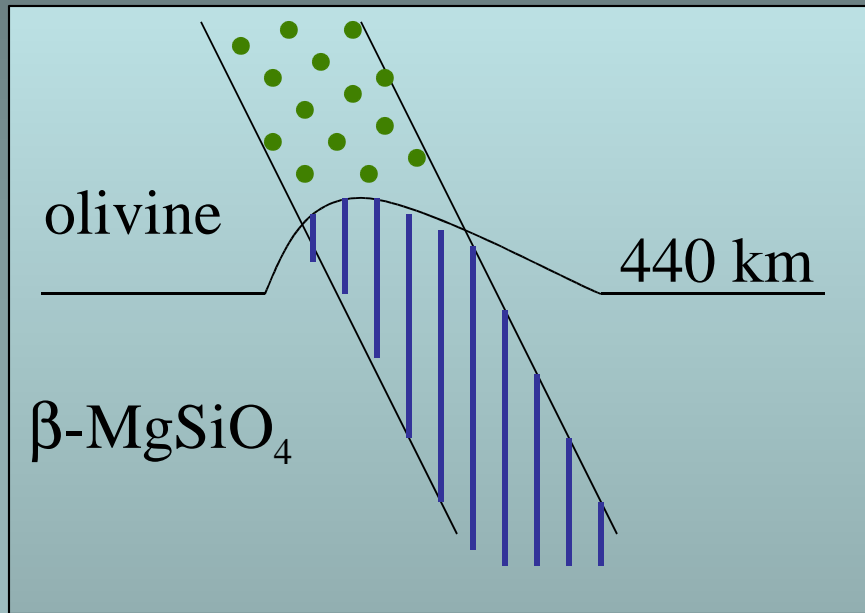


|                                |          |
|--------------------------------|----------|
| SiO <sub>2</sub>               | 45.4 wt% |
| MgO                            | 37.1 wt% |
| FeO                            | 8.3 wt%  |
| Al <sub>2</sub> O <sub>3</sub> | 4.3 wt%  |
| CaO                            | 3.3 wt%  |

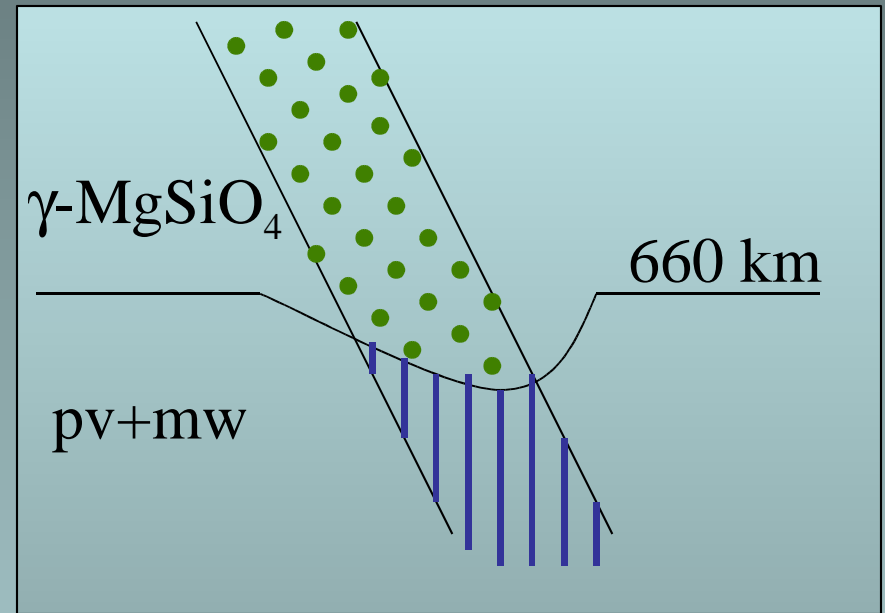
# Chemical Constraints on Density Distribution



# Cold Slabs, Clapeyron Slopes and Whole Mantle Convection



exothermic reaction

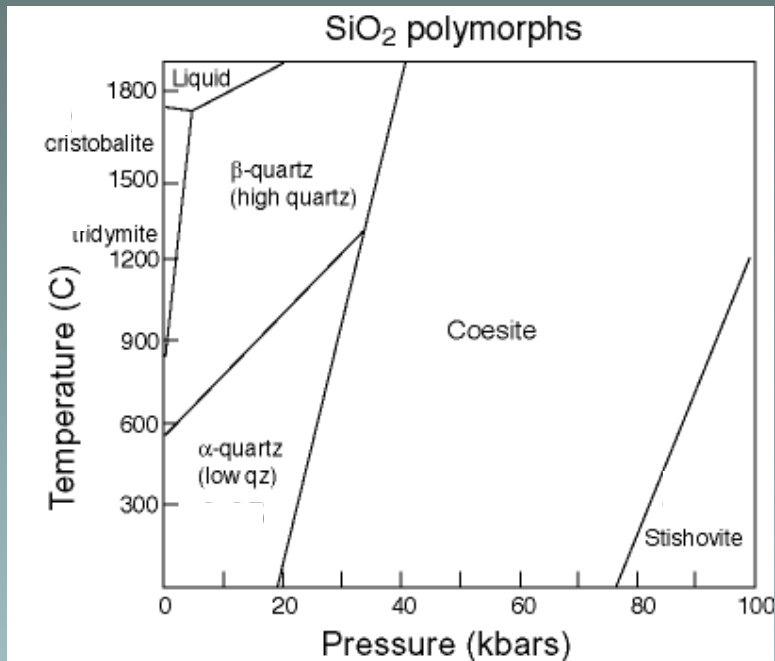


endothermic reaction

$$F_b = -g \sum v_i (Dr_i) (\partial z / \partial P) (\partial P / \partial T)_i DT$$

# Clapeyron Slope

$$G = \mathcal{P} - \mathcal{T}$$



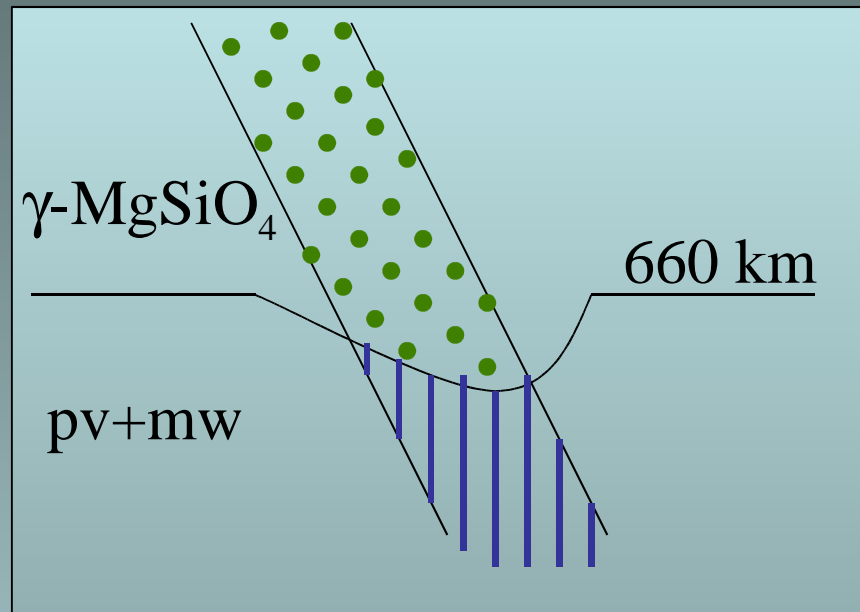
Equilibrium:

$$\Delta G_1 = \Delta G_2$$

$$V_1 d\mathcal{P} - S_1 d\mathcal{T} = V_2 d\mathcal{P} - S_2 d\mathcal{T}$$

$$\frac{d\mathcal{P}}{d\mathcal{T}} = \frac{DV_{rxn}}{DS_{rxn}}$$

# Cold Slabs, Clapeyron Slopes and Whole Mantle Convection



endothermic reaction

$$F_b = -g \sum v_i \left( \frac{\partial r_i}{\partial z} \right) \left( \frac{\partial z}{\partial P} \right) \left( \frac{\partial P}{\partial T} \right)_i \Delta T$$

Clapeyron slope must be greater than... ask a geodynamicist

# Determination of Clapeyron Slopes

$$\frac{dP}{dT} = \frac{DV_{rxn}}{DS_{rxn}}$$

Phase Equilibria

ex-situ

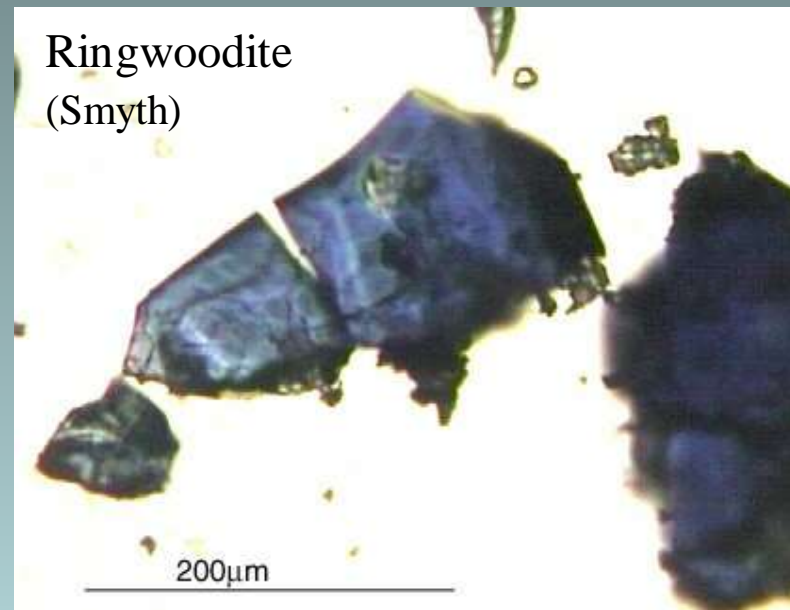
in-situ

Thermodynamic

# Determination of Clapeyron Slopes

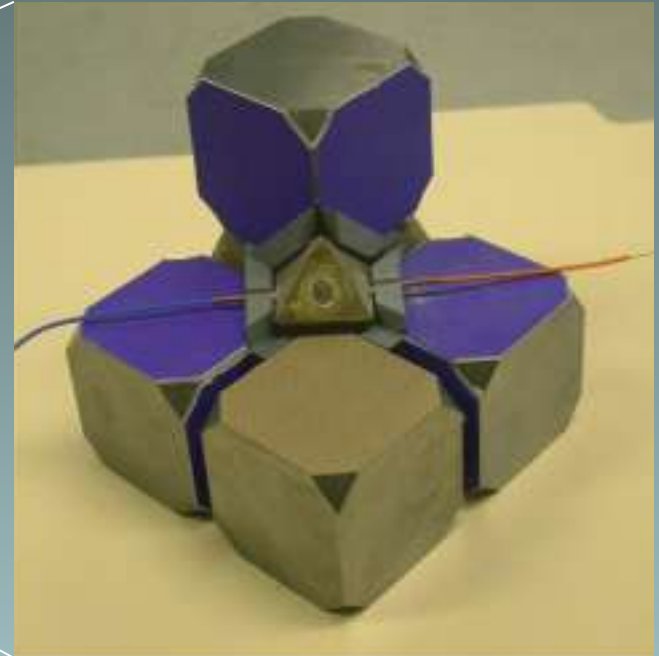
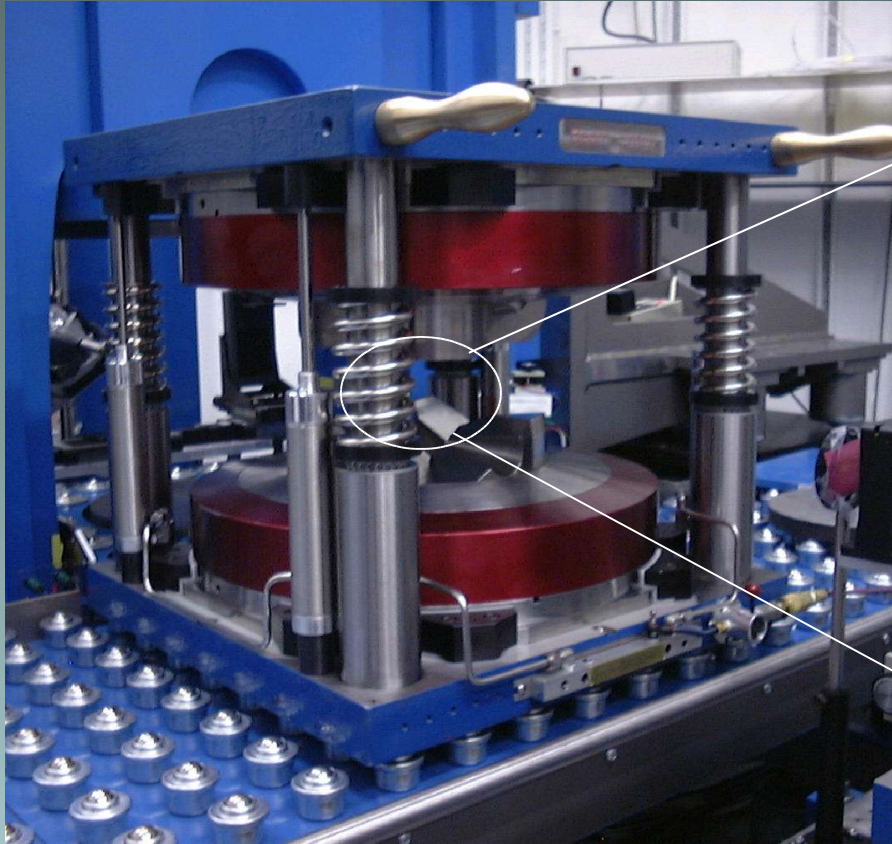
$$\frac{dP}{dT} = \frac{DV_{rxn}}{DS_{rxn}}$$

Phase Equilibria  
**ex-situ**  
in-situ  
Thermodynamic





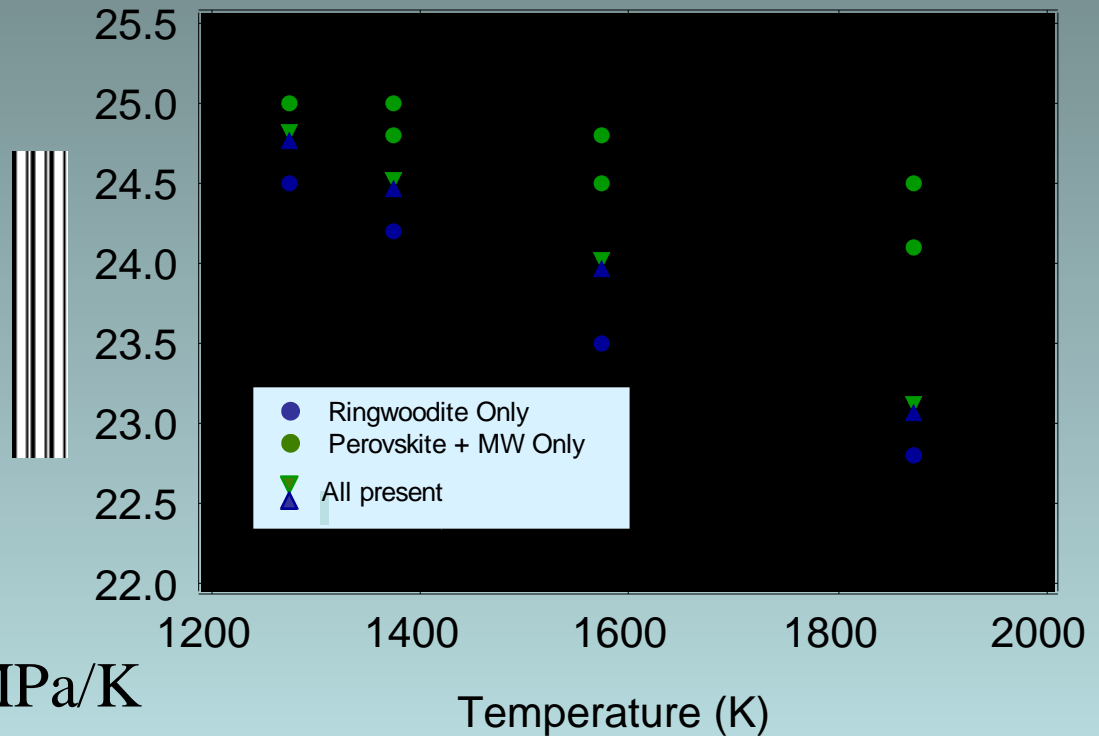
# Multi-Anvil Press



# Determination of Clapeyron Slopes

$$\frac{dP}{dT} = \frac{DV_{rxn}}{DS_{rxn}}$$

Phase Equilibria  
**ex-situ**  
in-situ  
Thermodynamic

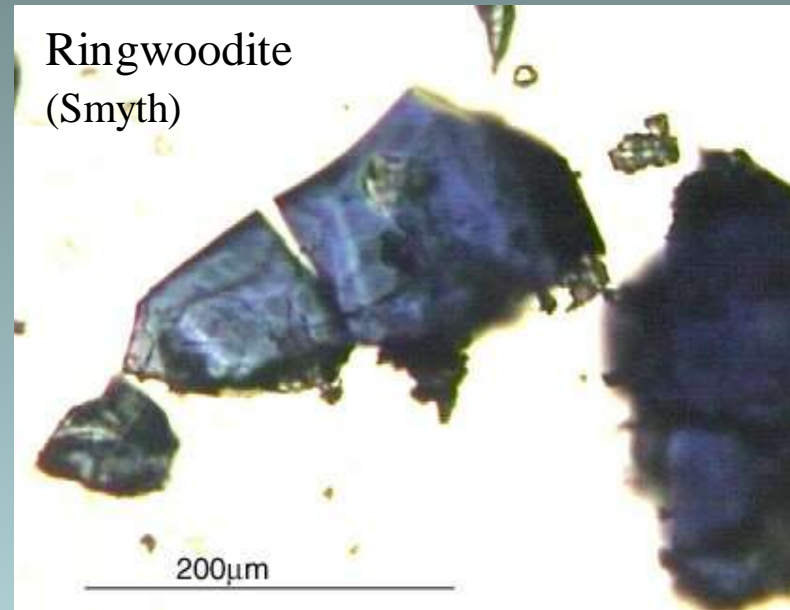


Clapeyron slope = -2.8 MPa/K

# Determination of Clapeyron Slopes

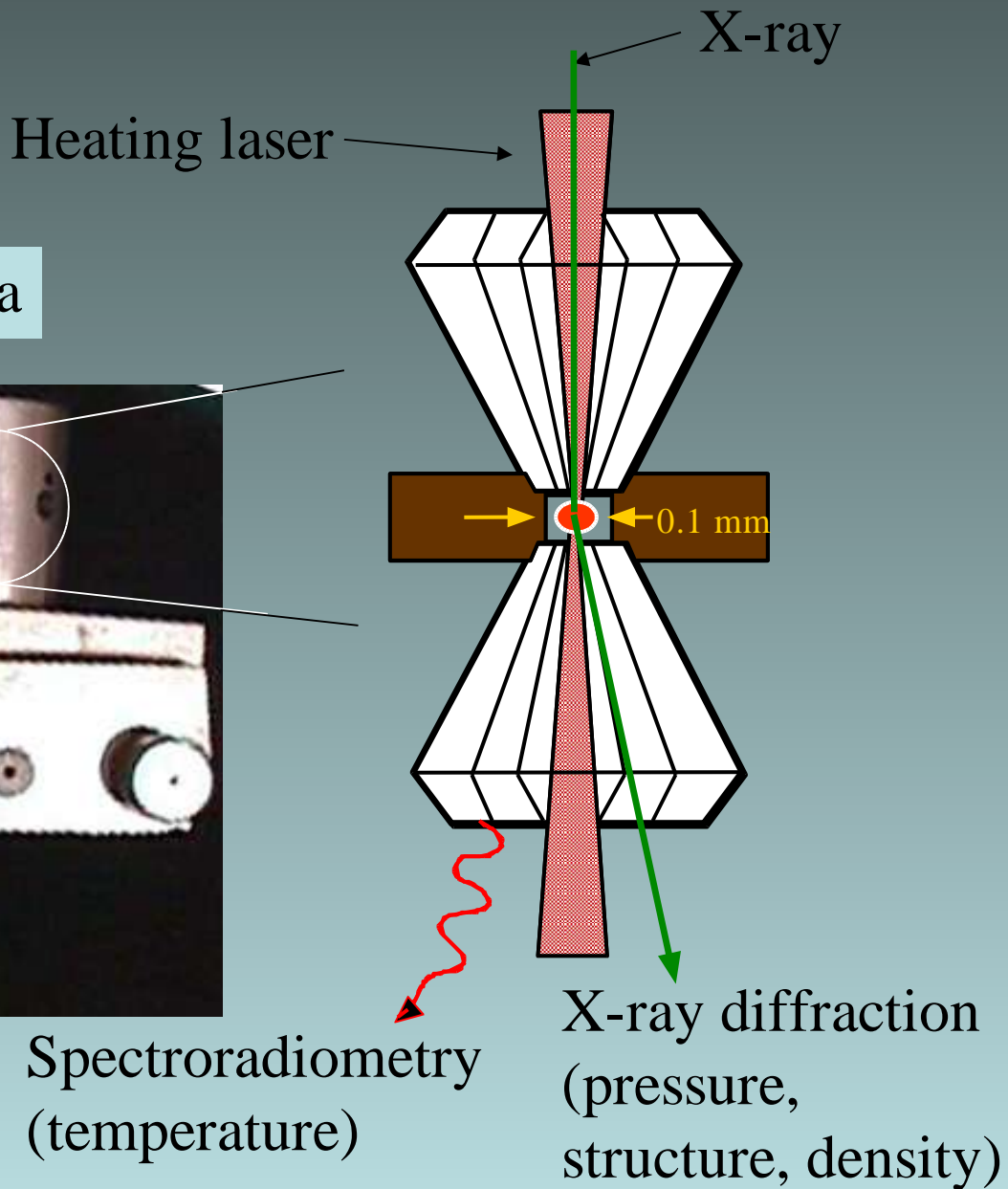
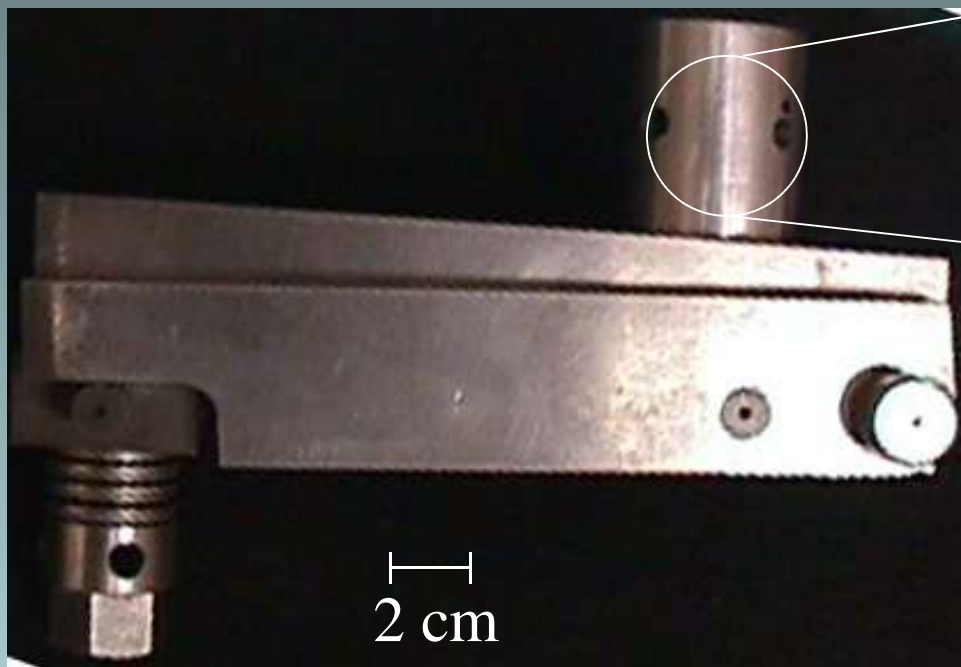
$$\frac{dP}{dT} = \frac{DV_{rxn}}{DS_{rxn}}$$

Phase Equilibria  
ex-situ  
**in-situ**  
Thermodynamic



# The Laser-Heated Diamond Anvil Cell

$$\text{Pressure} = \text{Force}/\text{Area}$$



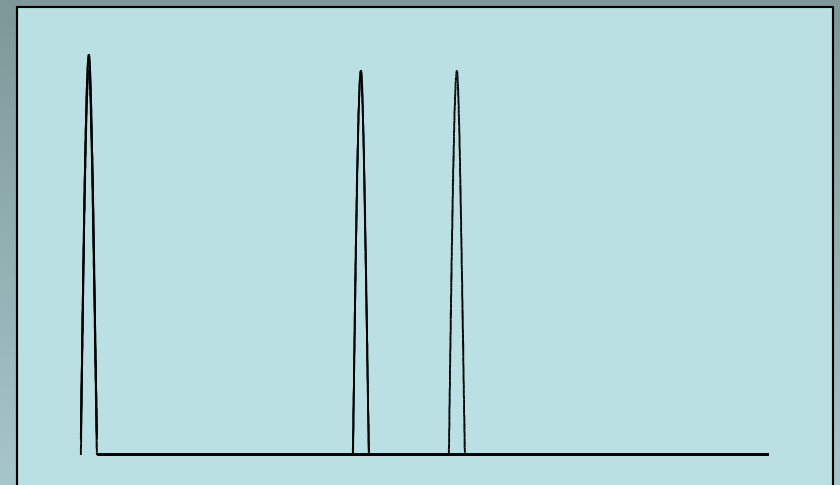
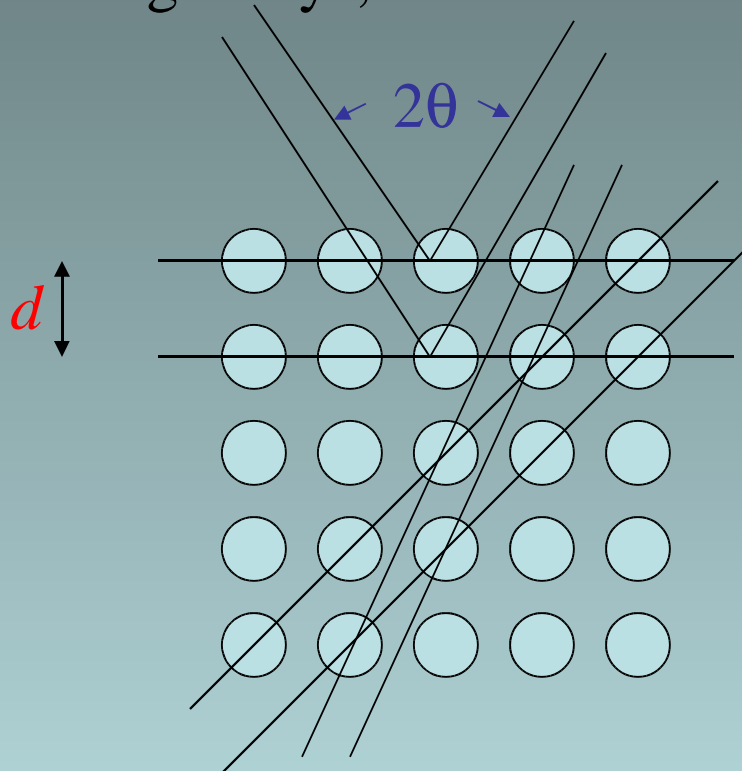
# Techniques

## X-ray Diffraction

incoming x-rays,  $\lambda$       reflected x-rays,  $\lambda$

Diffraction condition:

$$\lambda = 2d \sin(2\theta)$$

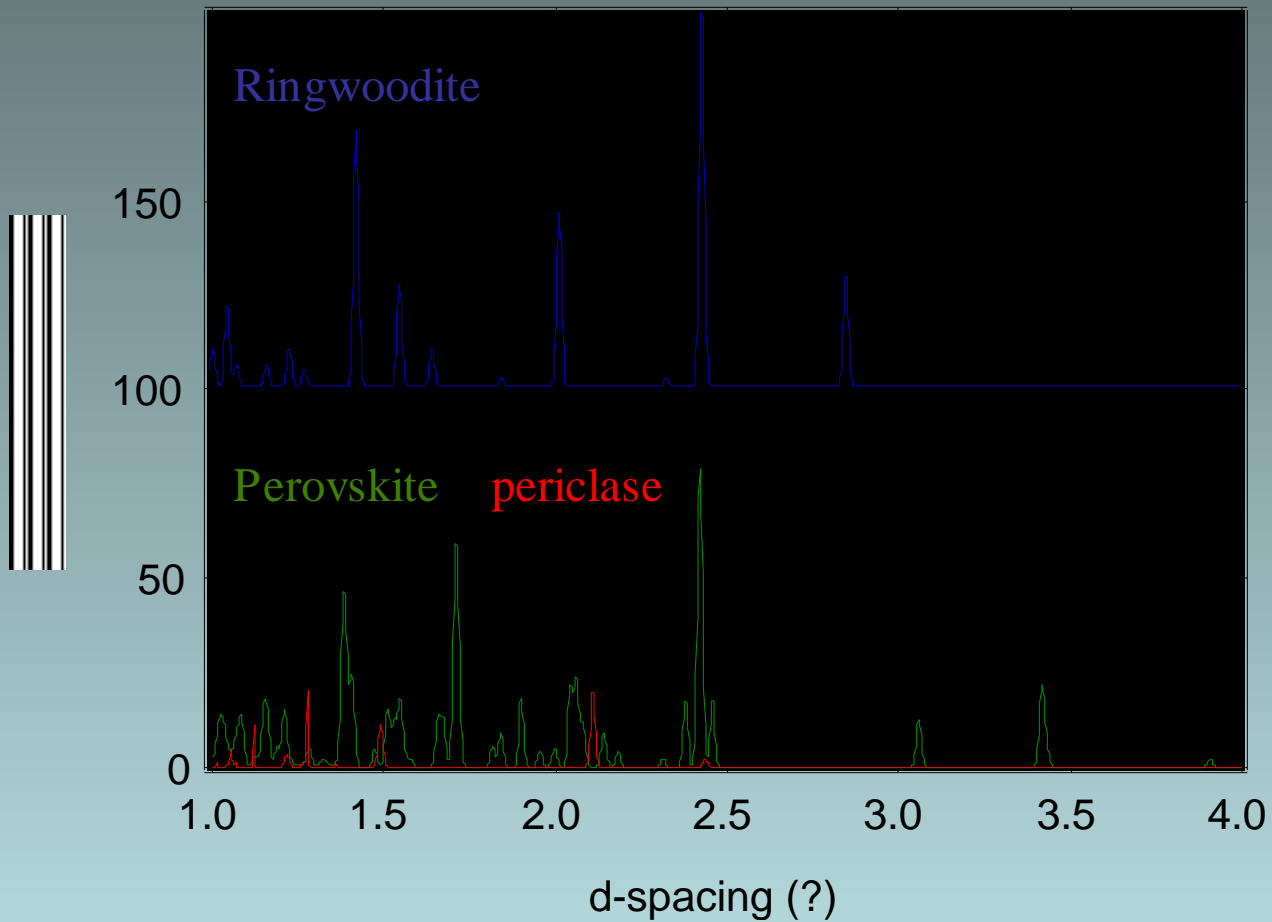


$2\theta$

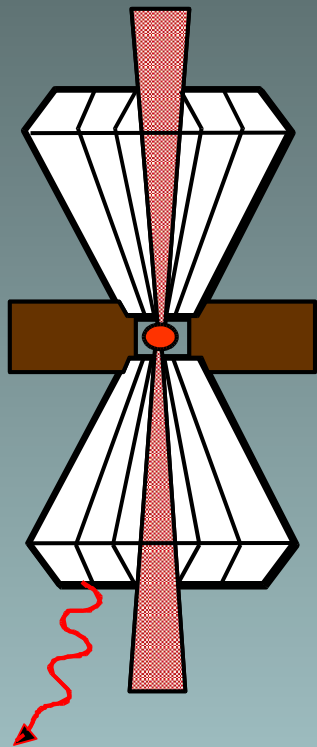
e.g. Cullity

# Techniques

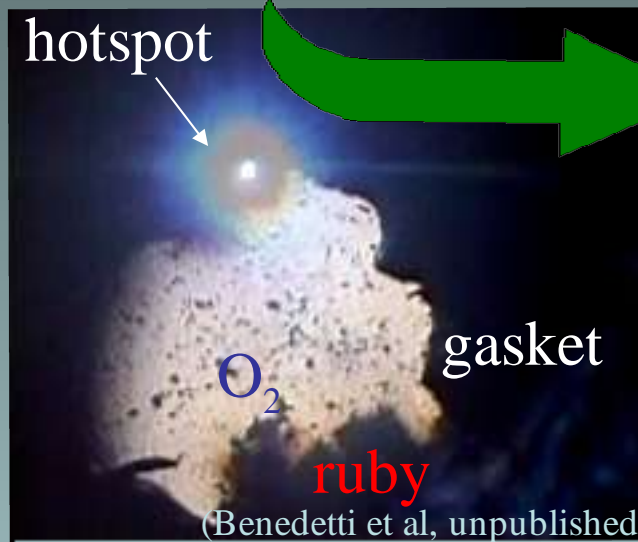
## X-ray Diffraction



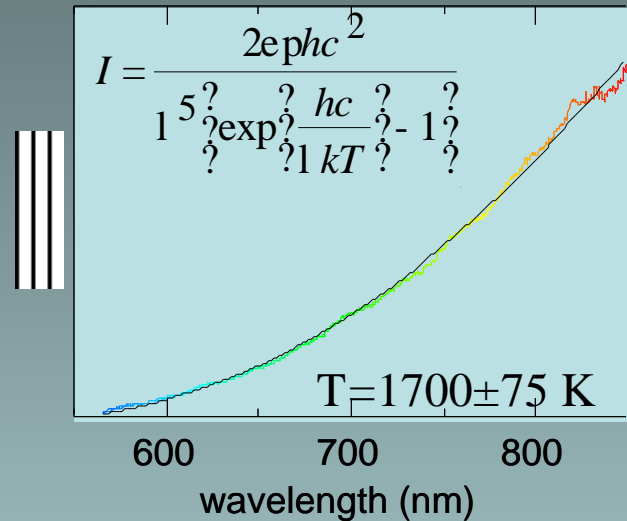
# Temperature Measurements



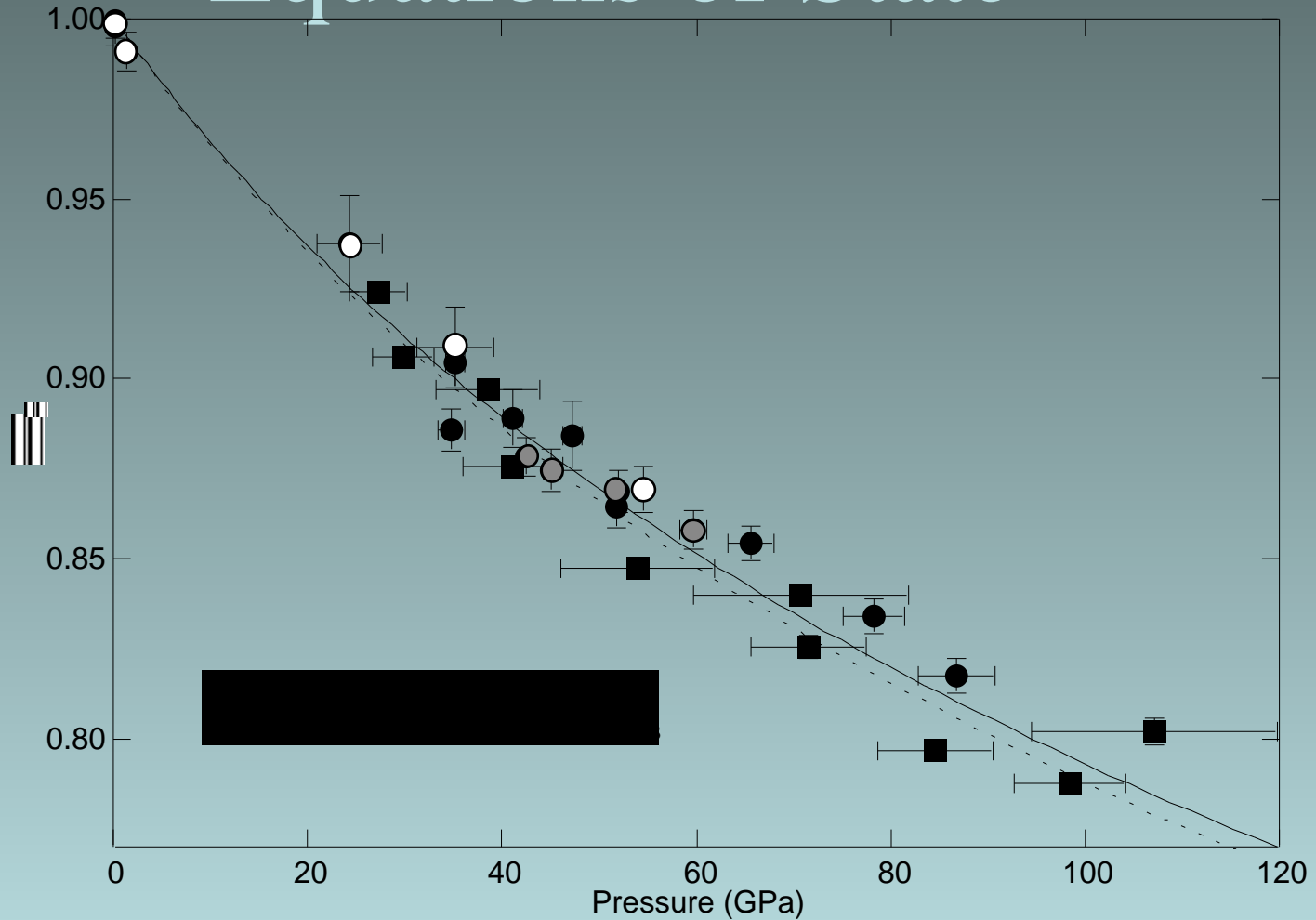
side view



top view



# Pressure Measurements: Equations of State





# Constant Temperature Equations of State

Bulk Modulus  $K_{0T} = \frac{? \ ?P \ ?}{?? \ln(V) \ ?}_T$

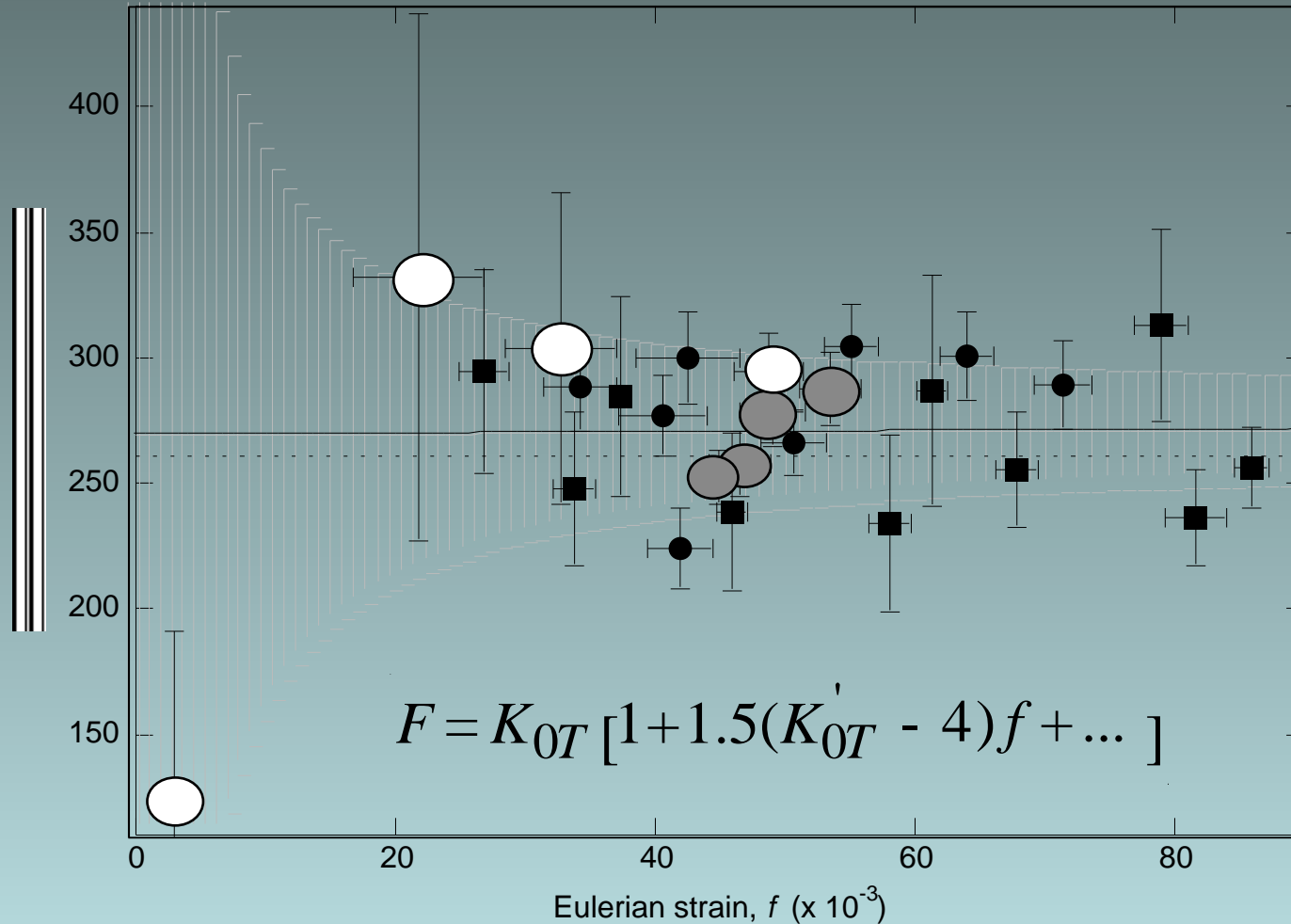
$$f = [(v/v_0)^{-2/3} - 1]/2$$

$$P = 3f(1+2f)^{5/2} K_{0T} [1 + 1.5(K'_{0T} - 4)f + \dots]$$

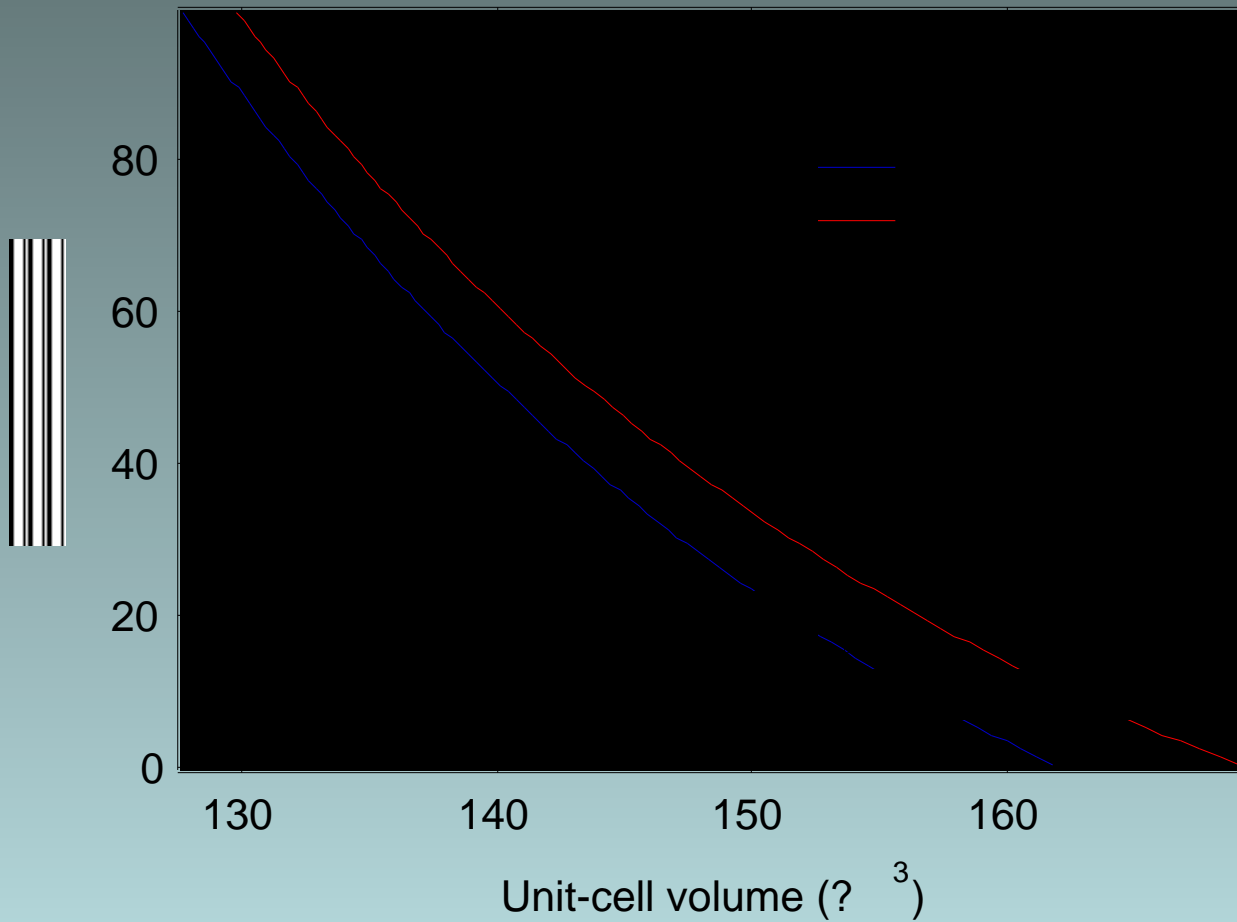
$$F = \frac{P}{3f(1+2f)^{5/2}}$$

$$F = K_{0T} [1 + 1.5(K'_{0T} - 4)f + \dots]$$

# Constant Temperature Equations of State



# PVT Equations of State



# PVT Equations of State

$$P(V, T) = P_{\text{ext}}(V) + P_{\text{th}}(T)$$

Thermodynamic definition  $-\left(\frac{\partial E}{\partial V}\right)_T = P$

$$P_{\text{th}} = -\left(\frac{\partial E_{\text{th}}}{\partial V}\right)_T = \frac{g}{V} E_{\text{th}}$$

Model for internal energy:

e.g. Debye

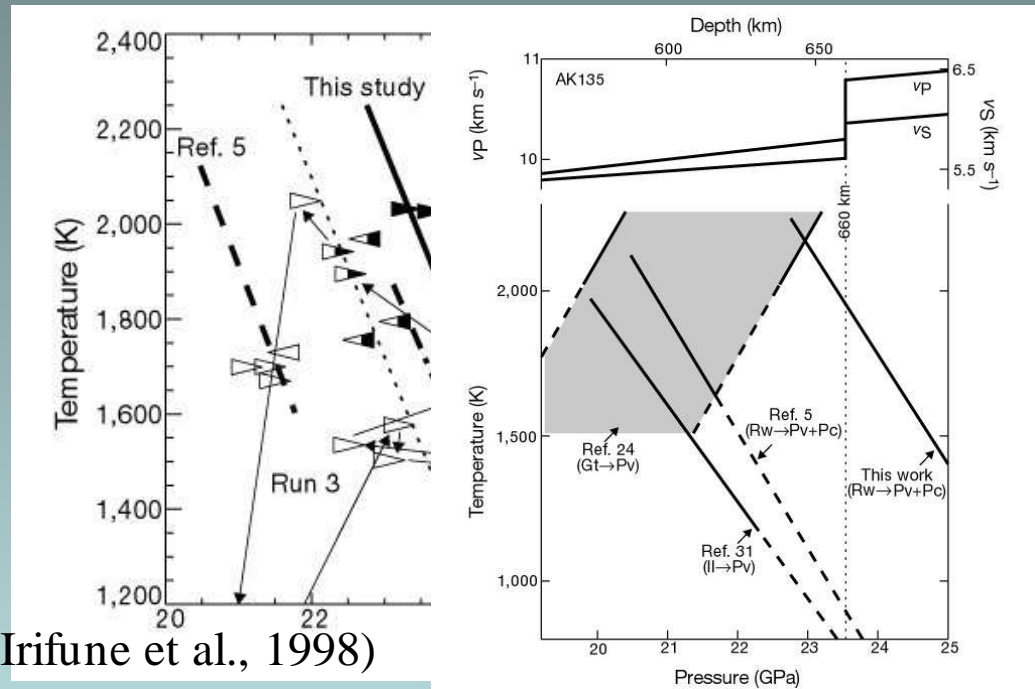
$$E_{\text{th}} = 9nk_B T \left(T/Q_D\right)^3 \int_0^{Q_D/T} \frac{x^3}{e^x - 1} dx$$

# Determination of Clapeyron Slopes

$$\frac{dP}{dT} = \frac{DV_{rxn}}{DS_{rxn}}$$

Shim et al., 2001

Phase Equilibria  
*ex-situ*  
**in-situ**  
 Thermodynamic



Clapeyron slope = -3 MPa/K (Irifune et al., 1998)

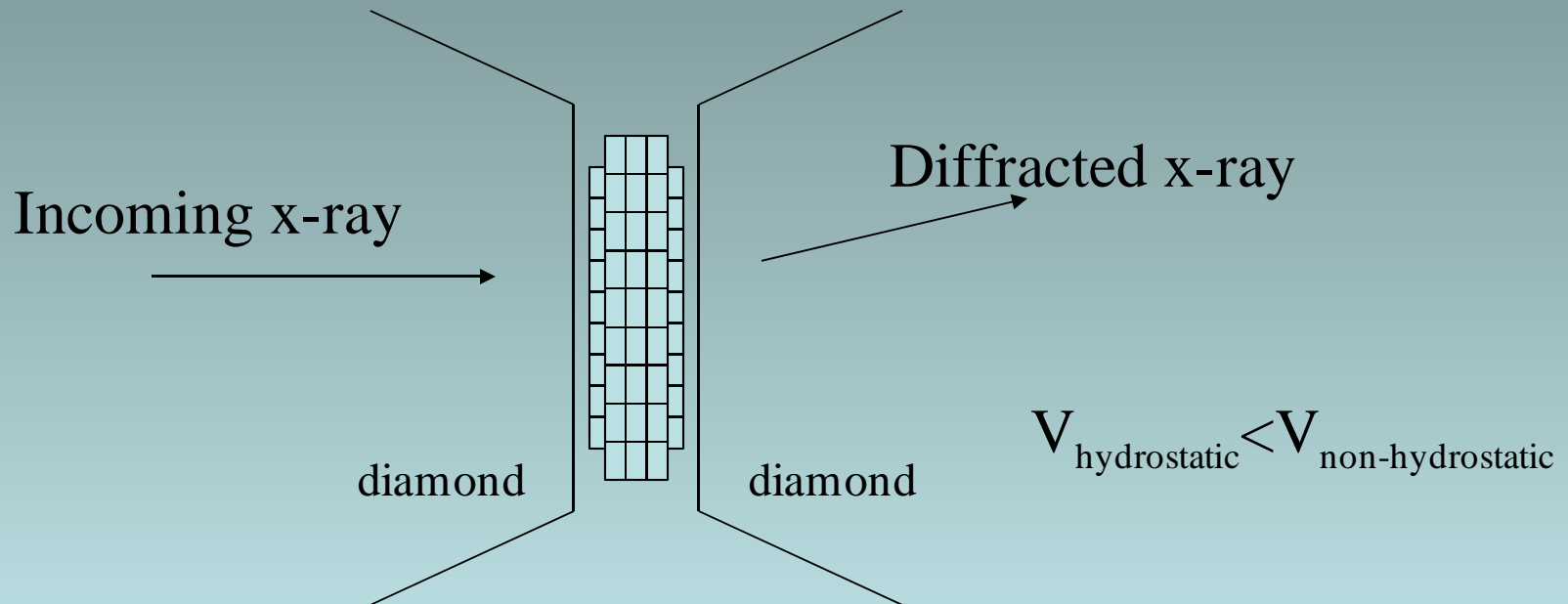
Clapeyron slope = no constraint (Shim et al., 2001; Chudinovskikh et al., 2001)

# Sources of Error

## Non-hydrostatic stresses

Pressure standards

Temperature and pressure gradients

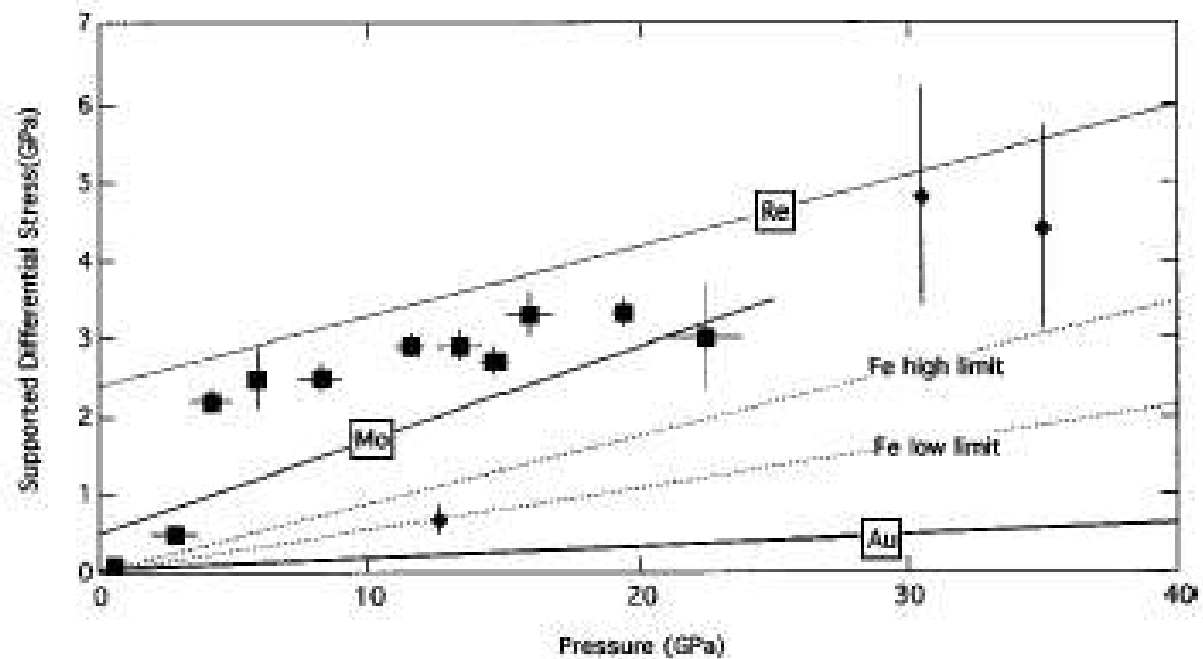


# Sources of Error

## Non-hydrostatic stresses

Pressure standards

Temperature and pressure gradients



Kavner and Duffy, 2003

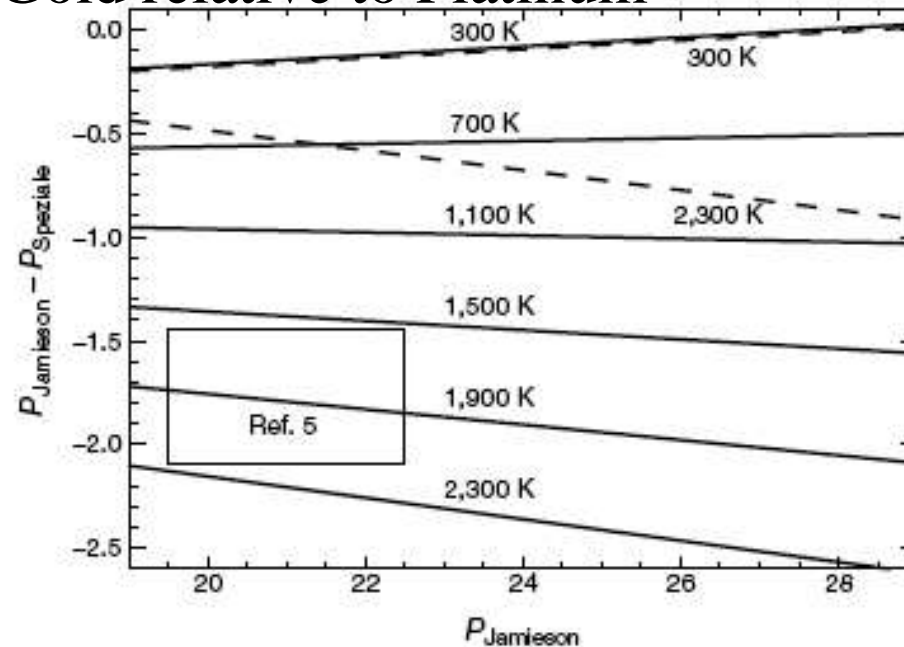
# Sources of Error

Non-hydrostatic stresses

**Pressure standards**

Temperature and pressure gradients

## Gold relative to Platinum



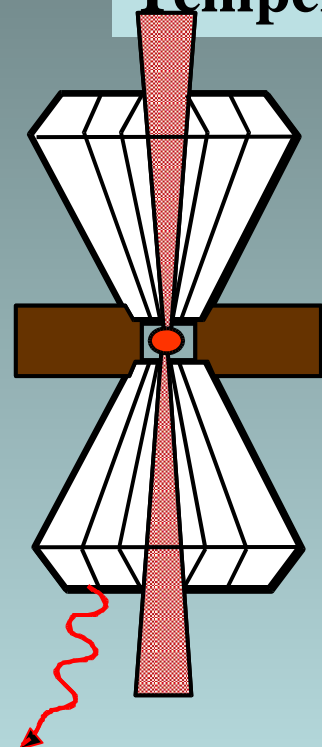


# Sources of Error

Non-hydrostatic stresses

Pressure standards

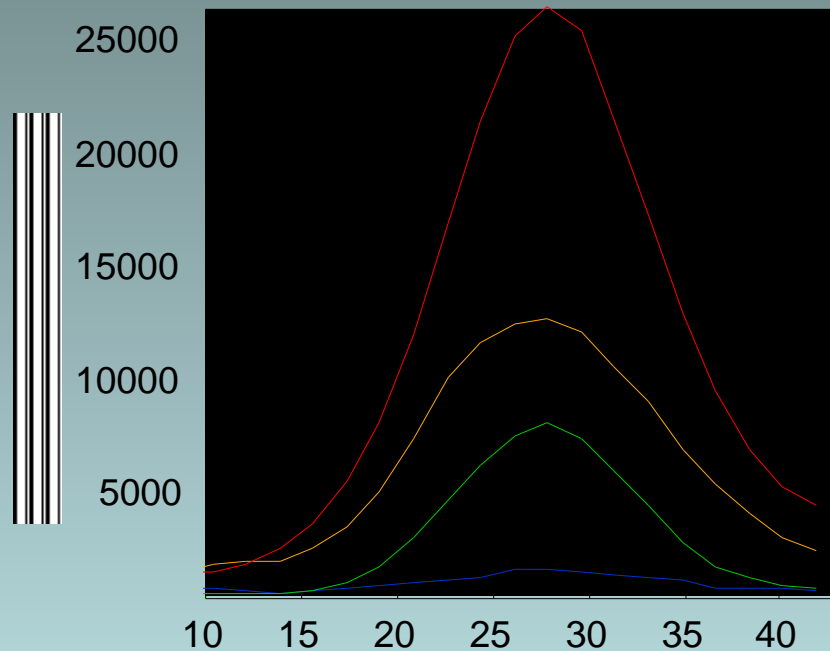
**Temperature and pressure gradients**



side view



top view

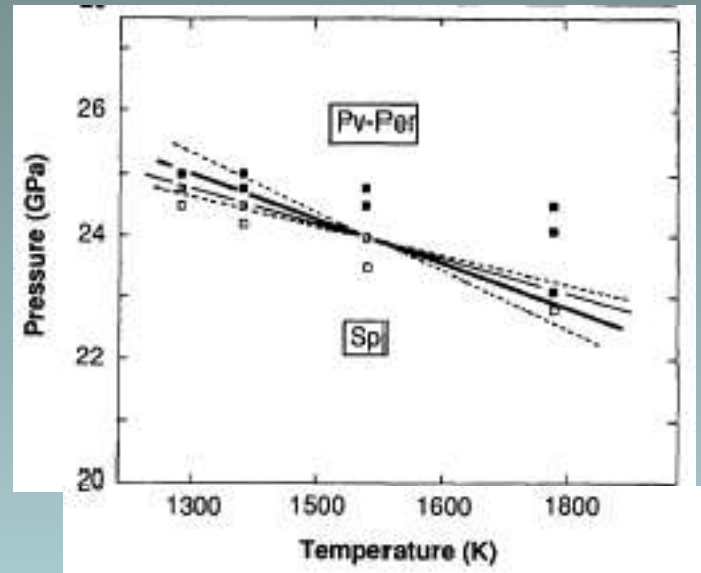


Position ( $\mu\text{m}$ )  
Kavner and Panero, *PEPI* 2004

# Determination of Clapeyron Slopes

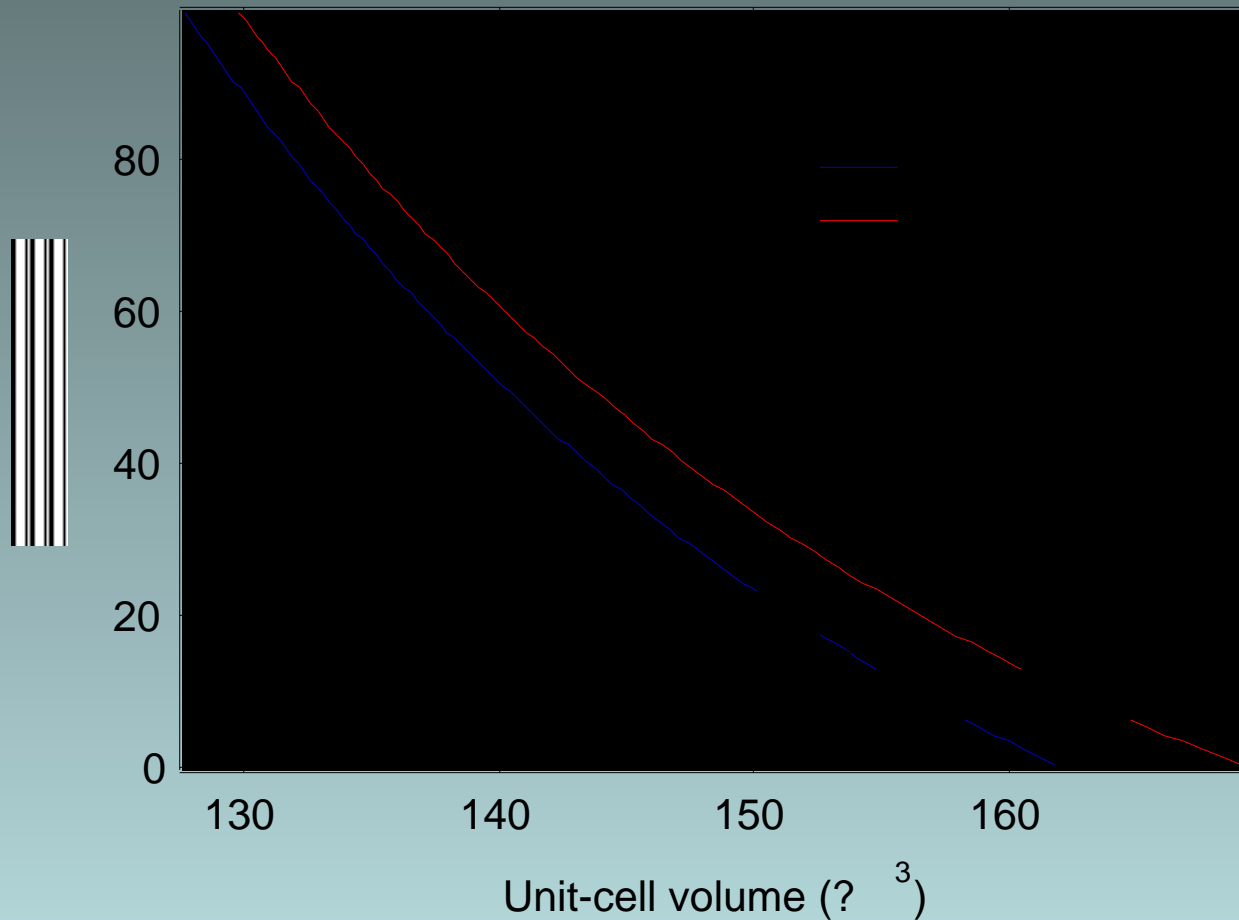
$$\frac{dP}{dT} = \frac{DV_{rxn}}{DS_{rxn}}$$

Phase Equilibria  
ex-situ  
in-situ  
**Thermodynamic**

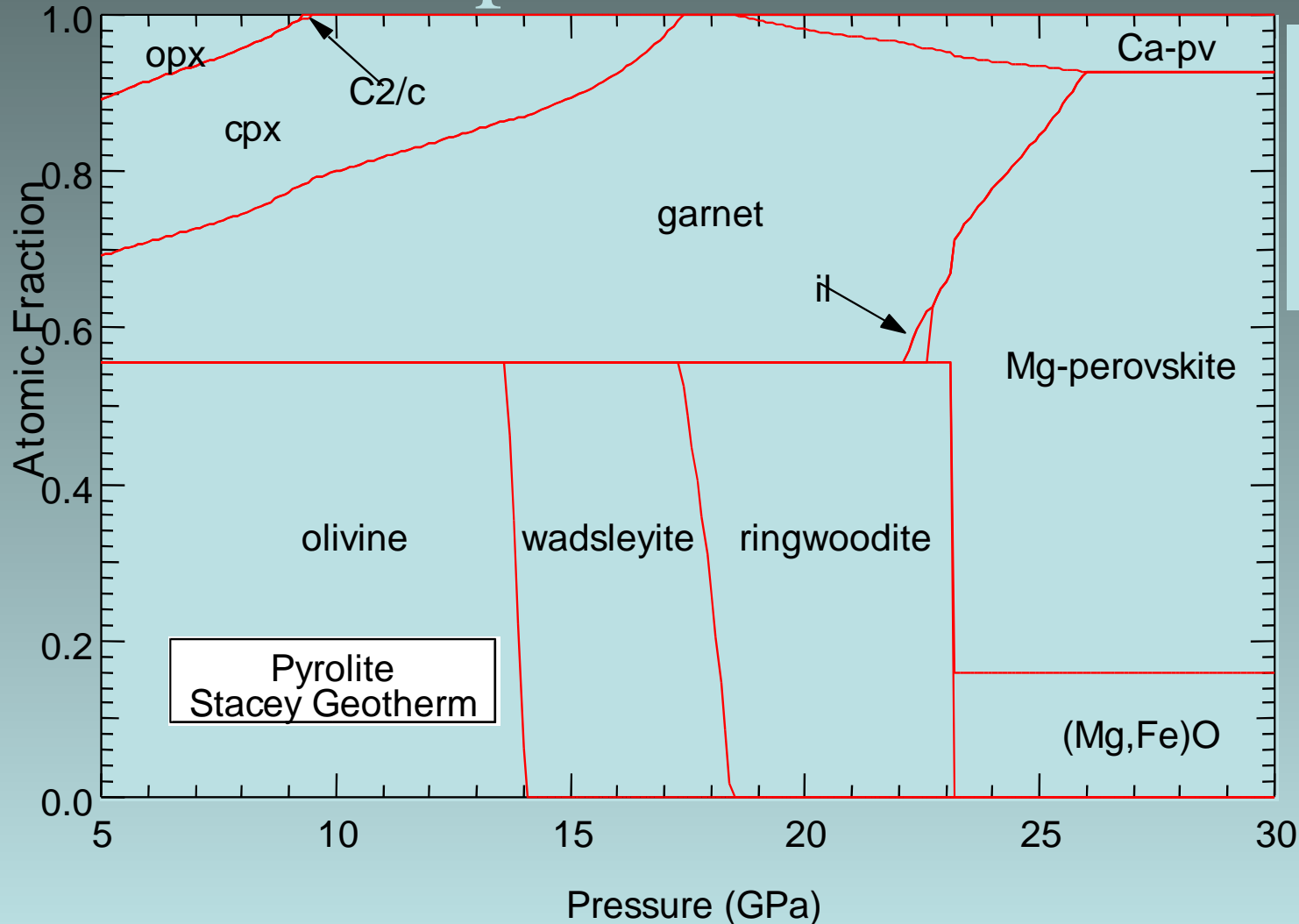


Clapeyron slope =  $-4 \pm 2$  MPa/K

# Interpretation of Tomography: Thermal Variations



# Interpretation of Tomography: Compositional Variations

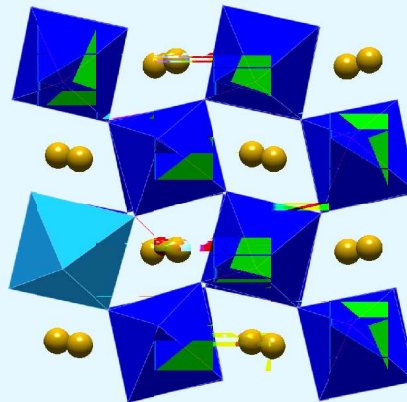


|                                |          |
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| MgO                            | 37.1 wt% |
| FeO                            | 8.3 wt%  |
| Al <sub>2</sub> O <sub>3</sub> | 4.3 wt%  |
| CaO                            | 3.3 wt%  |

# Interpretation of Tomography: Compositional Variations

Perovskite

| Composition  | $K_0$ (GPa) | $\rho$ (Mg/m <sup>3</sup> ) | $\sqrt{K_0/r}$ (km/s) |
|--|-------------|-----------------------------|-----------------------|
| MgSiO <sub>3</sub>   | 262         | 4.12                        | 7.974                 |
| MgSiO <sub>3</sub> ~10% FeO  | 262         | 4.25                        | 7.851                 |
| MgSiO <sub>3</sub> ~3.25% Al <sub>2</sub> O <sub>3</sub>                   | 261         | 4.123                       | 7.956                 |
| MgSiO <sub>3</sub> ~3.25% Al <sub>2</sub> O <sub>3</sub> +H <sub>2</sub> O | 256         | 4.088                       | 7.913                 |



# Theory

Quantum mechanical or classical

–effects of *a priori* assumptions

–size of calculation, time for calculation

General approach:

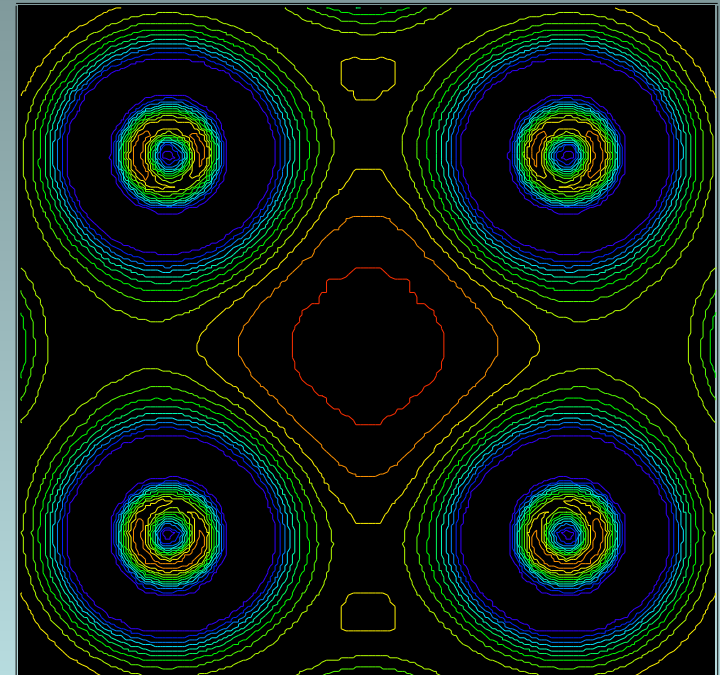
G of each phase

PT-space for lowest energy

Limitations:

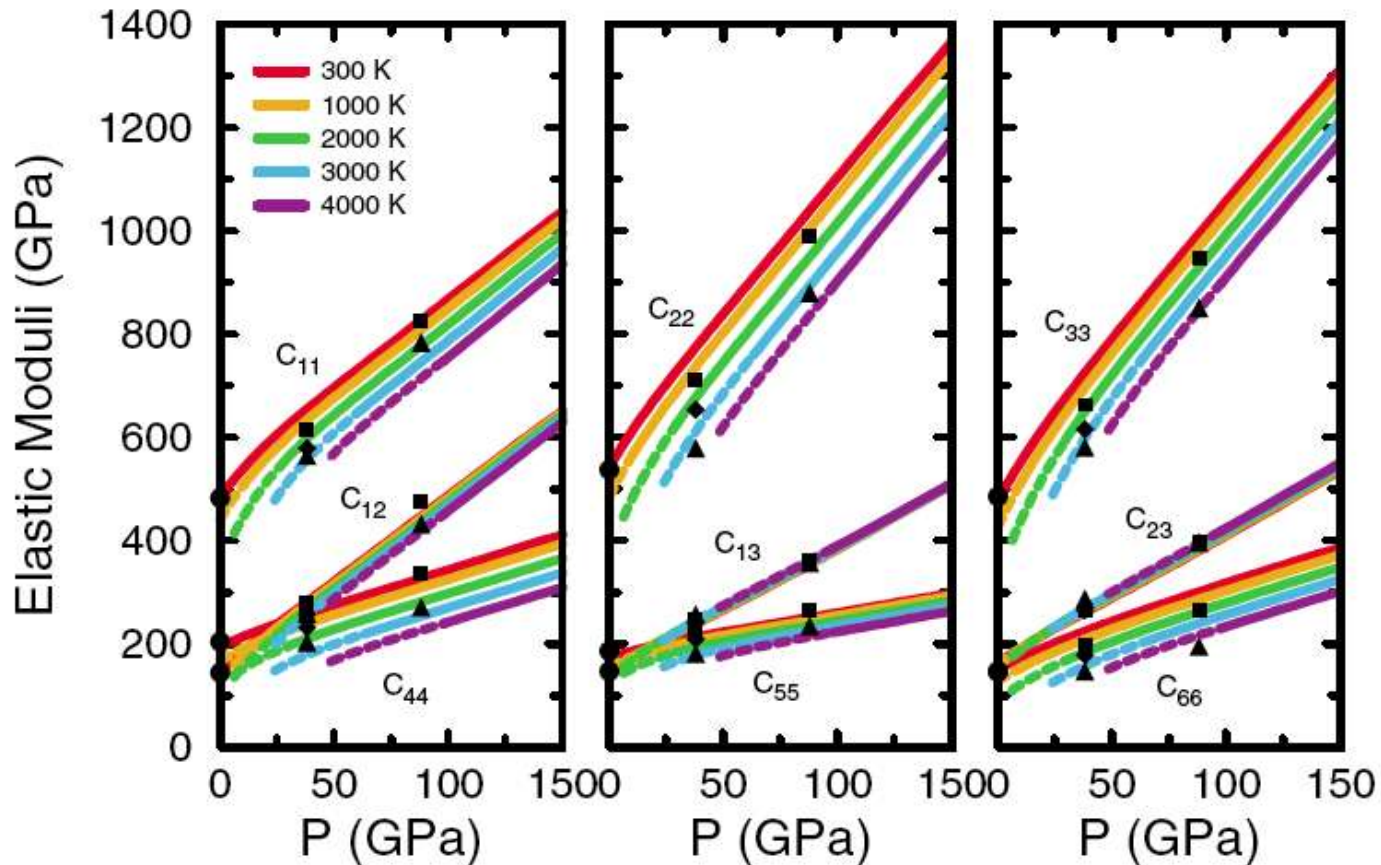
Temperature

Multi-component systems



# Theory

MgSiO<sub>3</sub> perovskite



?

