

# **Subduction III**

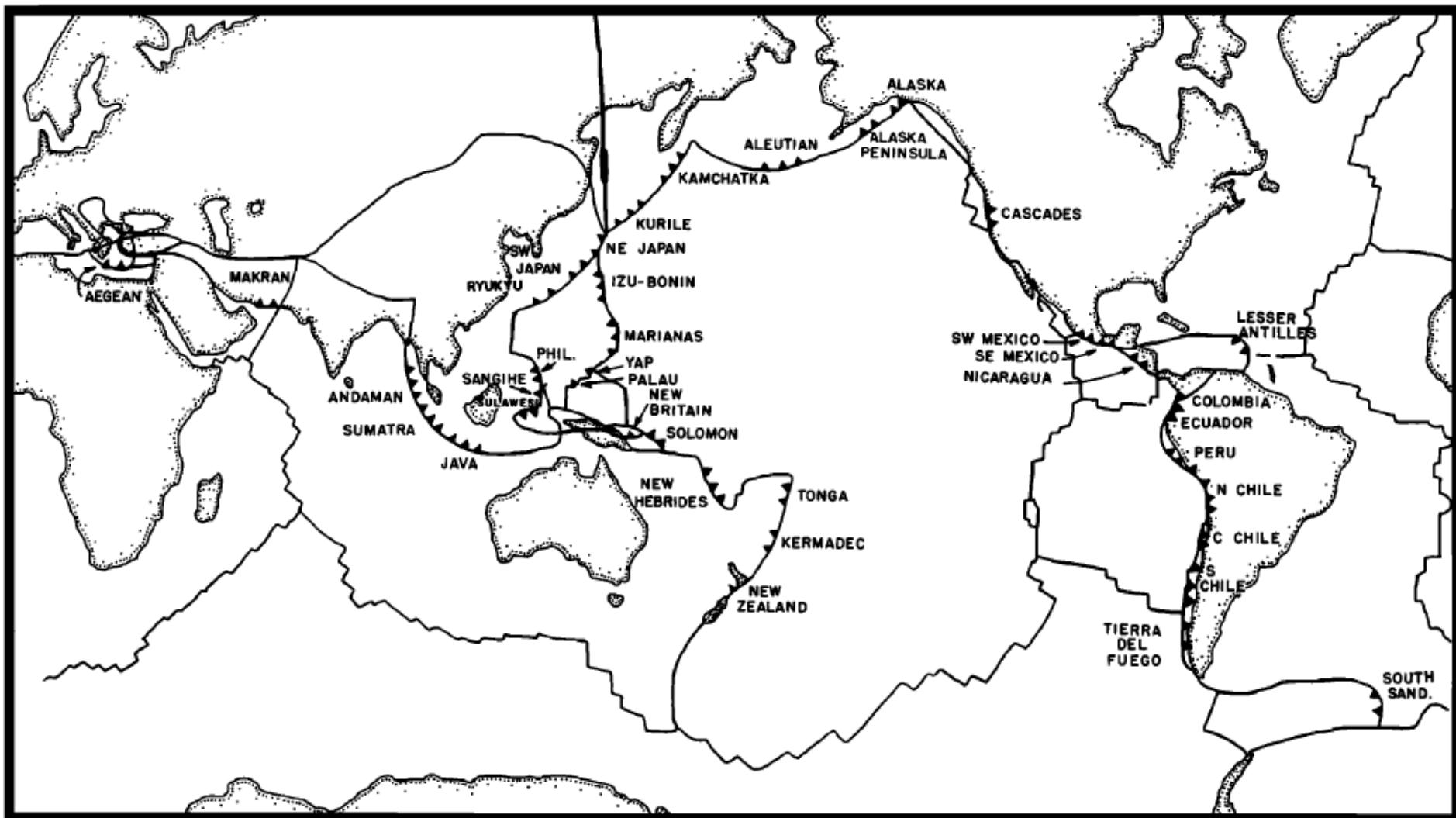
## **Regional subduction zone modeling**

Thorsten W Becker  
University of Southern California

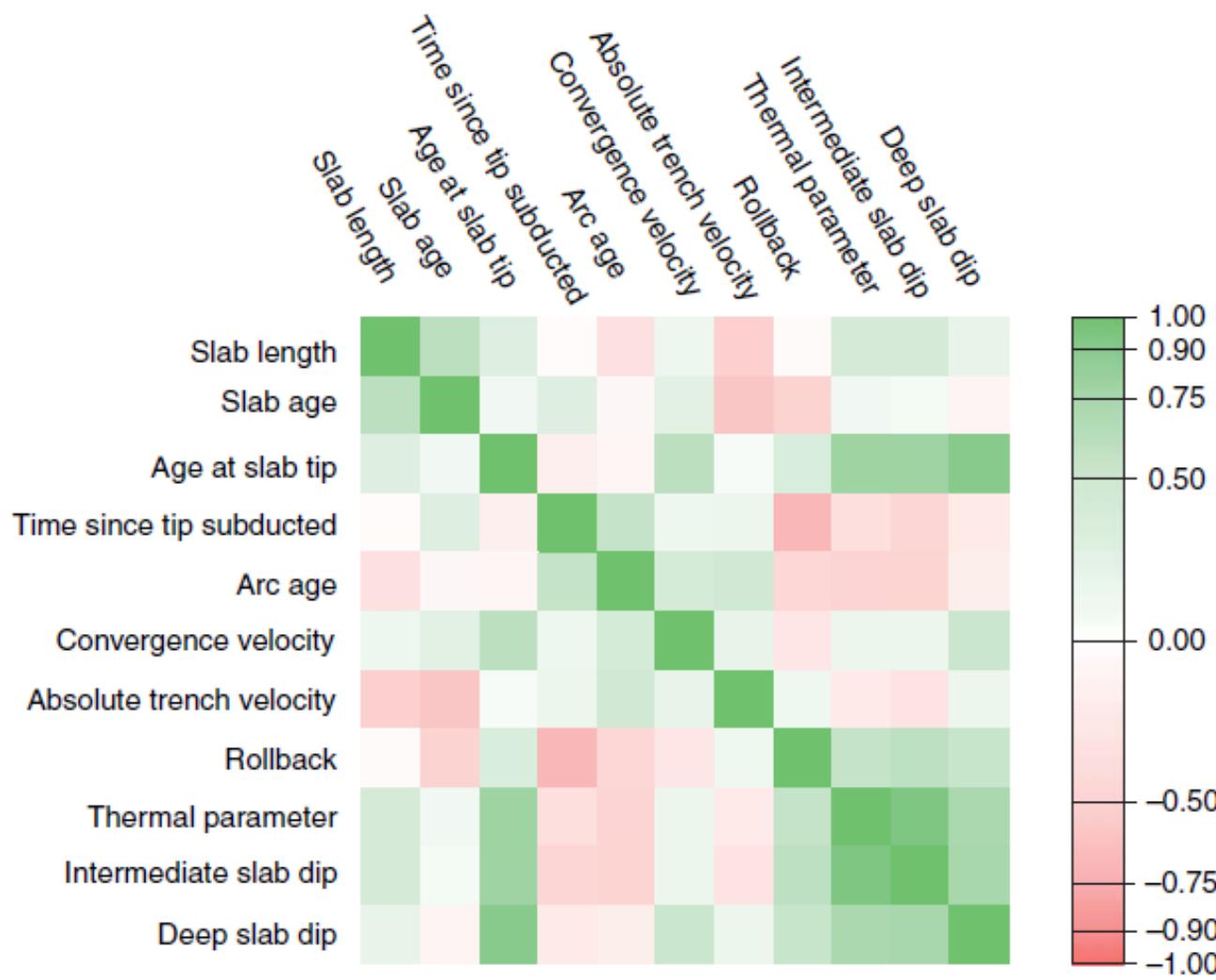
Short course at Universita di Roma TRE  
April 18 – 20, 2011

# Reading

- King, S. (Elsevier Treatise, 2007)
- Billen, M. (Ann Rev, 2009)
- Becker & Faccenna (2009)

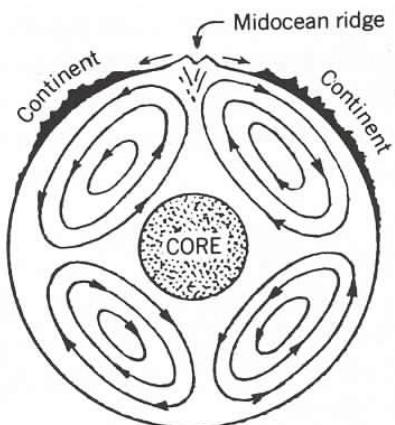
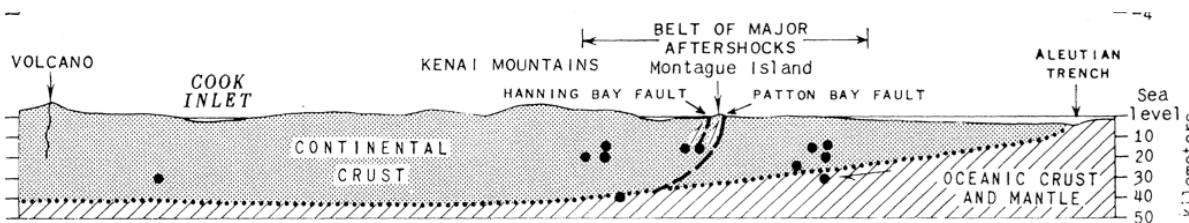


Jarrard (1986)



**Figure 3** Covariance matrix for nine observations compiled from 39 modern subduction zones (Jarrard, 1986). The color scale represents the value of the correlation coefficient, with +1.0 being strongly correlated and -1.0 being strongly anticorrelated. Rollback is the rate of trench migration estimated from the global plate models (Minster and Jordan, 1978). Velocity is the velocity of the plate at the trench from the same global plate models. Slab age is the age of the plate entering the trench, and slab-tip age is calculated using the length of the slab and rate of change of the plate age for the plate entering the trench. The intermediate dip is calculated from the trench to the 100 km depth of the slab. The deep dip is calculated from the 100–400 km depth of the slab. The thermal parameter is the product of the slab age and the length of the slab.

# Pre - Plate Tectonics



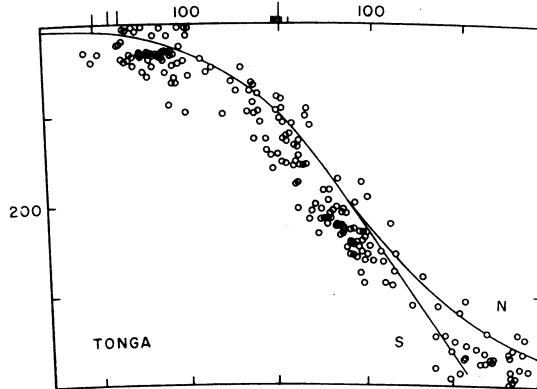
Mantle Convection

- Holmes, 1944

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1940s

- ***Subduction into the mantle was one of the last pieces of the plate tectonics puzzle.***



Mega-shear to 700 km

- Benioff, 1954

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1950s

Internal deformation of subducted lithosphere.

- Isacks & Molnar, 1969

Deep planar fault zone

- Elsasser, 1968

Lithospheric thrusting

- Plafker, 1965

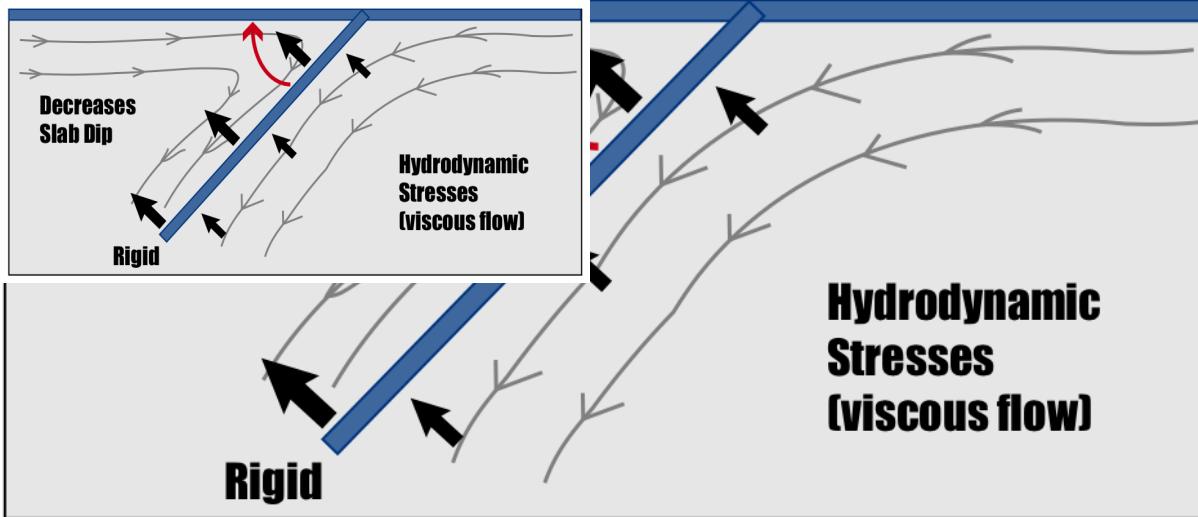
Crustal-scale thrusting

- Hess, 1962

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1960s

# Plate Tectonics: in the SZ

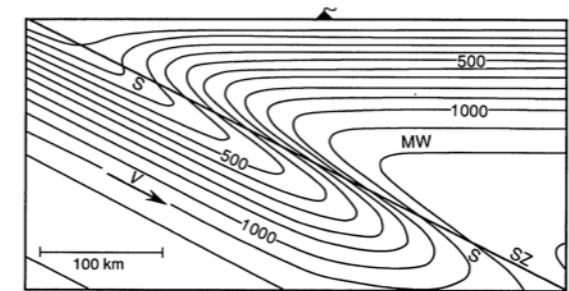


Corner-flow model.  
- McKenzie, 1969

- Yokokura, 1981  
Dynamic topography  
from corner-flow  
- Sleep, 1975

1960s

- ***Early analytic models capture major processes.***
  - ***Force balance on slab.***
  - ***Slab thermal structure.***

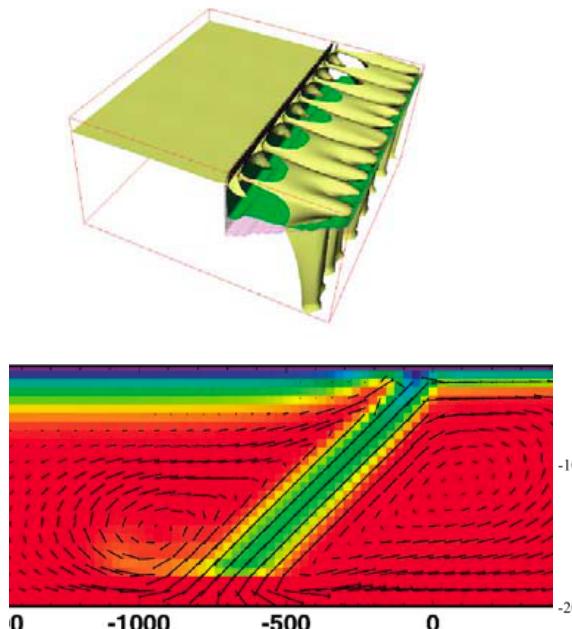


Linking slab temp. to  
mineralogy & petrology  
- Peacock, 1990

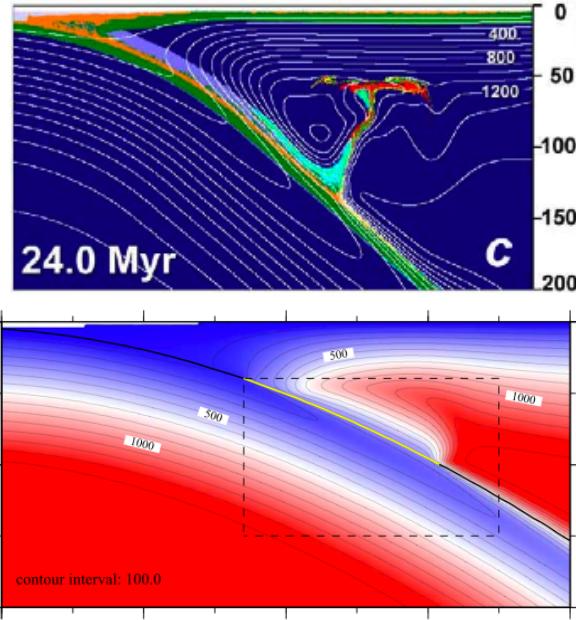
Slab thermal structure  
-Toksov, 1971; 1973

1970s    1990s

# Kinematic Slab - Dynamic Wedge



Wedge/back arc flow  
- Bodri & Bodri, 1978  
- Toksov & Hsui, 1978



Convection in the wedge  
- Ida, 1983  
- Honda, 1985

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1970s

- ***Slab & mantle wedge thermal/min./pet. structure.***
- ***Fluid transport***
- ***Seismic anisotropy.***

3D, anisotropy implication  
- Kneller & van Keken, 2007

Non-linear viscosity

- Kneller et al., 2007

Compositional & phase:  
density & viscosity  
- Gerya & Yuen, 2003

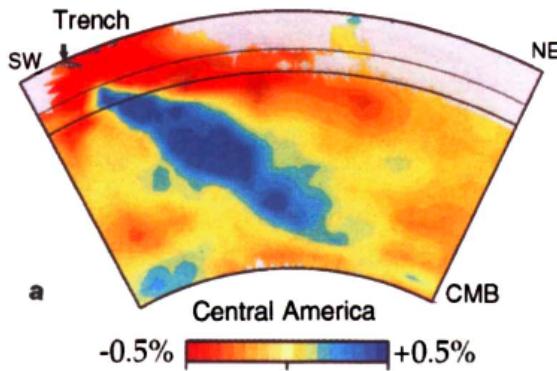
Low viscosity wedge  
- Honda & Saito, 2003

Temperature-dep. visc.  
- Eberle, 2001

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1990s      2000s

# Observations



Arc curvature, slab dip,  
subduction velocity.  
- Tovich & Schubert, 1978

**1970s**

- ***Connecting kinematics to dynamics.***

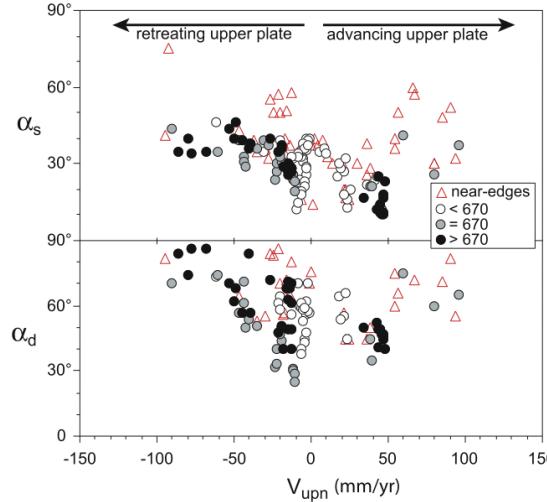


Plate kinematics &  
characteristics  
- Jarrard, 1986

Geoid & dynamic topo.  
- Hager 1984

Plate kinematics &  
characteristics  
- Mueller et al., 1997  
- Lallemand et al., 2005

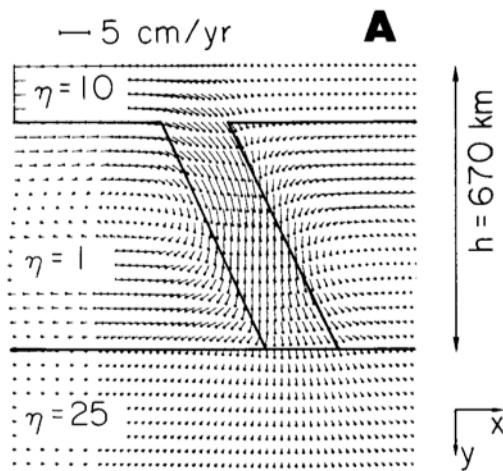
Seismic anisotropy  
- Russo & Silver, 1994  
- Fischer et al., 1998  
- Long & Silver, 2008

Seismic tomography  
- e.g., van der Hilst, 1997

Plate tectonic recons.  
- e.g., DeMets, 1990

**1990s      2000s**

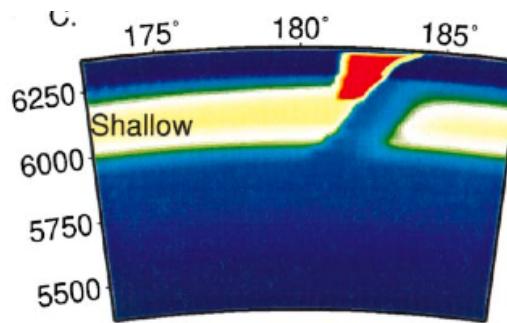
# Instantaneous (quasi) Dynamic



Stress-state in slab  
- Vassiliou, 1984

1980s

- **Rheologic Structure:**
  - mantle, slab, plate boundaries, wedge, crust...
- **Surface deformation:**
  - topography, geoid, stress-state.



3D, Weak plate bndy,  
non-linear rheology  
- Zhong & Gurnis, 1996

3D, Lateral (moderate)  
viscosity variations  
- Moresi et al., 1996

2D, Faults & non-linear  
viscosity  
- Zhong & Gurnis, 1992, 1994

2D, Overriding plate  
root geometry & slab  
suction

- Driscoll et al., 2009

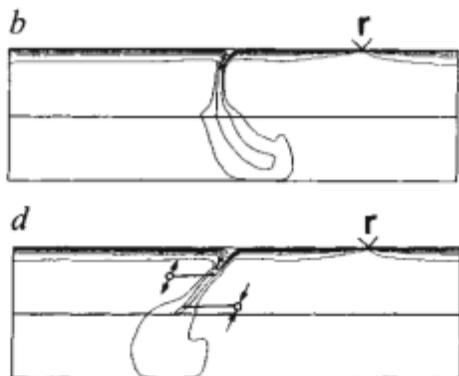
3D, Slab strength effect  
toroidal & poloidal flow  
- Piromallo et al., 2006

3D, Temp-dep, low  
viscosity wedge  
- Billen & Gurnis, 2001

1990s

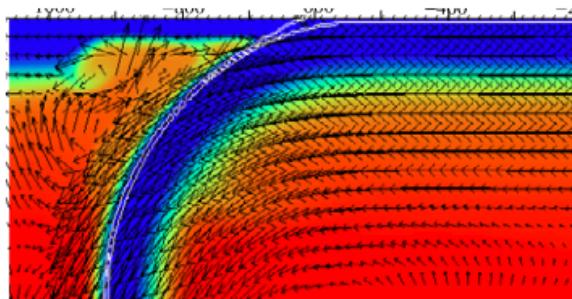
2000s

# Fully Dynamic (t-dependent)



2D, Temp-dep,  
- Gurnis & Hager 1988

2D, Phase trans. (mech)  
- Christensen & Yuen, 1984



2D, Subduction initiation  
- Toth & Gurnis, 1998

2D, Trench migration  
- Olbertz et al., 1997  
- Griffiths et al., 1995

2D, Phase trans.  
(T-dep. viscosity)  
- King, 1991

2D, wedge rheology  
- Arcay et al., 2008

3D, Slab width effects  
- Stegman, 2006

2D, Slab detachment

- Gerya & Yuen, 2004  
3D, Trench migration

- Funiciello et al., 2003  
2D, Comp., grain-size-  
dep. slab visc  
- Cizkova et al., 2002

2D, Oceanic plateaus  
- van Hunen et al 2000

## 1980s

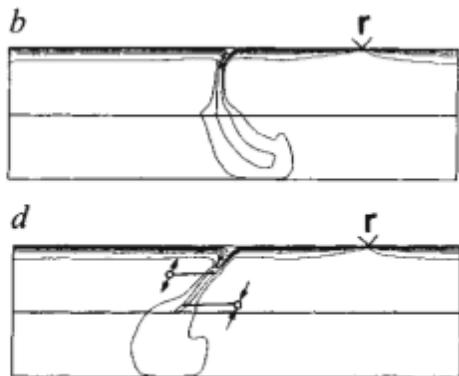
- **Buoyancy forces: phase transition, slab, crust...**
- **Rheologic structure: mantle, slab, wedge...**
- **Geometry: 2-D, 3-D, slab edges, interactions...**

## 1990s

- **Buoyancy forces: phase transition, slab, crust...**
- **Rheologic structure: mantle, slab, wedge...**
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## 2000s

# Fully Dynamic (t-dependent)

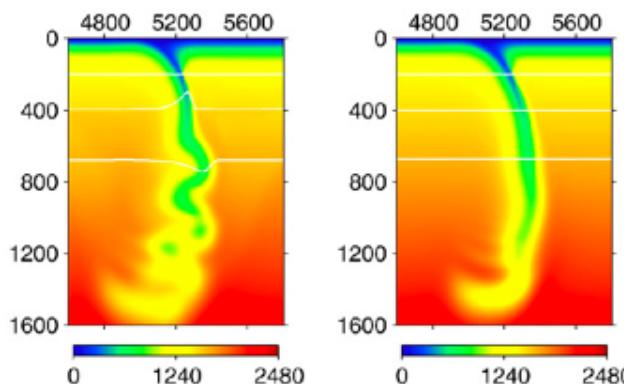


2D, Temp-dep,  
- Gurnis & Hager 1988

2D, Phase trans. (mech)  
- Christensen & Yuen, 1984

## 1980s

- **Buoyancy forces: phase transition, slab, crust...**
- **Rheologic structure: mantle, slab, wedge...**
- **Geometry: 2-D, 3-D, slab edges, interactions...**



2D, Trench migration  
- Olbertz et al., 1997  
- Griffiths et al., 1995

2D, Phase trans.  
(T-dep. viscosity)  
- King, 1991

## 1990s

3D, Slab-edge flow &  
slab depth  
- Honda, 2009

2D, Slab Buckling LM.  
- Behounkova & Cizkova 2008

2D, Double-slab sub.  
- Mishin et al., 2008

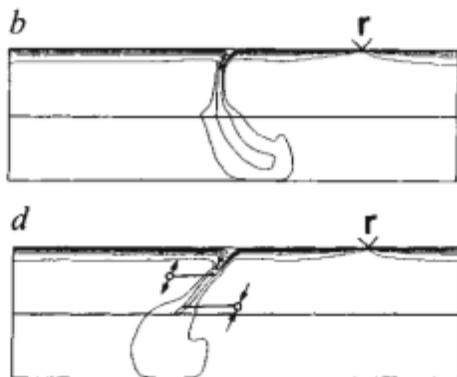
2D, 1-sided subduction  
- Gerya et al., 2008

2D, Flat slabs & LVC  
- Manea & Gurnis, 2007

2D, wedge rheology  
3D, Slab width effects  
2D, Slab detachment  
3D, Trench migration  
- Gerya & Yuen, 2004  
2D, Inhomogeneous size dep. slab visc  
- Van Hunen et al. 2000

## 2000s

# Fully Dynamic (t-dependent)



2D, Temp-dep,  
- Gurnis & Hager 1988

2D, Phase trans. (mech)  
- Christensen & Yuen, 1984

2D, Meta-stable olivine,  
- Schmeling, 1999

2D, Subduction initiation  
- Toth & Gurnis, 1998

2D, Trench migration  
- Olbertz et al., 1997  
- Griffiths et al., 1995

2D, Phase trans.  
(T-dep. viscosity)  
- King, 1991

2D, Compressibility  
- Lee & King, 2009

2D, Ridge-trench int.  
- Burkett & Andrews, 2009

2D, Coupled/uncoupled  
continental collision  
- Faccenda et al., 2009

3D, Slab-edge flow & slab depth  
- Hager & Buckling LM.  
2D, Double-sided subduction  
- Doubled-sided subduction  
2D, Flat slabs & 10°C  
- Manea & Gurnis, 2007

2D, wedge rheology  
3D, Airy isostasy effects  
2D, Slab detachment  
3D, Trench migration  
- Gervais & Yuen, 2004  
2D, Deepening plates  
- Van Hunen et al. 2000

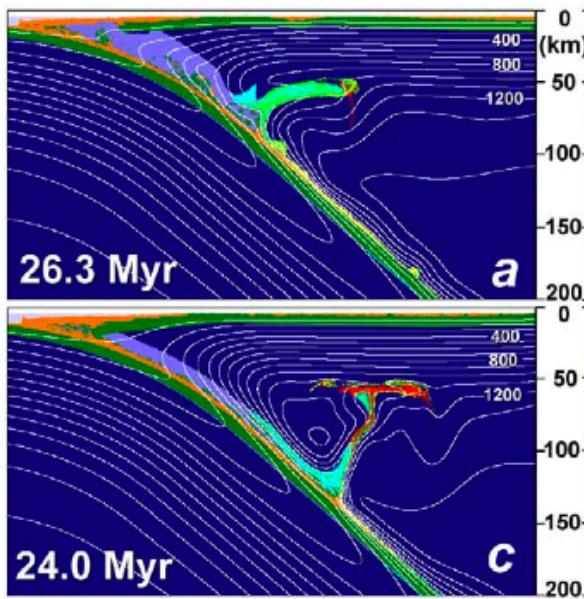
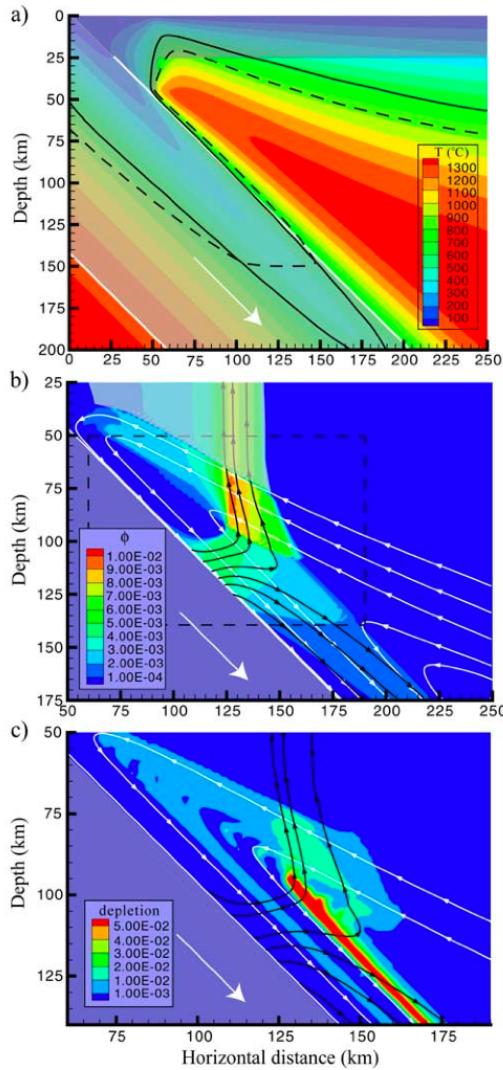
## 1980s

- **Buoyancy forces: phase transition, slab, crust...**
- **Rheologic structure: mantle, slab, wedge...**
- **Geometry: 2-D, 3-D, slab edges, interactions...**

## 1990s

## 2000s

# Mineralogical-Petrological



Fully-coupled mantle-wedge dynamics & petrology  
- Baker-Hebert et al., 2009

Fluid transport, melting

- Cagniocle et al., 2007

Composite crust-mantle density & rheology in wedge

- Gerya & Yuen, 2003

Min./pet. implications

- Davies & Stevenson, 1992

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**1990s      2000s**

- **Need coupled solid & fluid flow, density & rheology, detailed tracking of composition & phase.**

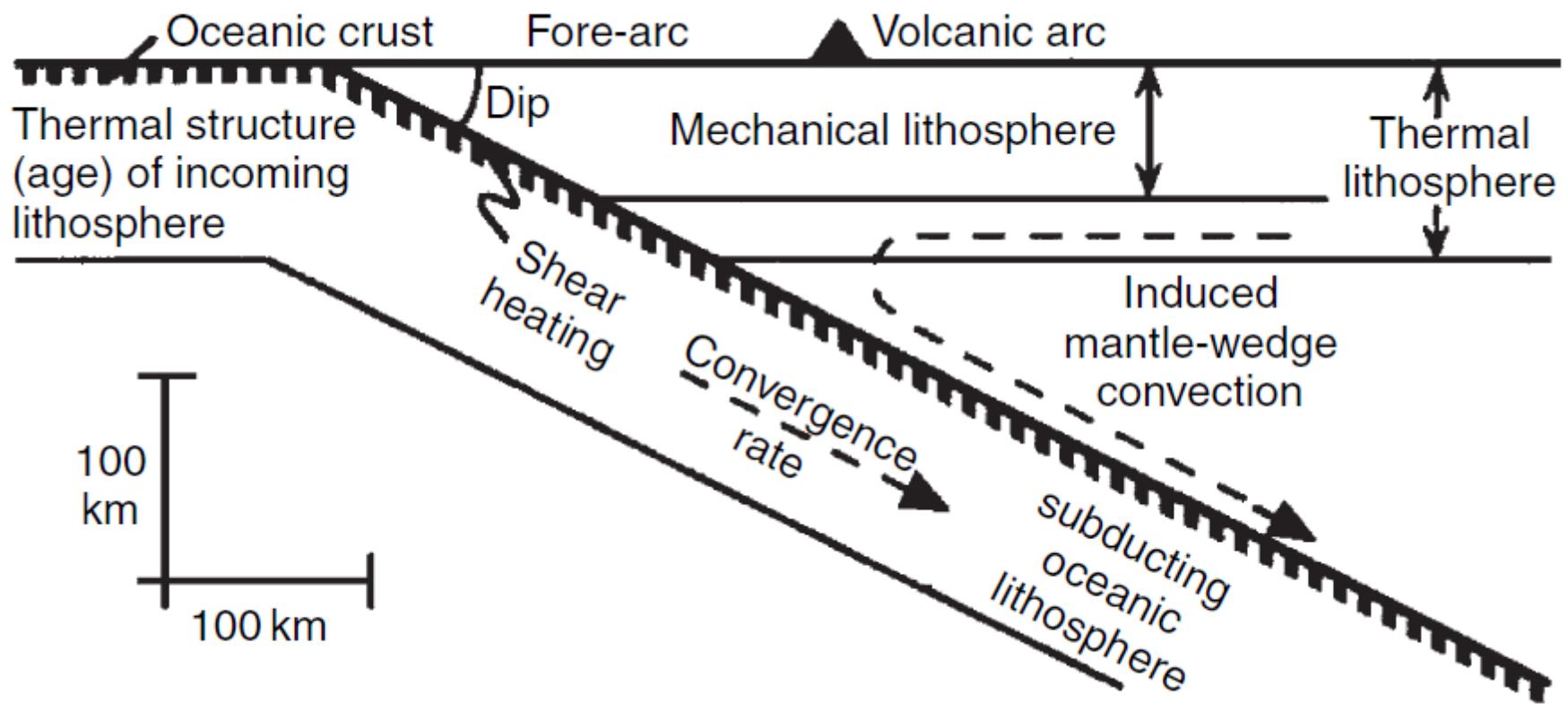
# A Multi-variate System

- **Geometrical Variables**
  - 2D vs. 3D
  - Over-riding plate
  - Interaction w/ other plate boundaries.
- **Mineral-/Petro-logical**
  - Compositional variation
    - Density
    - Rheology
- **Physical Properties**
  - Rheology
  - Thermal parameters ( $\alpha, \kappa$ )
  - Compressibility
- **Coupled Systems**
  - Solid phase changes
  - Hydration/dehydration
  - Melting

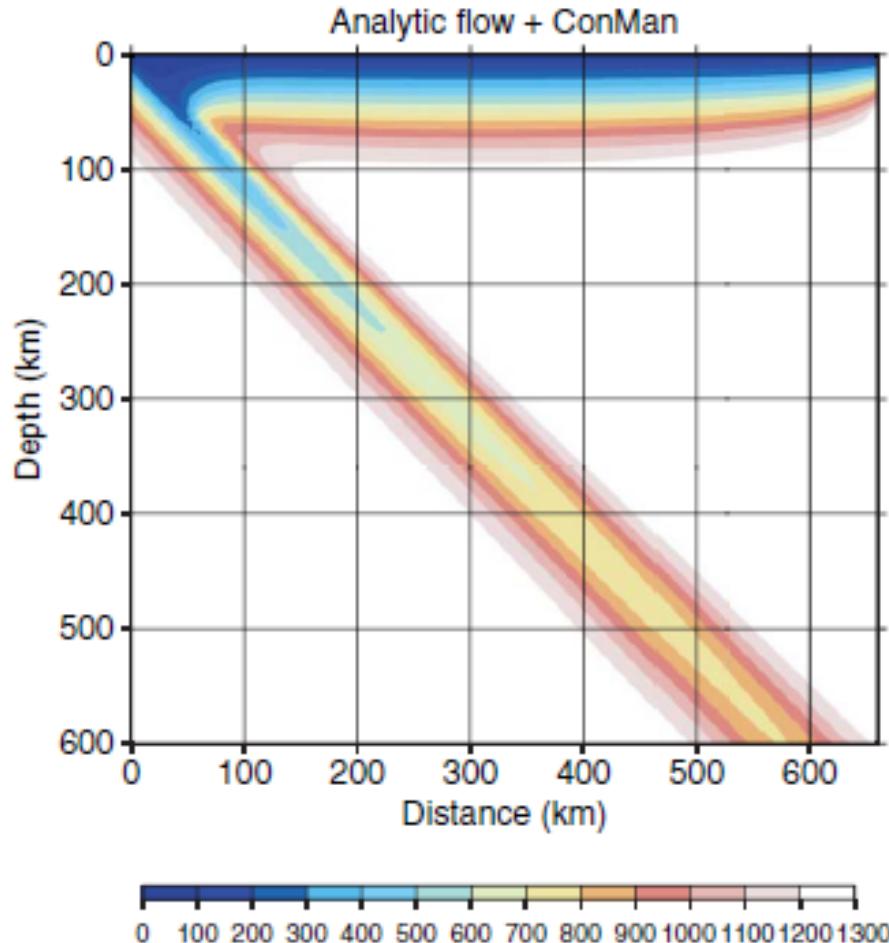
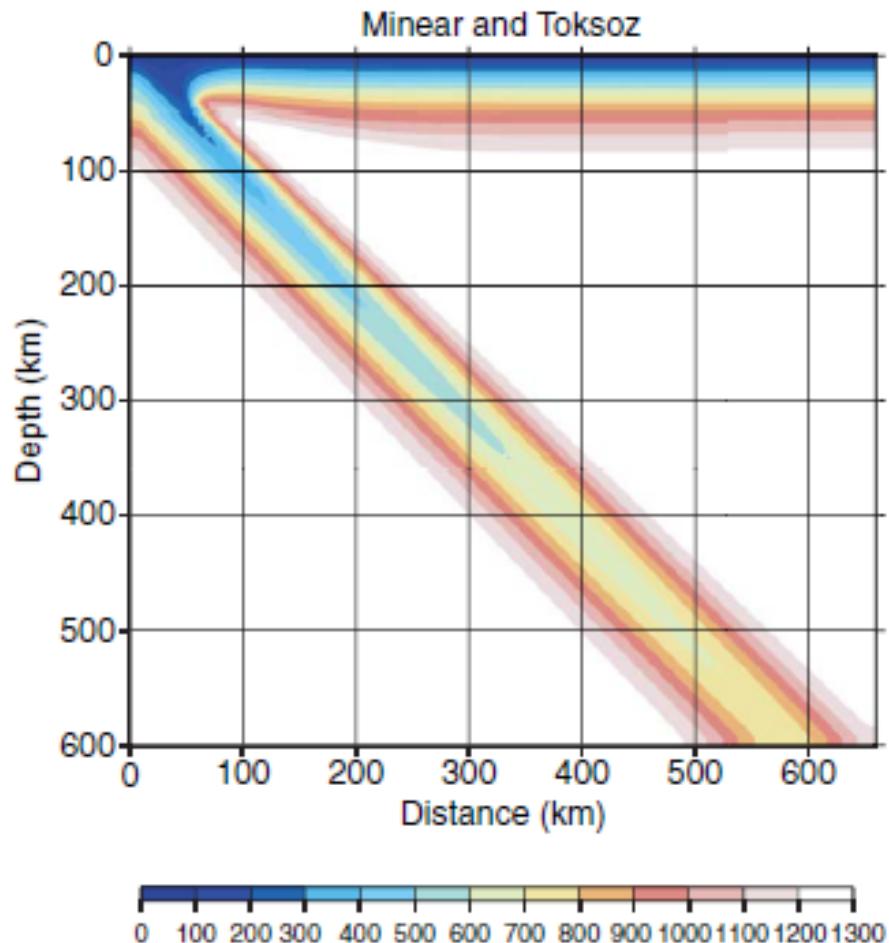
***Link to Observations & Time Evolution***

***Transform a kinematic theory to a dynamic theory.***

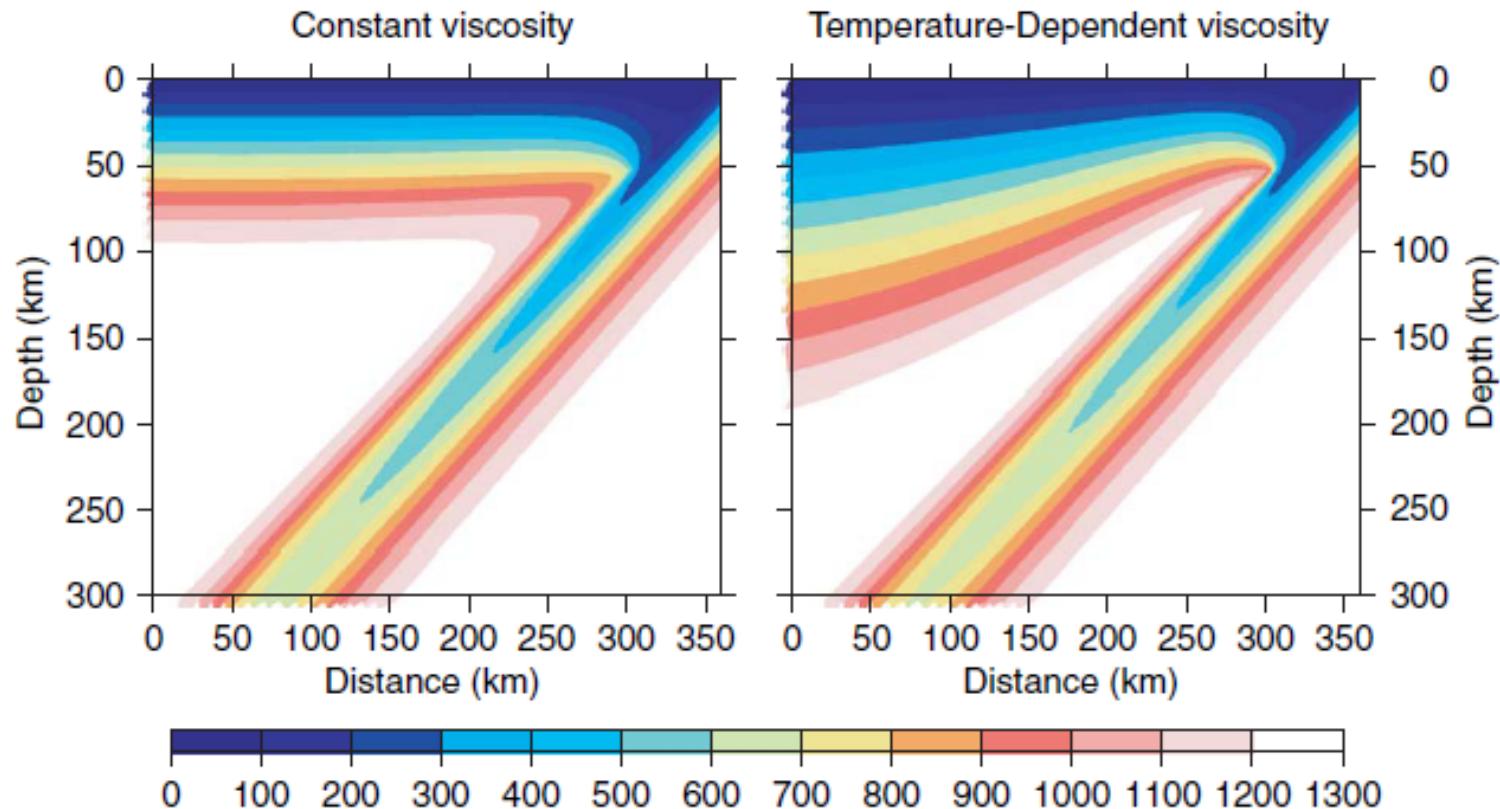
# **Kinematic models**



Peacock, 1996

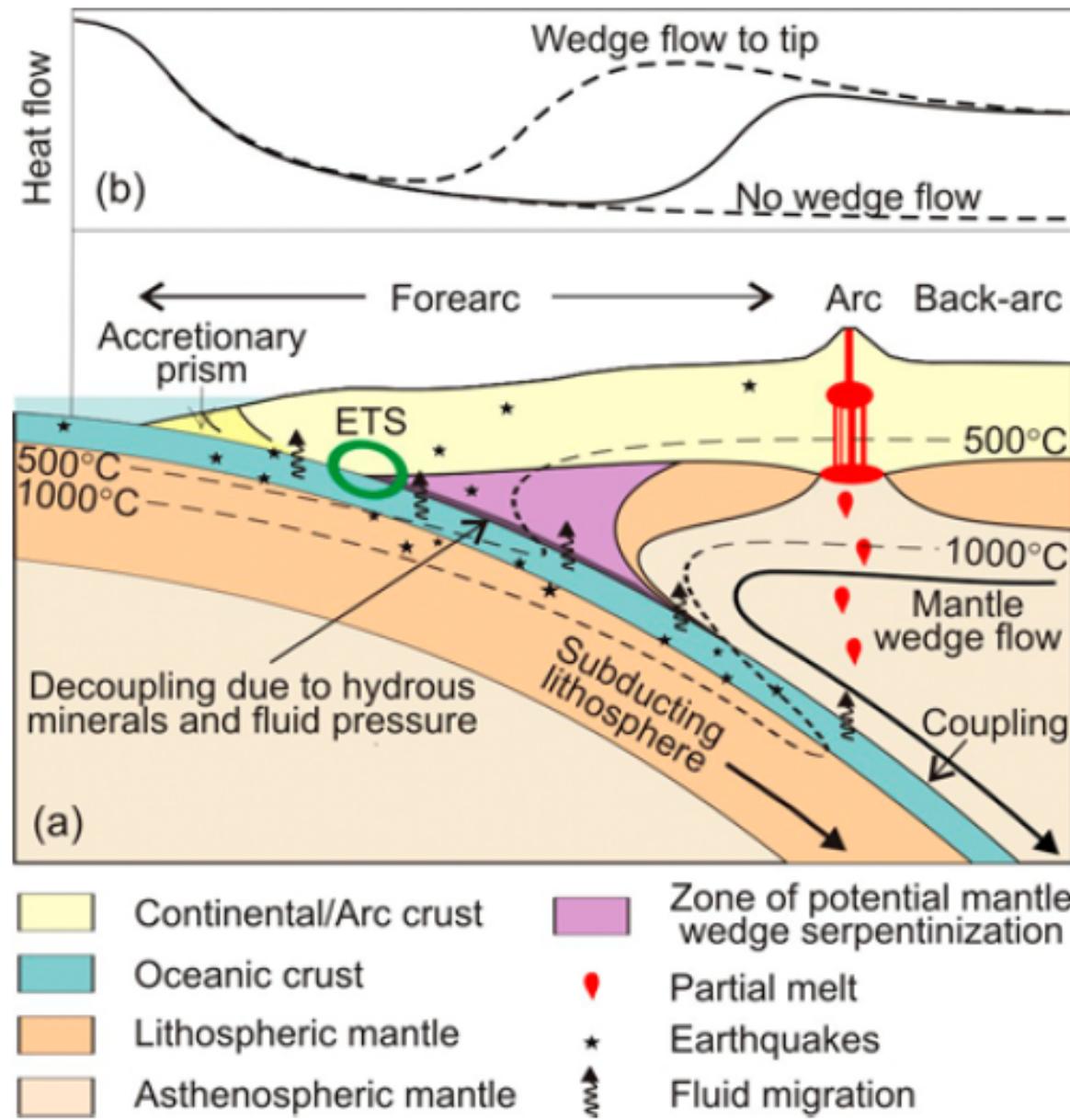


**Figure 7** A comparison of slab thermal structures from a 50-Myr-old,  $45^\circ$  dipping slab descending at  $5 \text{ cm yr}^{-1}$  with kinematic slab approximations (left) (Minear and Toksöz, (1970)) and (right) the analytic corner flow solution for flow and ConMan's temperature solver. Below 50 km depth, the Minear and Toksöz slab is colder than the corner flow plus ConMan solution.

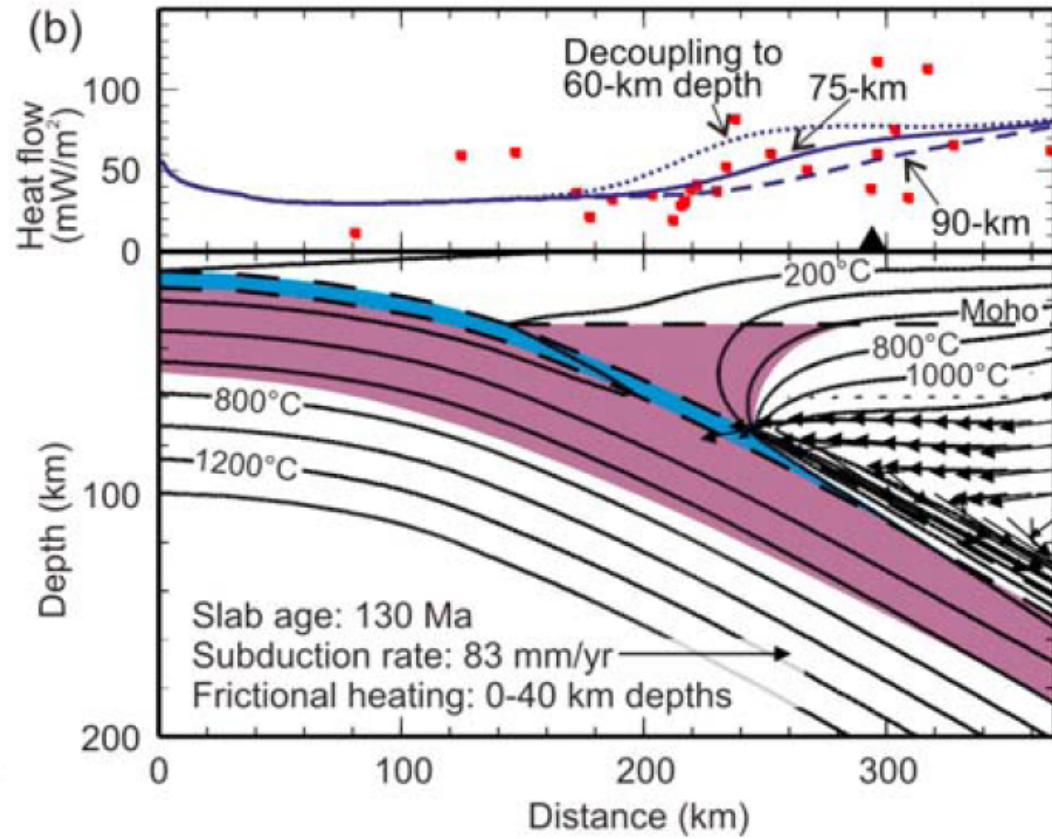
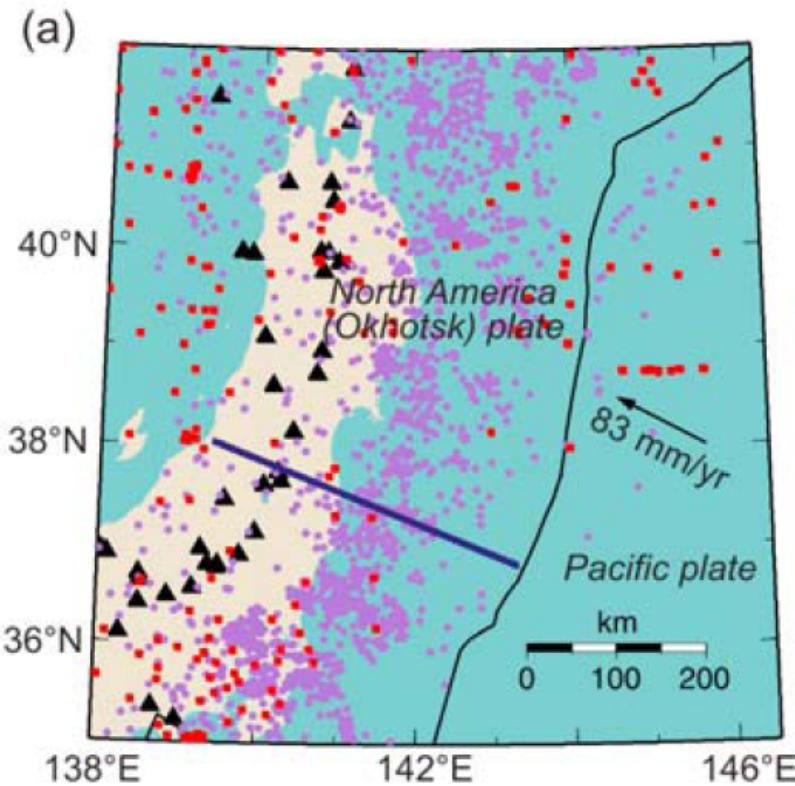


**Figure 9** Thermal structure from two slab calculations using ConMan (King *et al.*, 1990). Both calculations have a slab descending at  $45^\circ$  at a fixed velocity of  $5 \text{ cm yr}^{-1}$ . The incoming plate material is 50 My old. The left image is a constant-viscosity mantle wedge and the right image is a temperature-dependent viscosity wedge, with an activation energy of  $335 \text{ kJ mol}^{-1}$ .

# Heatflow



# Constraints on decoupling zone



Wada and Wang, G3, 2009

# Water flux

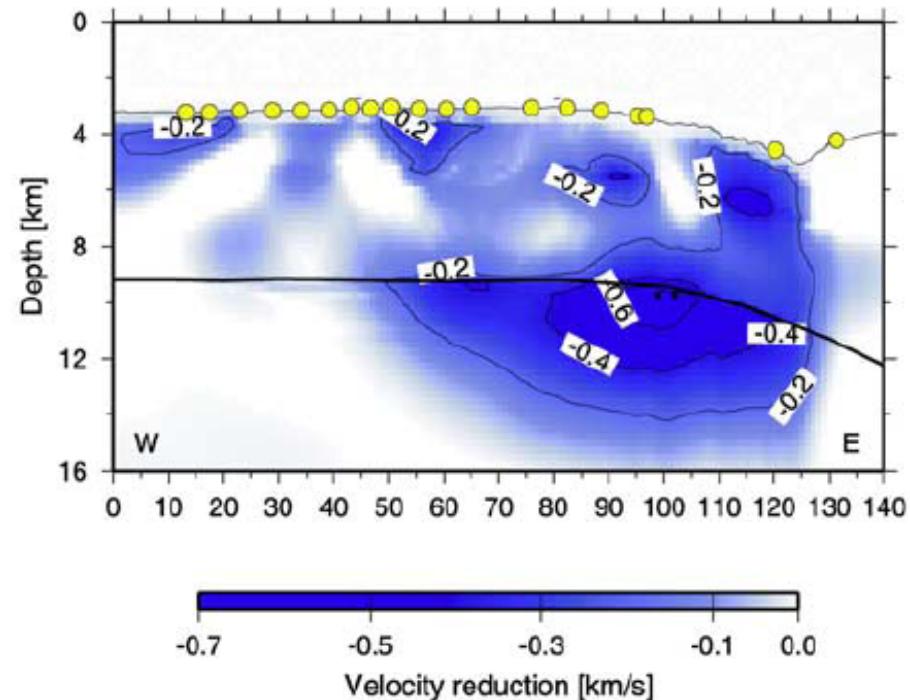
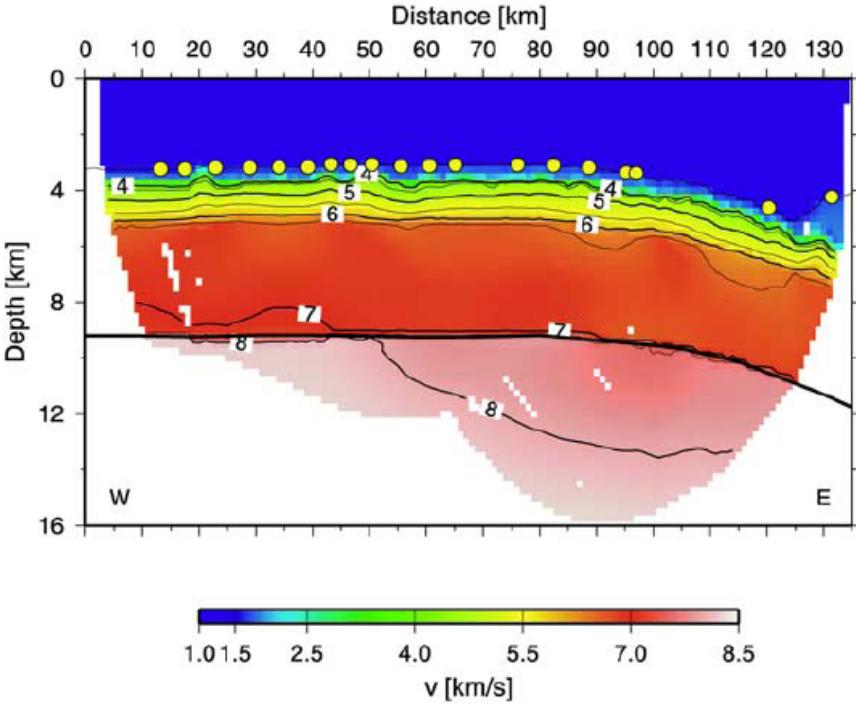
Water distribution in incoming slab

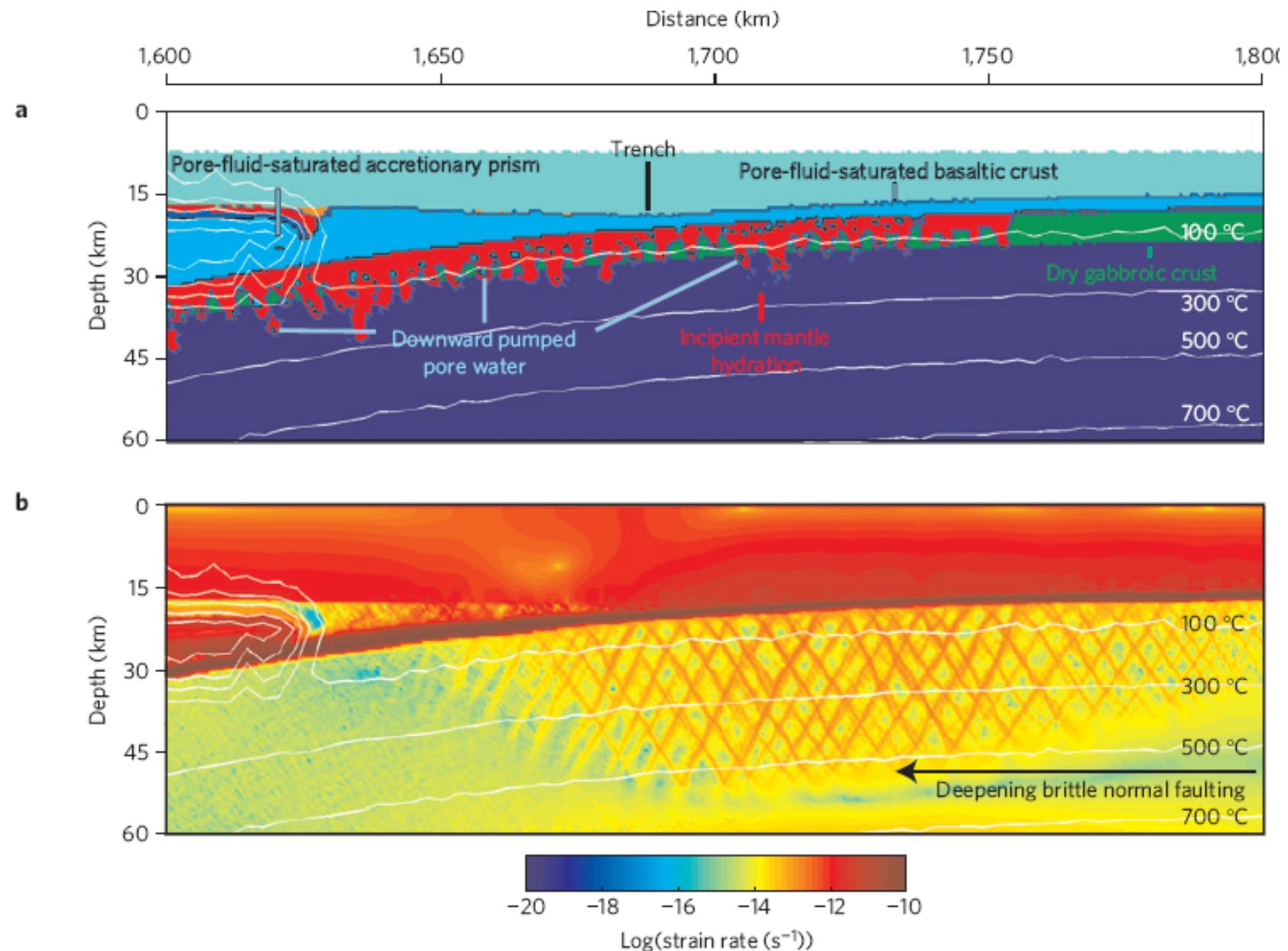
Compacted sediments: 0.4-5 wt%

Upper crust: few wt%

Serpentinite in upper mantle: up to 2 wt%

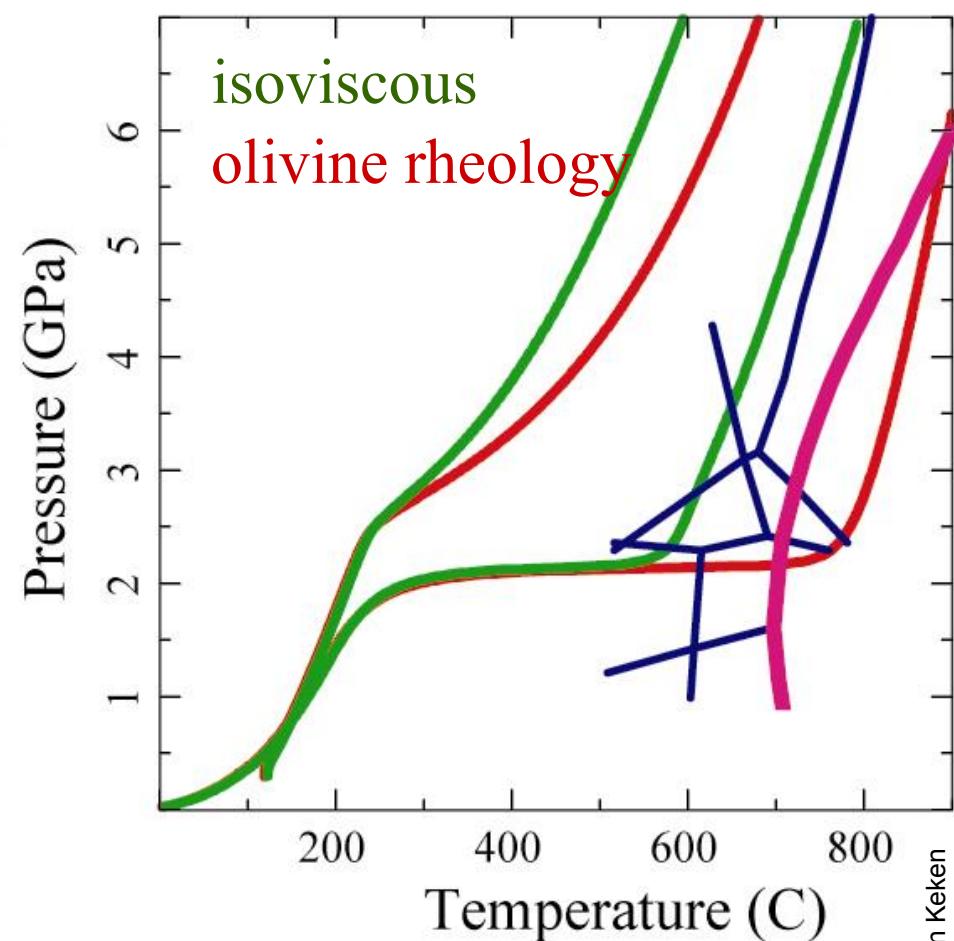
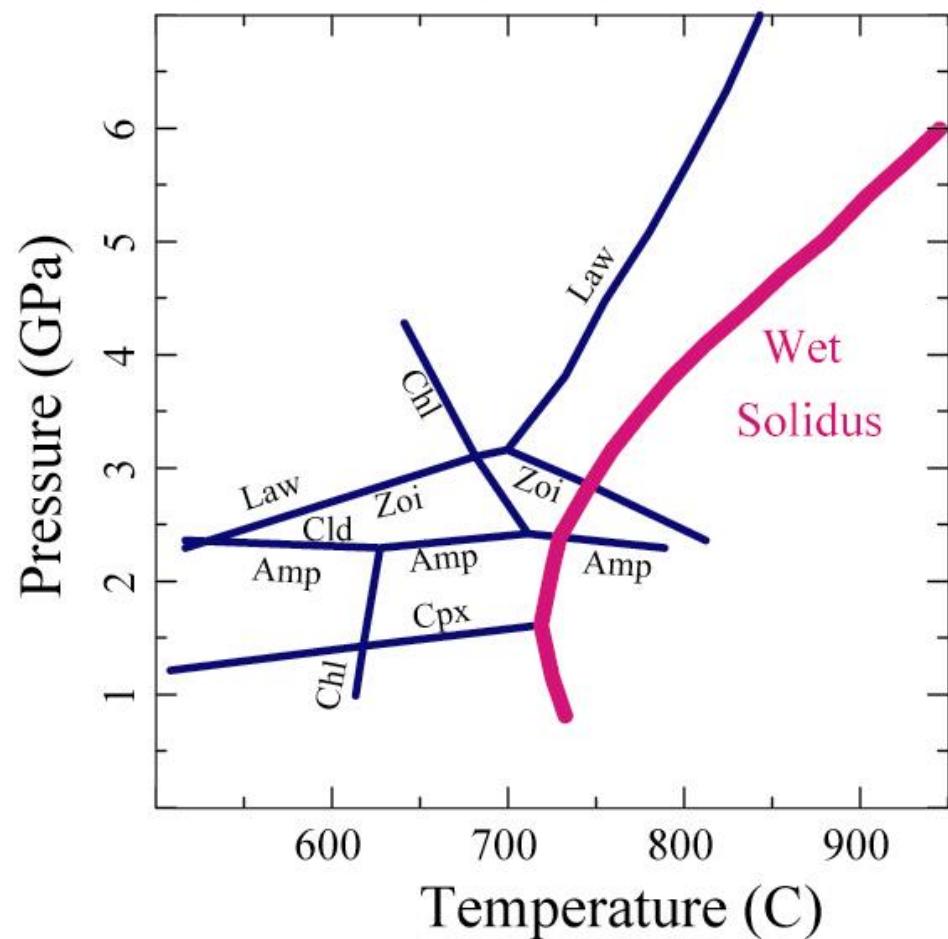
Slab structure outboard of trench at Nicaragua (Ivandic et al., 2008)





# Temperature in subducted oceanic crust

Water saturated basalt



Van Keken et al., G<sup>3</sup>, 2002: model for Honshu

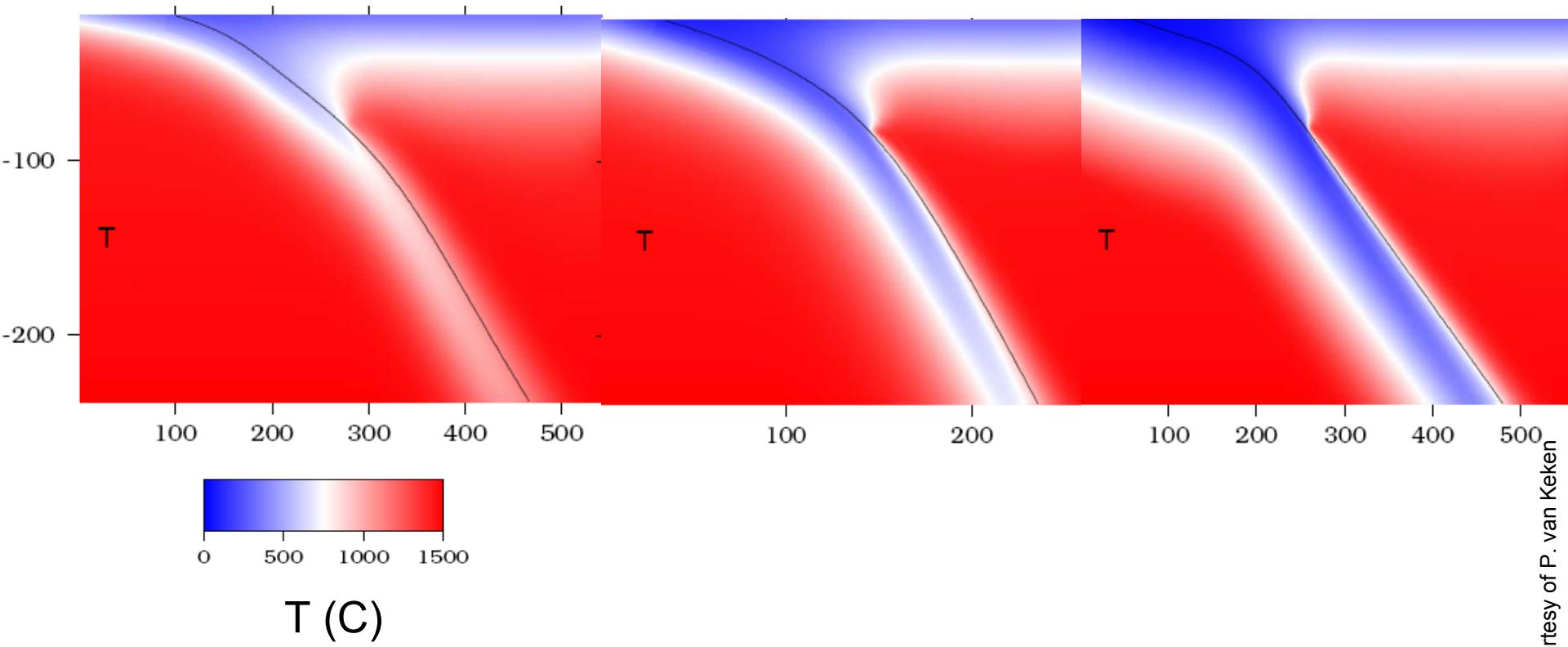
See also: Kelemen et al., 2003; Conder et al., 2003; Wada and Wang, 2008

Update to Hacker, Gcubed, 2008  
with full thermal models from Syracuse et al. (2010)

Cascadia

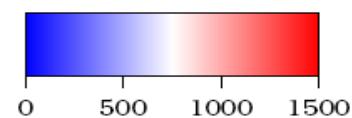
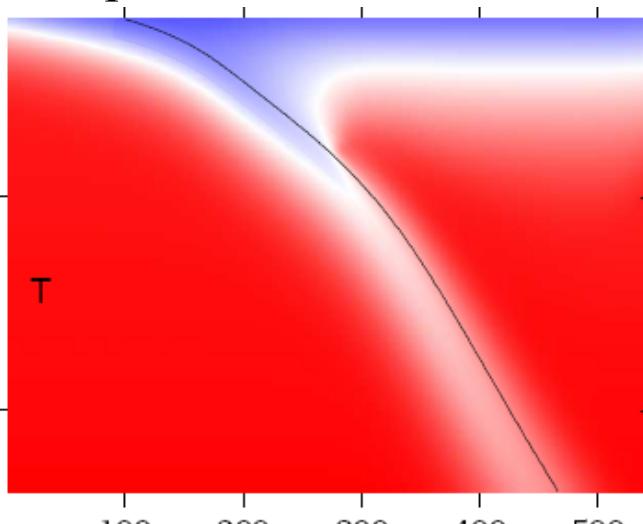
Nicaragua

Tohoku

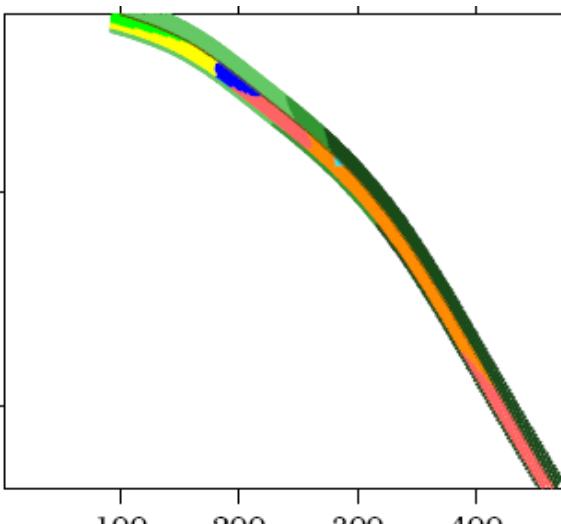


Cascadia

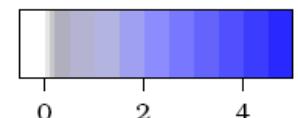
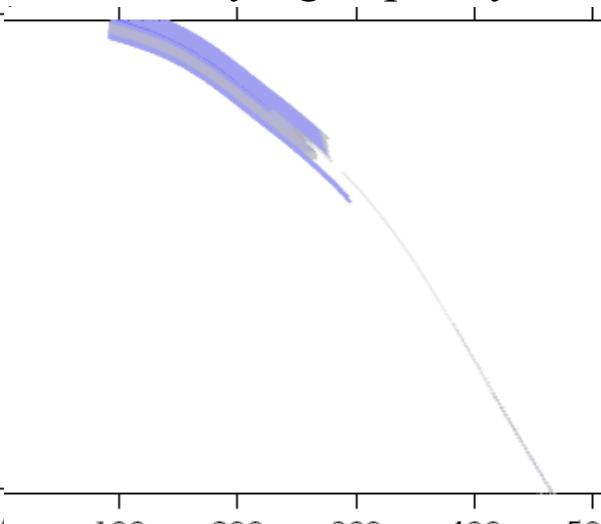
temperature



rock facies

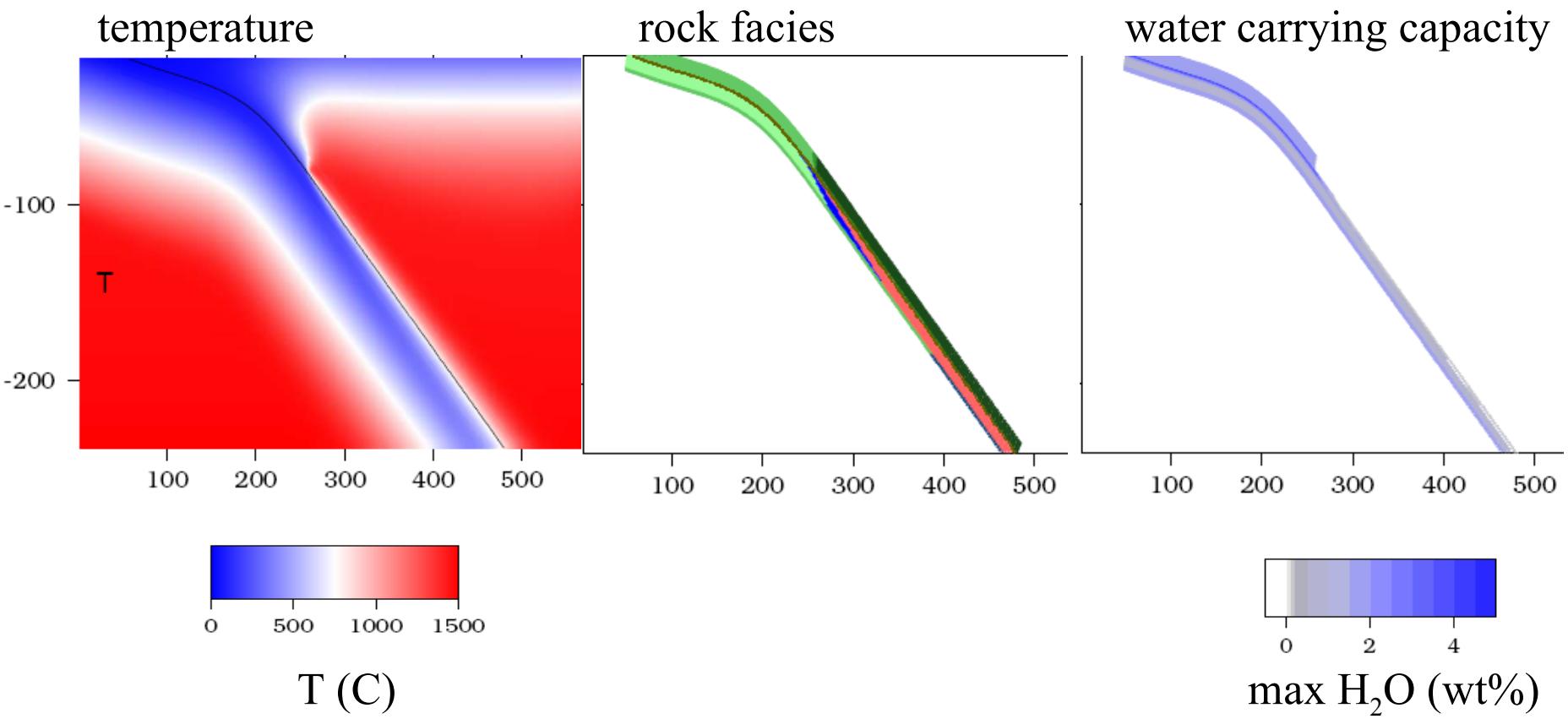


water carrying capacity



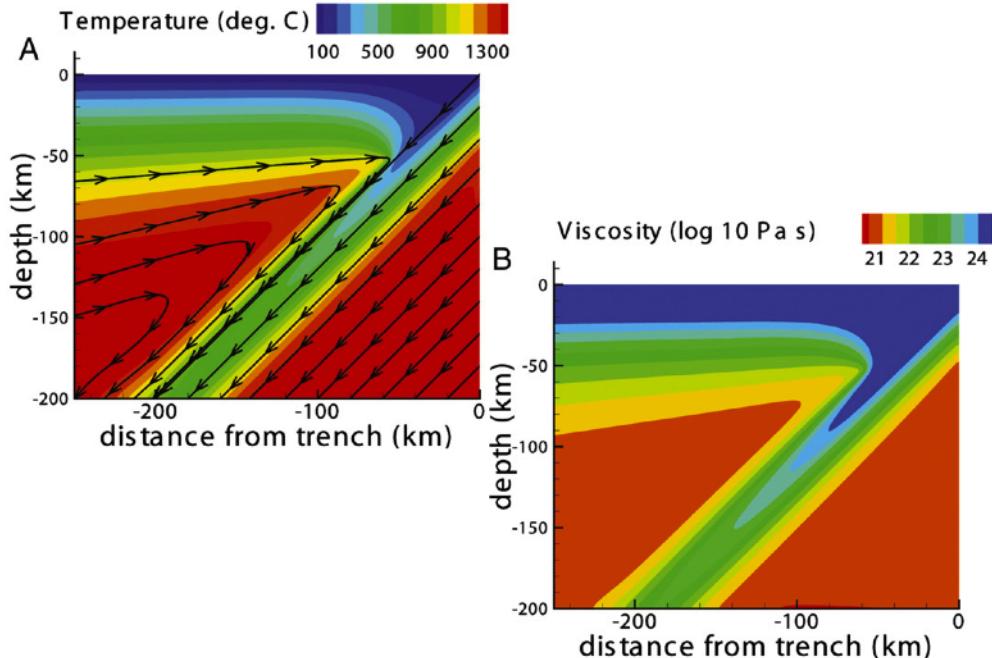
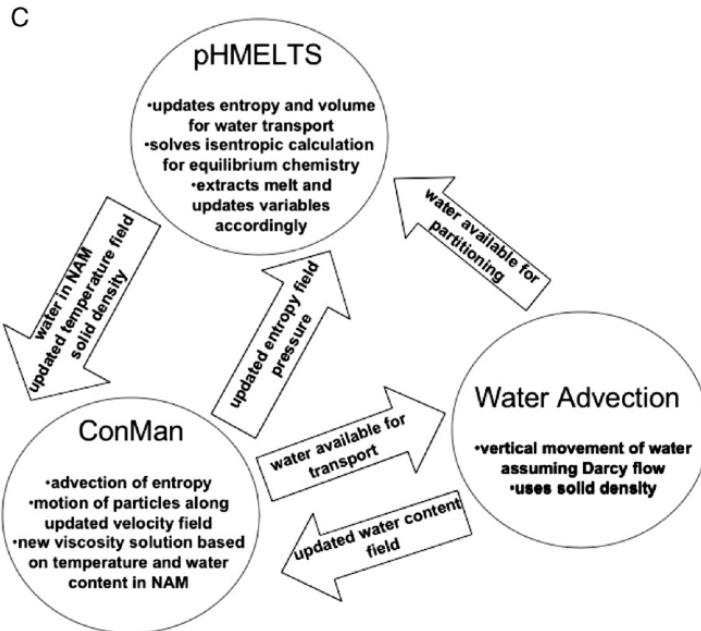
Syracuse et al. (2010)

Tohoku



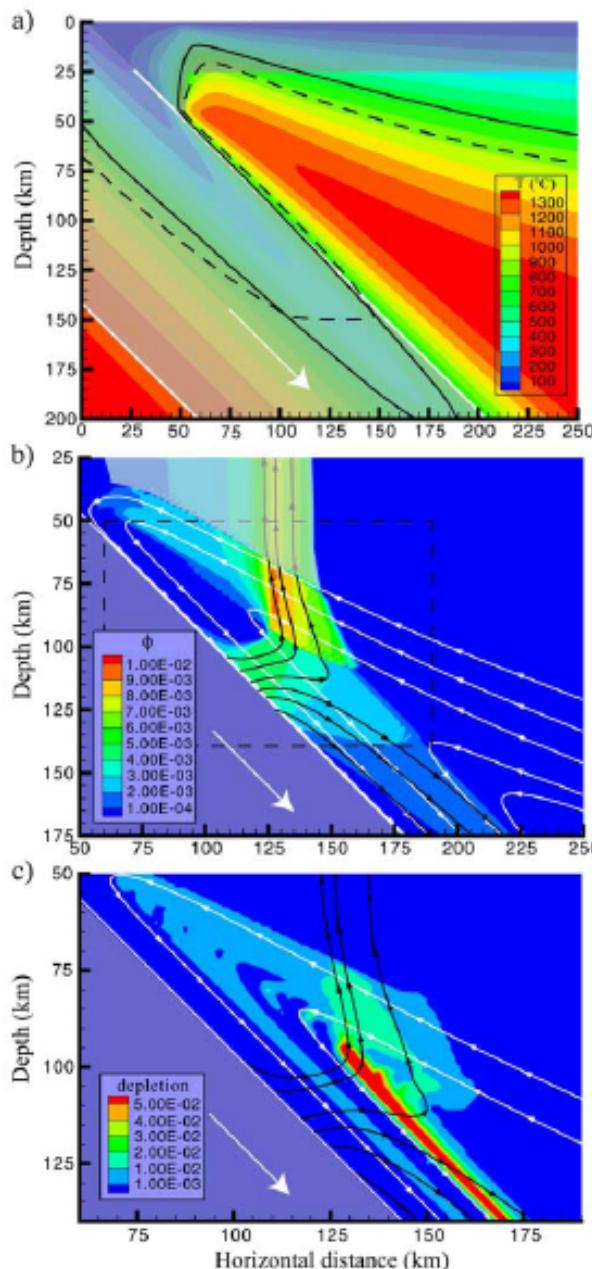
Syracuse et al. (2010)

# Coupled Solid-Fluid-Min.

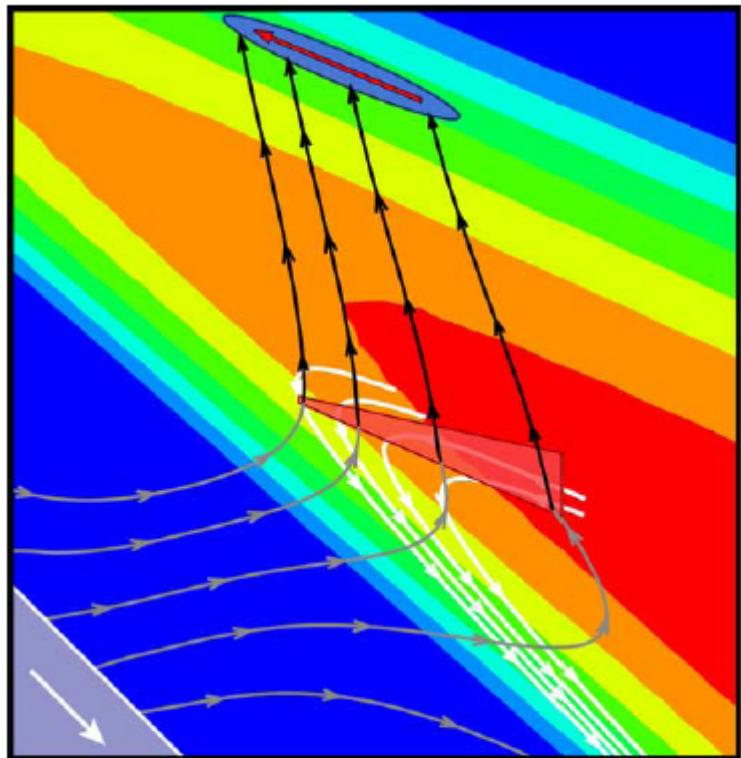


Hebert et al. (2009)

- Composition evolves including fluid & melt content.
  - Affects density ( $T$ ,  $X$ ) & rheology.
- Fluids move according to Darcy flow

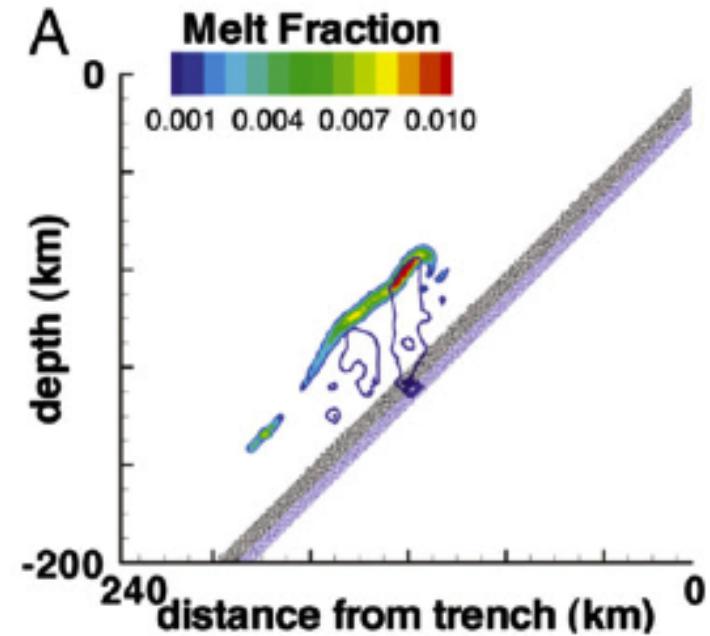
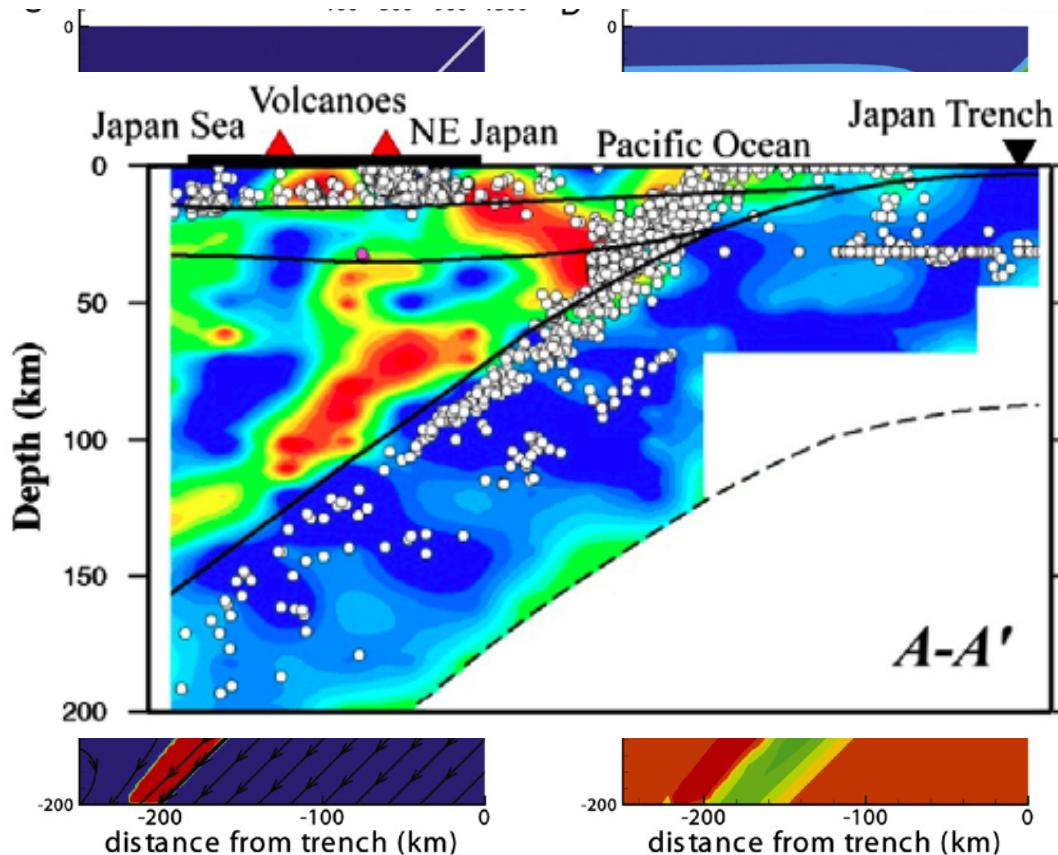


Cagnioncle et al. (2007)



**Figure 9.** Schematic diagram of fluid migration at subduction zones. Hydrous fluids (grey streamlines) are released from the slab by dehydration reactions and rise buoyantly into the wedge. Fluids do not rise vertically into the wedge but are influenced by solid flow. A melting front (pale red triangle) develops where the water which was not advected to greater depth reaches a region hot enough to melt. The fluid is then a mixture of dissolved oxides and a hydrous component (black streamlines). The large fluid fraction after melting front prevents solid flow from affecting fluid migration, and fluids migrate vertically to the surface until they reach colder temperatures (pale blue ellipse). The present study does not explicitly treat the final fate of melt, but a potential melt transport mechanism, shown by the red arrow, is discussed in the text.

# Fluids Affect Solid Flow.



Hebert et al. (2009)

- **Form low viscosity channel above slab.**
- **Spatially & temporally variable melt fraction.**
  - Limits region of water effect on rheology.

# **Semi-dynamic models**

King (2001)

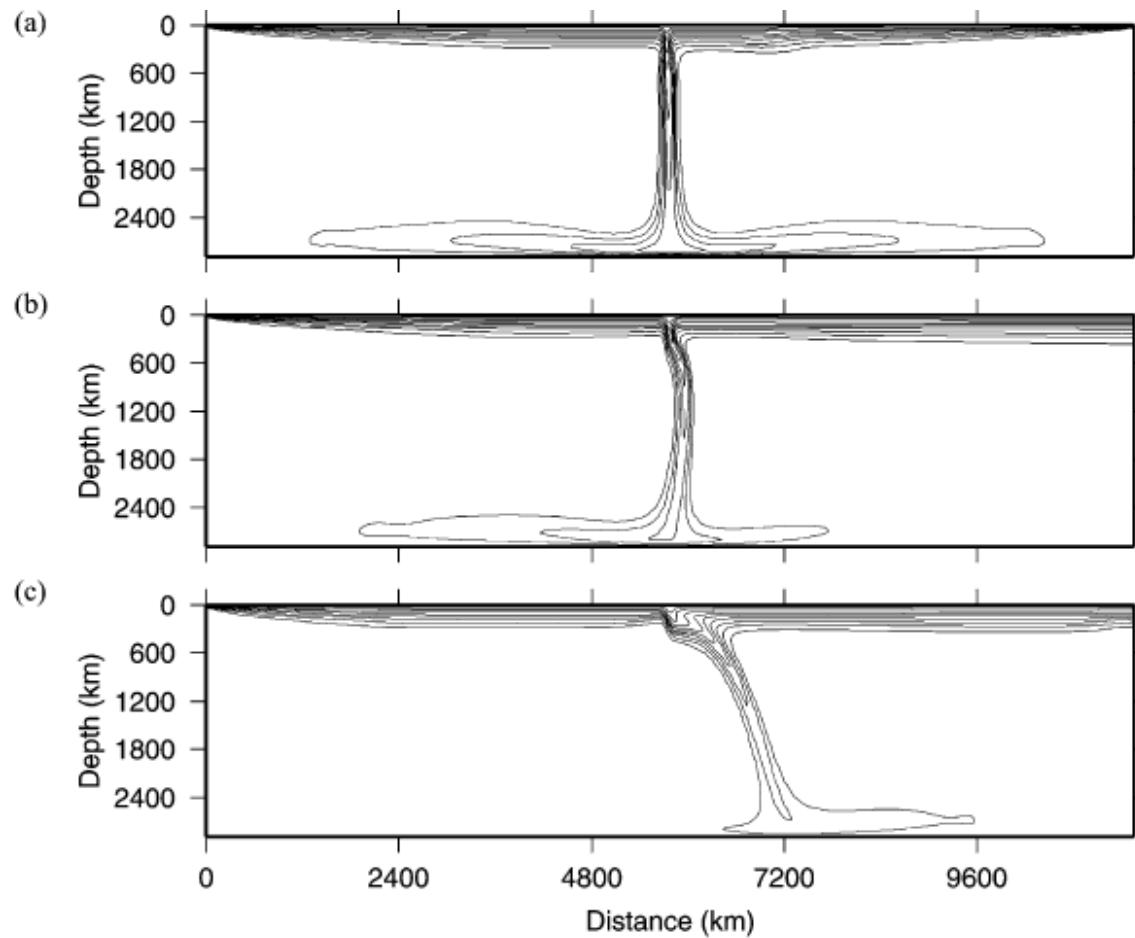
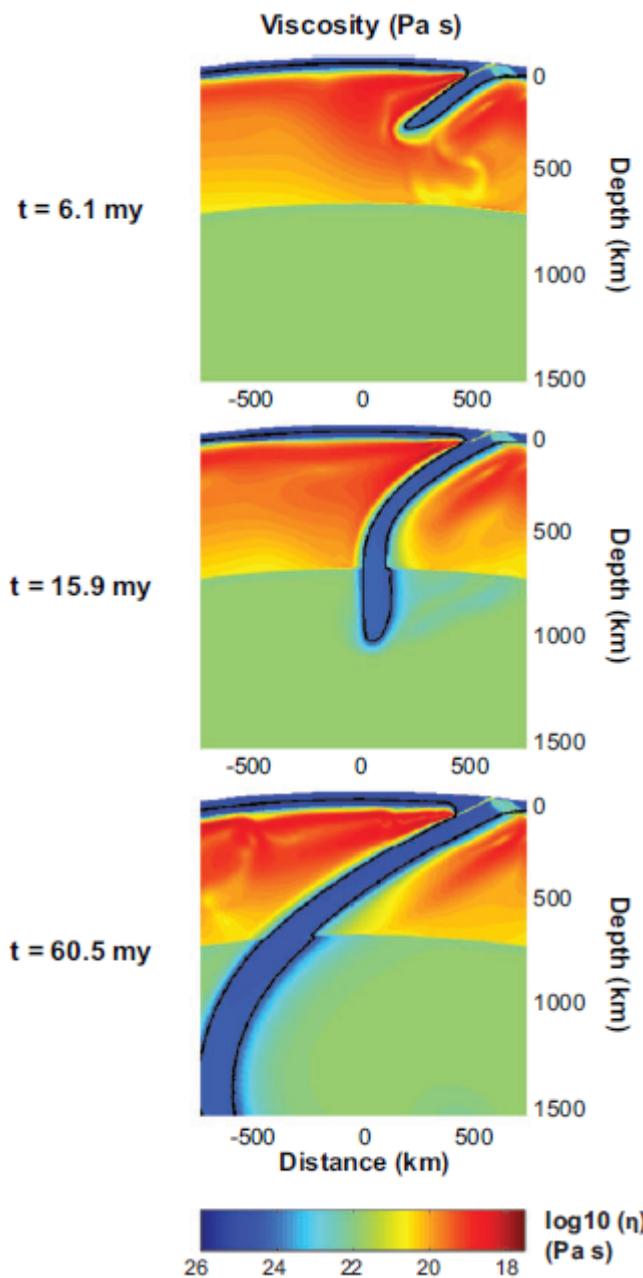
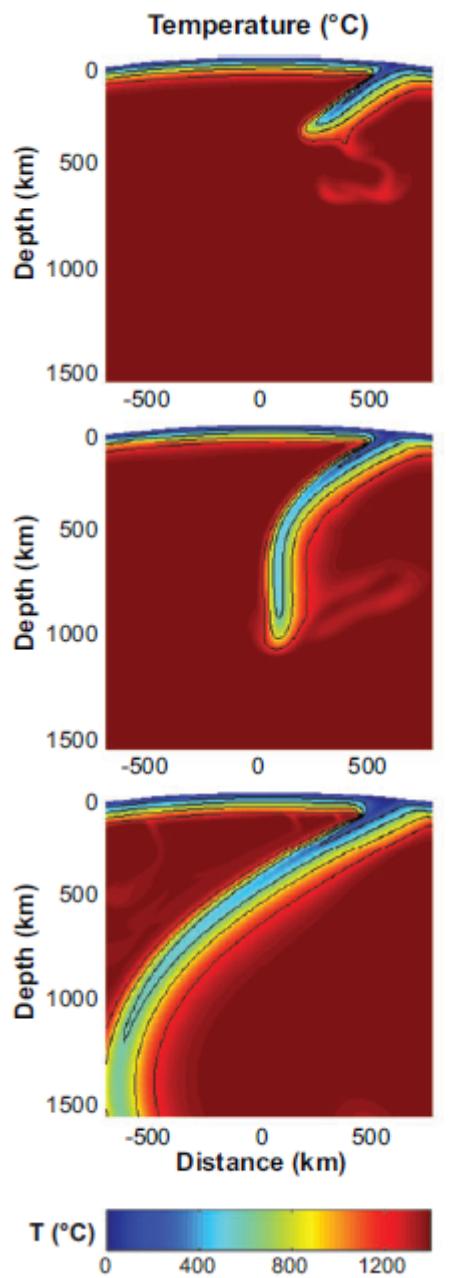
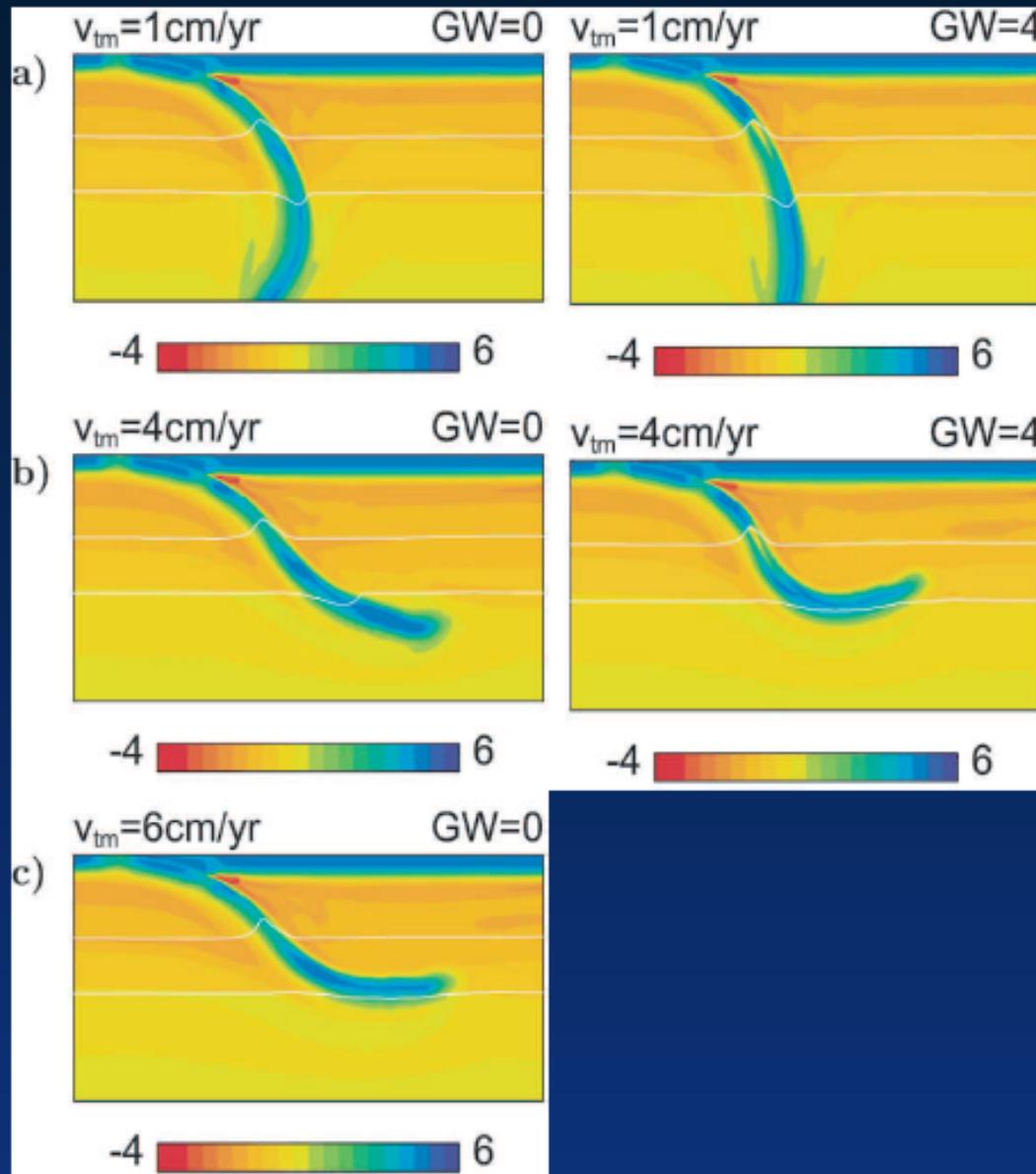


Fig. 1. Thermal fields from two convection calculations with plates. In both calculations the Rayleigh number is  $10^6$ , the top and bottom are isothermal free-slip boundaries, the fluid is internally heated, and the viscosity is temperature dependent. The initial temperature field has a square root of age plate thermal field on the left side of the box and a uniform boundary layer on the right side of the box. Weak material zones allow the plate to deform at the trench and the ridge. The 'ridge' is in the left corner of the box and the 'trench' is in the center of the box. Further details on this type of calculation can be found in Chen and King (1998). (a) The side velocity boundary conditions are free-slip (material is free to move vertically along the edge). (b) Identical to (a) except that the velocity of a single node on the right-hand side is set to zero, breaking the symmetry of the top boundary layer velocities. (c) Identical to (b) except that the side velocity boundary conditions are an imposed horizontal velocity of 20 mm per year. This is identical to moving the trench and plate relative to the center of mass of the mantle.



Billen (2009)

# Grain size weakening at 410



⇒  $v_{trench}$  and GW varied à la van Hunen *et al.* (2002)

⇒ strong slabs penetrate (Davies, 1995)

⇒ GW could explain weak, bent slabs (*c.f.* Karato *et al.*, 2001)

⇒ alternatives: faults,  $\eta_y$

Čížková *et al.* (2002)

# Rollback and ponding

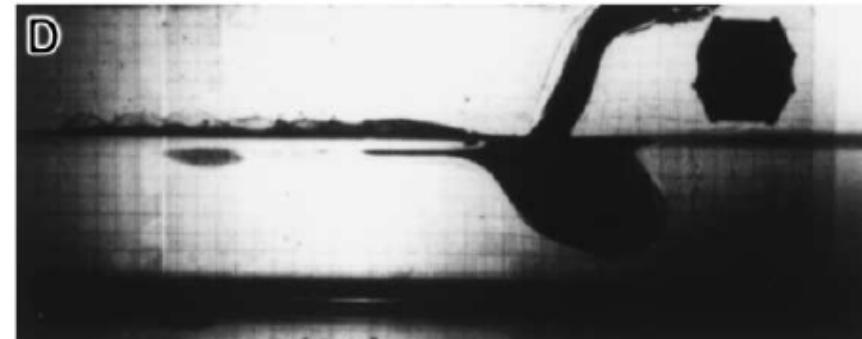
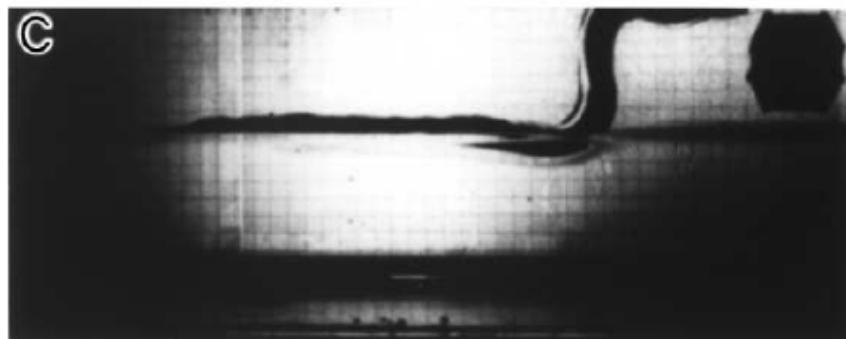
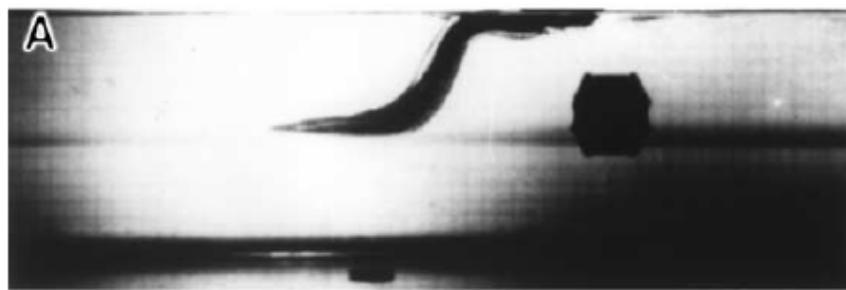
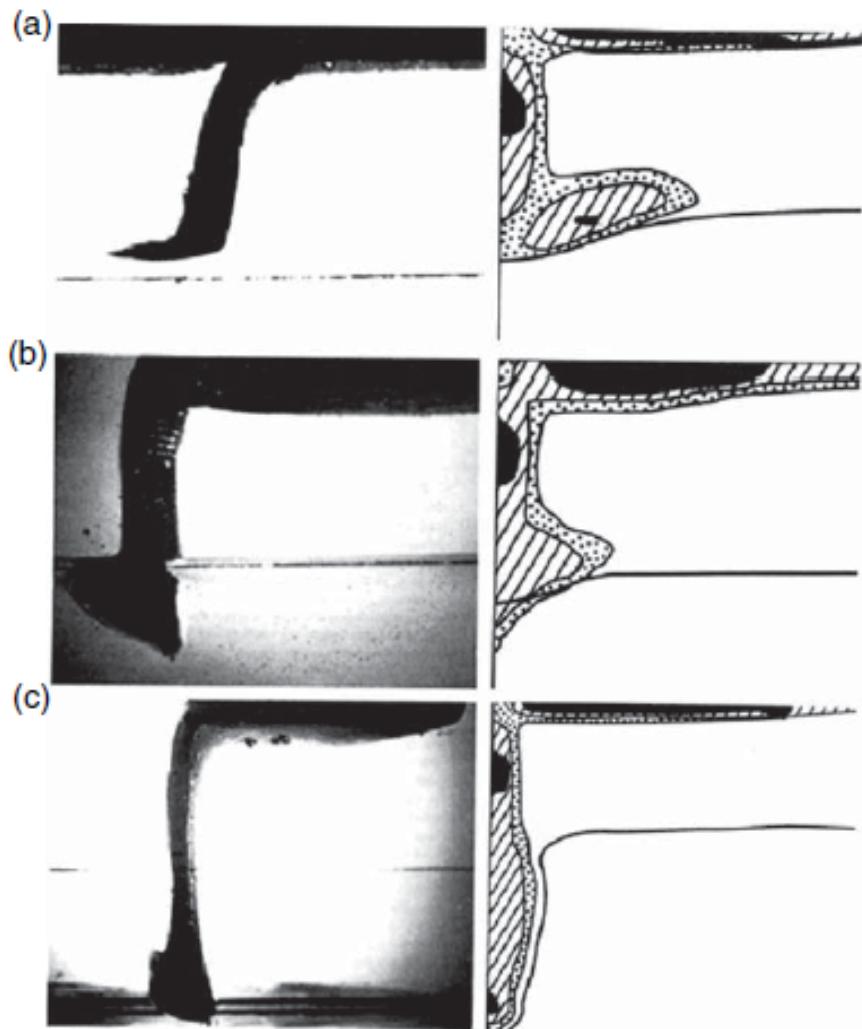
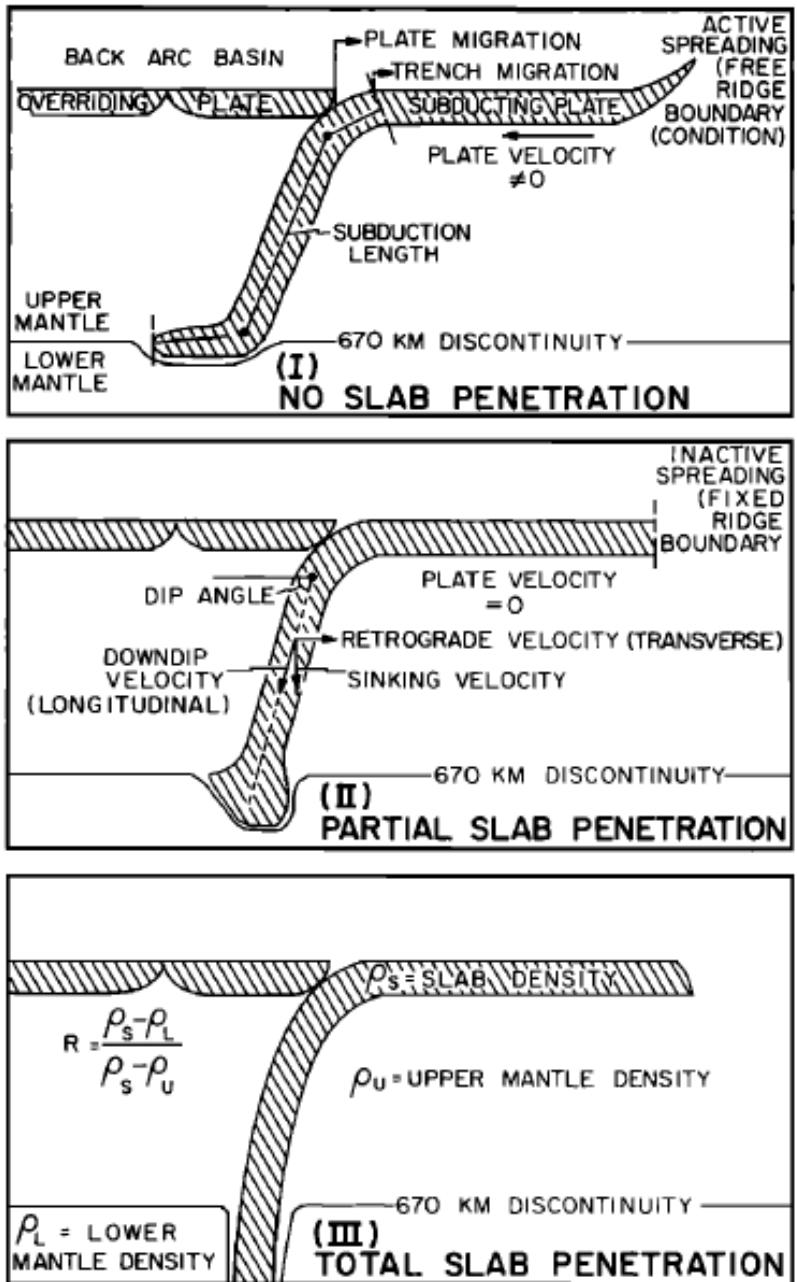
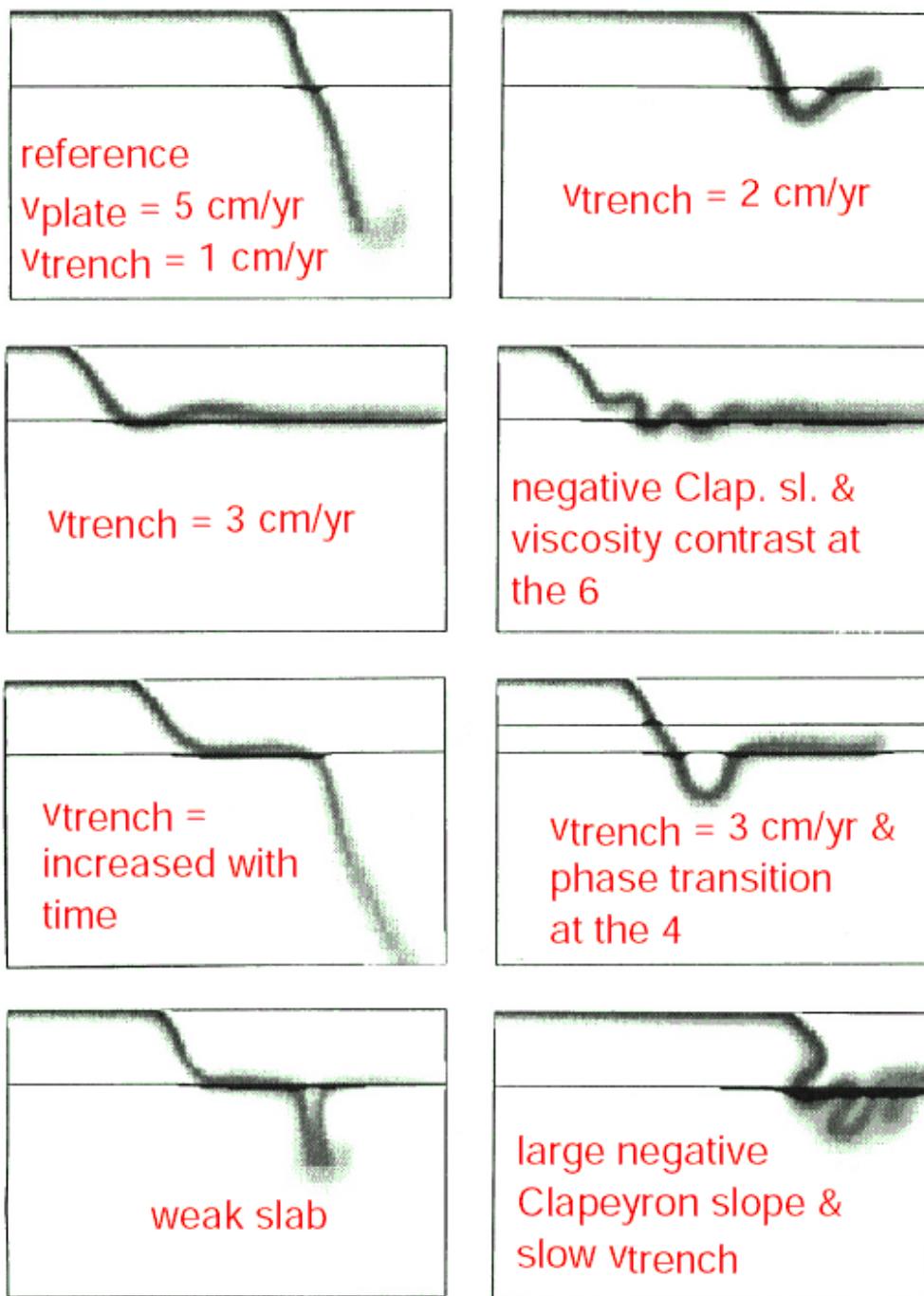


Fig. 1. Snapshots from a laboratory experiment by Guillou-Frottier et al. (1995). A sheet of chilled and dyed corn syrup is extruded into a tank with two layers of syrup. Initial rapid trench migration leads to a flat slab. After (B), trench-rollback is stopped and slab material accumulates in a pile that sinks into the lower layer. The whole sequence corresponds to approximately 400 million years of subduction.

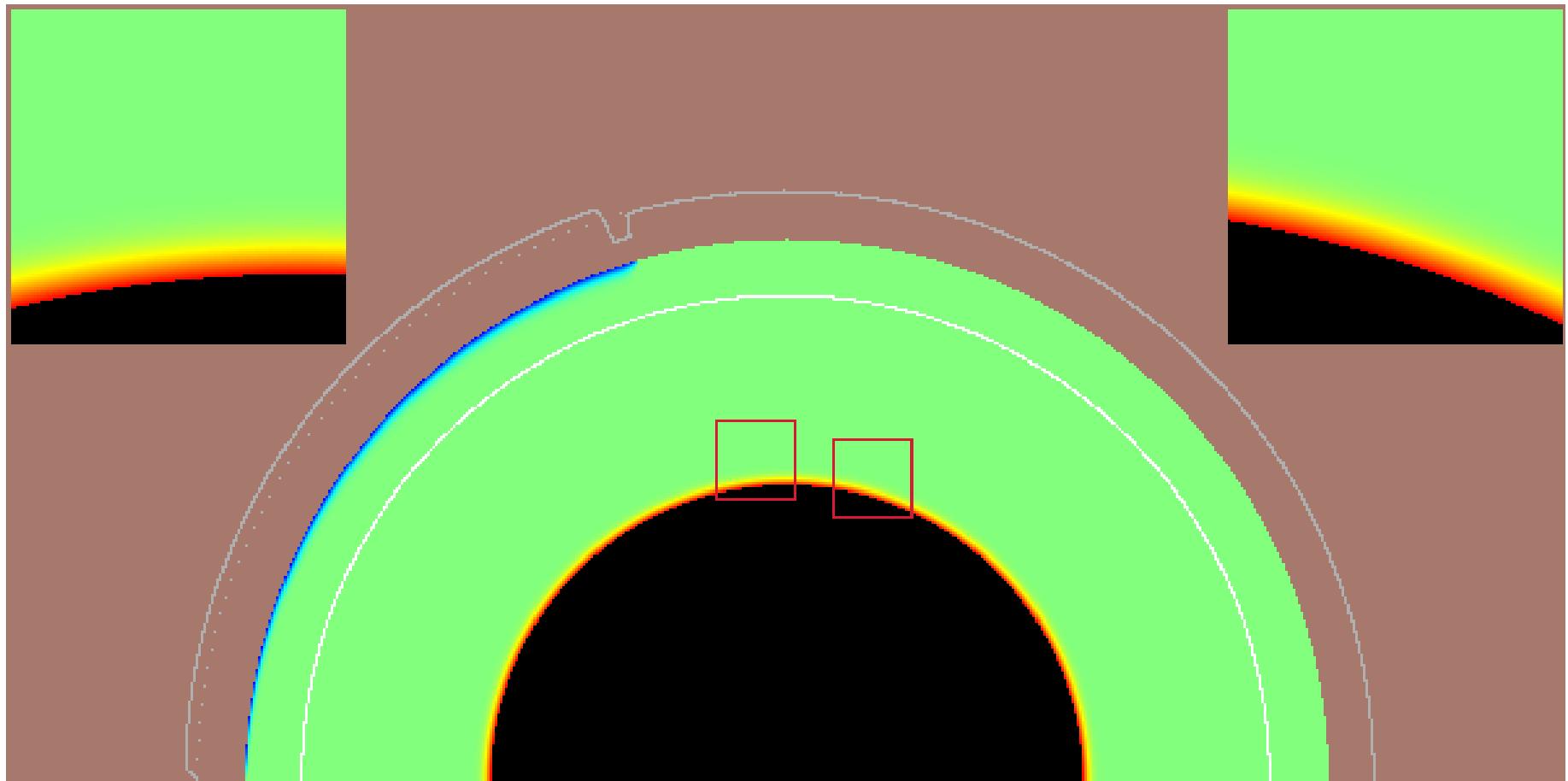


**Figure 14** Experimentally observed styles of slab penetration through a density discontinuity (left) compared with 2-D calculation by Christensen and Yuen (1984) (right). (a) Slab deflection with  $R \approx -0.2$ . (b) Partial slab penetration with  $R \approx 0.0$ . (c) Complete slab penetration with  $R \approx 0.5$ . Reproduced from Kincaid C and Olson PL (1987). An experimental study of subduction and slab migration. *Journal of Geophysical Research* 92: 13832–13840, with permission from American Geophysical Union.



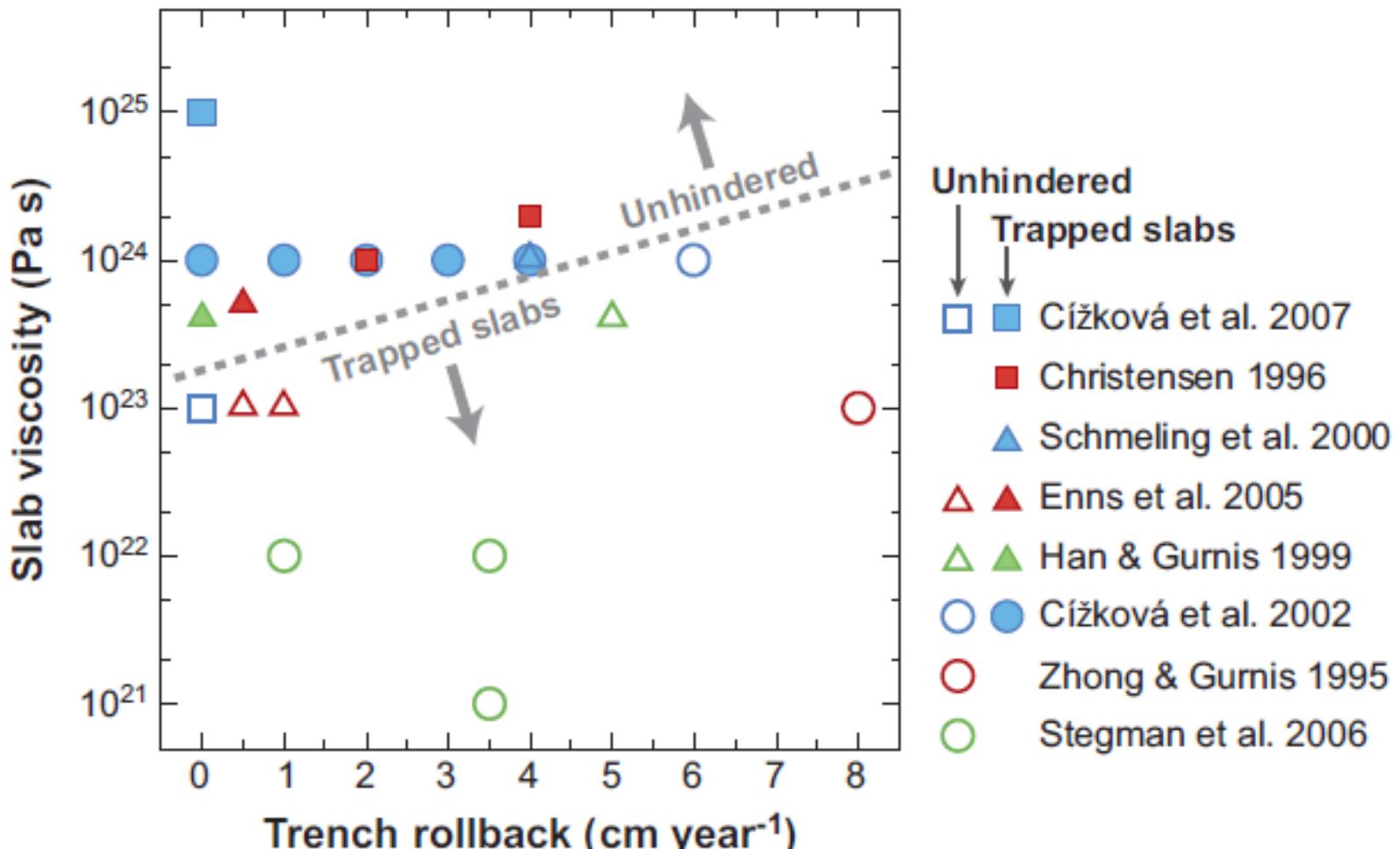
Christensen (1996)

# Effect of negative Clapeyron slope on slabs and plumes



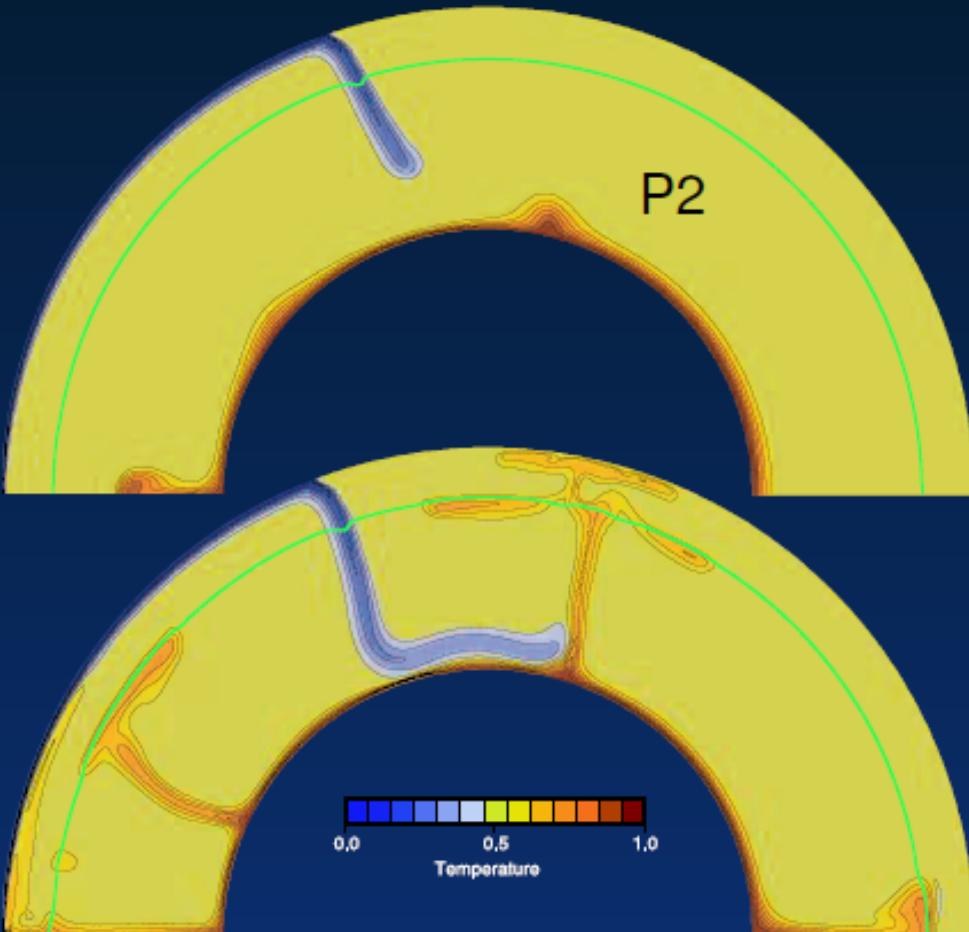
Tan et al. (2001)

# Ponding as f(strength, rollback)



Billen (2009),  
cf. Davies (1998)

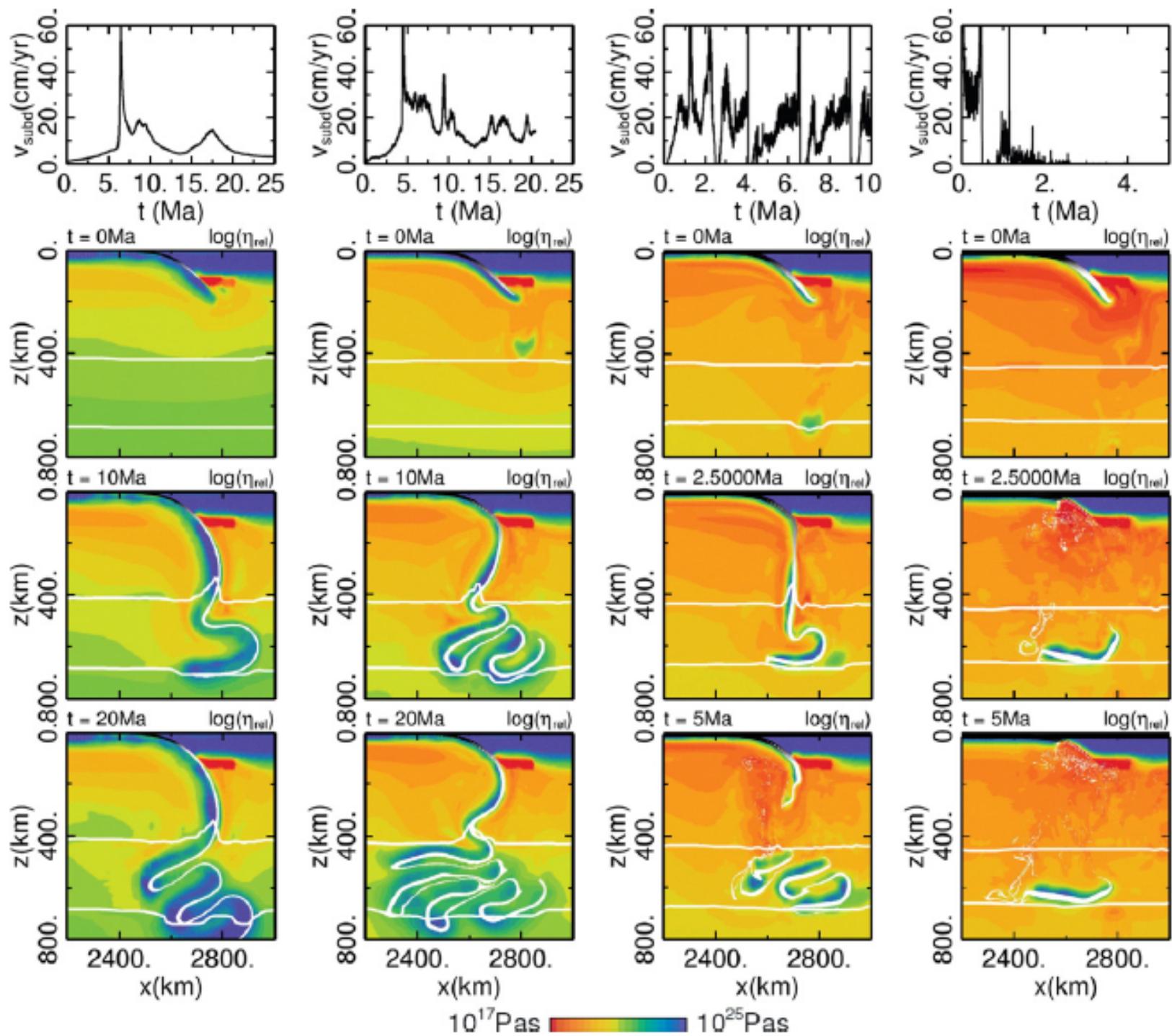
# Do slabs make it all the way to the CMB?



Yep.

- ⇒  $dp/dT| = -3 \text{ MPa/K}$  ✓
- ⇒ increase in  $\kappa$  with depth ✓
- ⇒ internal heating ✓
- ⇒ substantial ( $\sim 500 \text{ K}$ ) anomaly at CMB

Tan *et al.* (2002)



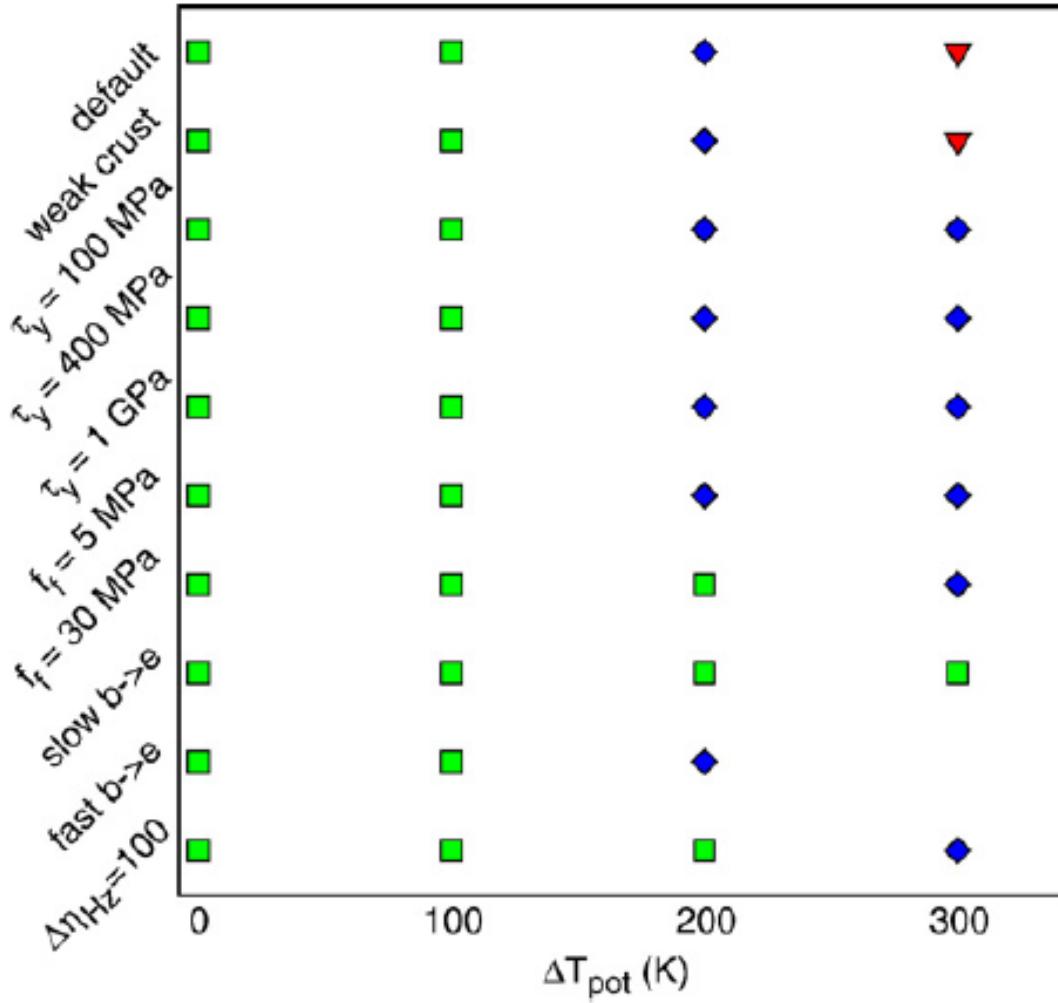
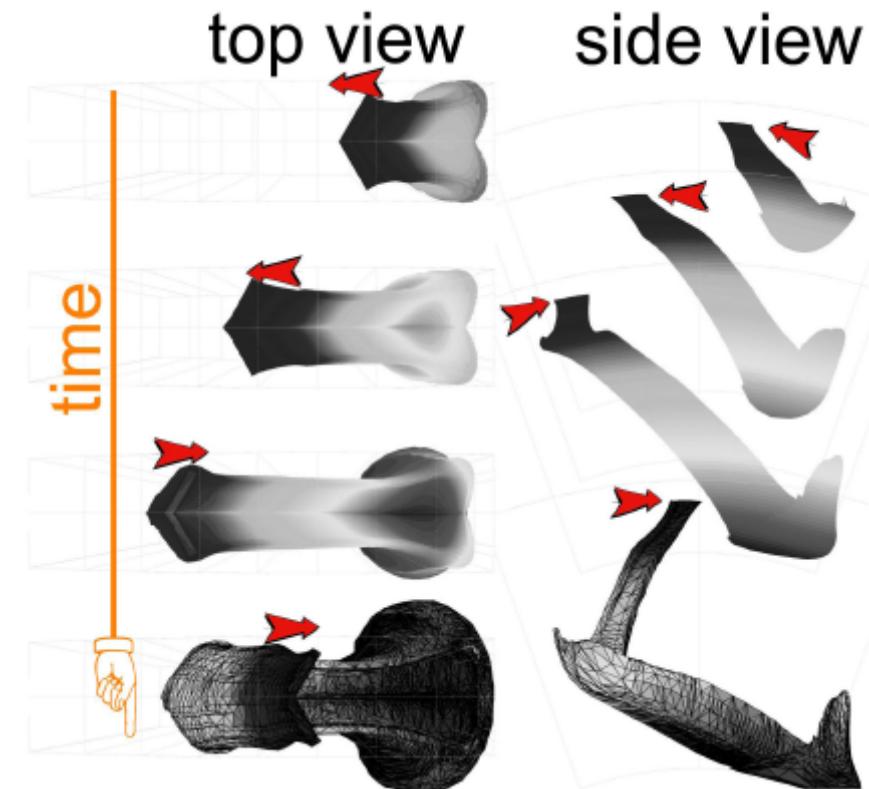
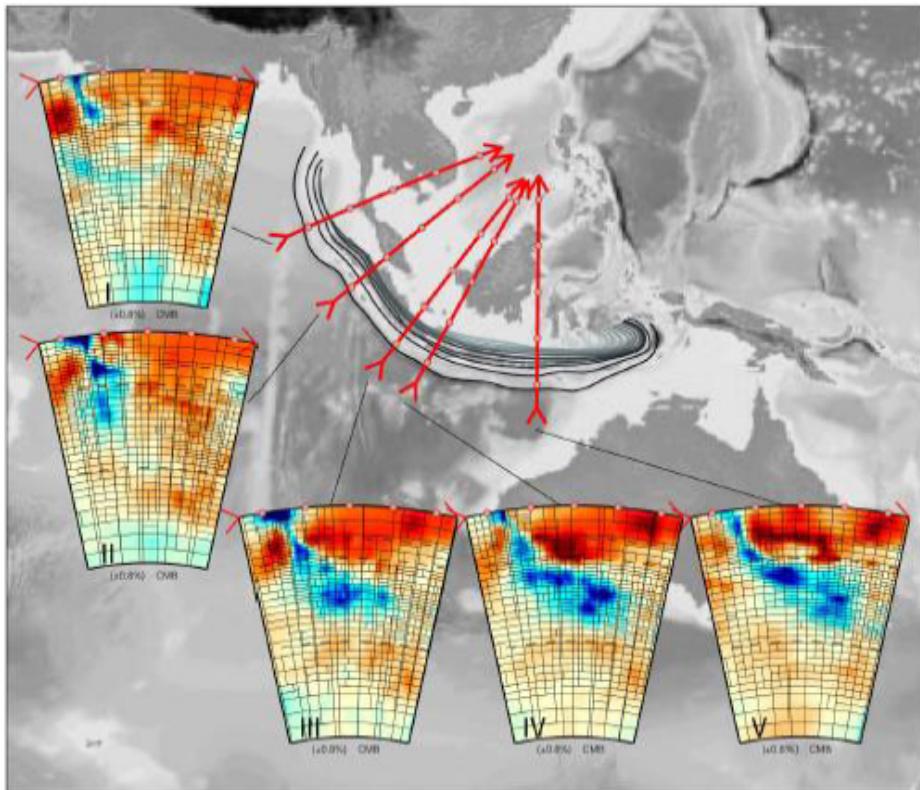


Fig. 10. Compilation of the subduction style of all presented calculations. Green blocks indicate a subduction style like at present. Blue diamond indicate frequent slab detachment events, and red triangles denote no continuing subduction.

# Tomographic slabs and Stokeslets for a moving trench scenario

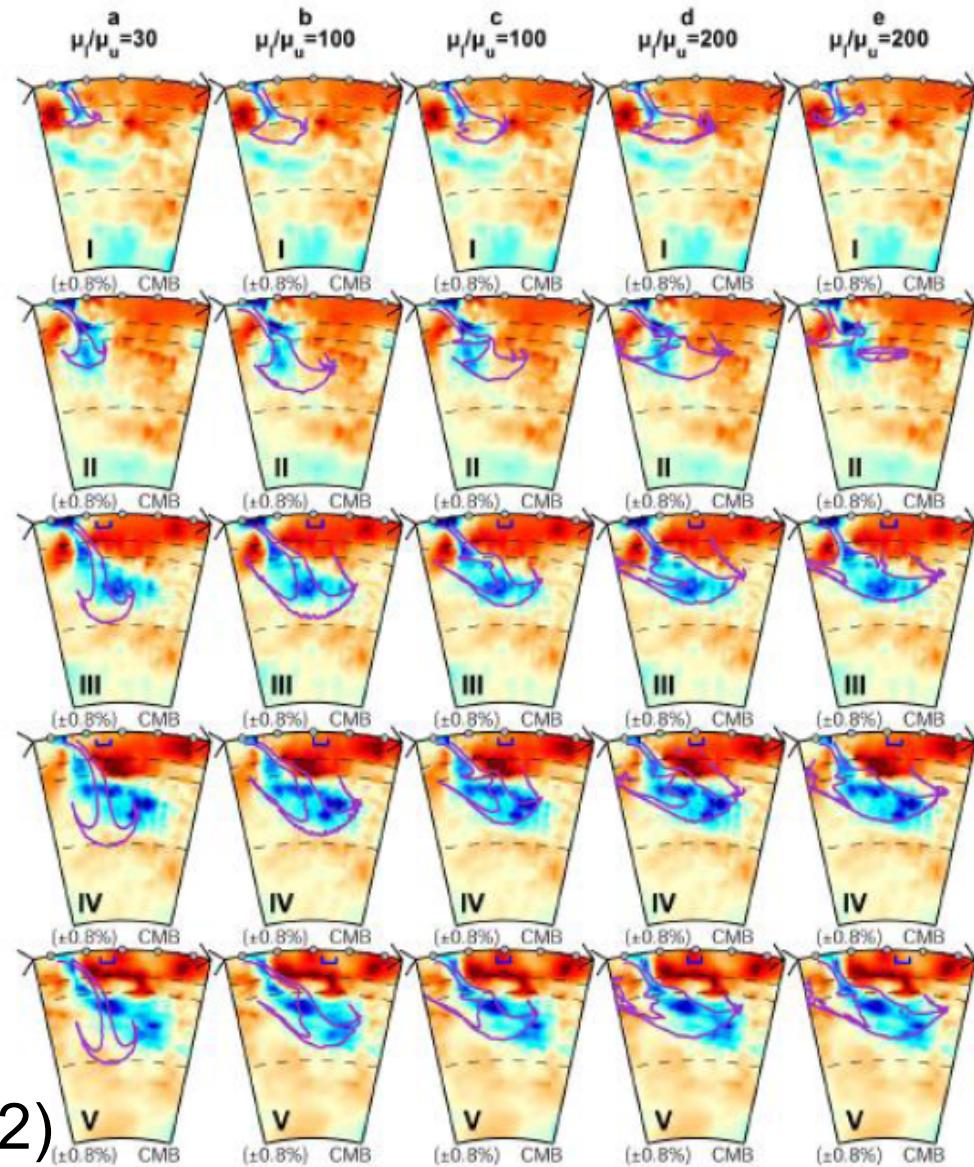


- Weak, fluid slab ( $\eta' = \eta_{\text{slab}}/\eta_{\text{mantle}} = 1$ ) hits the 660
- Prescribed trench motion

Karason (2002)

# Stokeslets and tomography

- Best fit for Sunda for a viscosity contrast between upper and lower mantle of  $> \sim 200$
- Strong anchoring of weak slab
- cf. slablets of Morra et al.



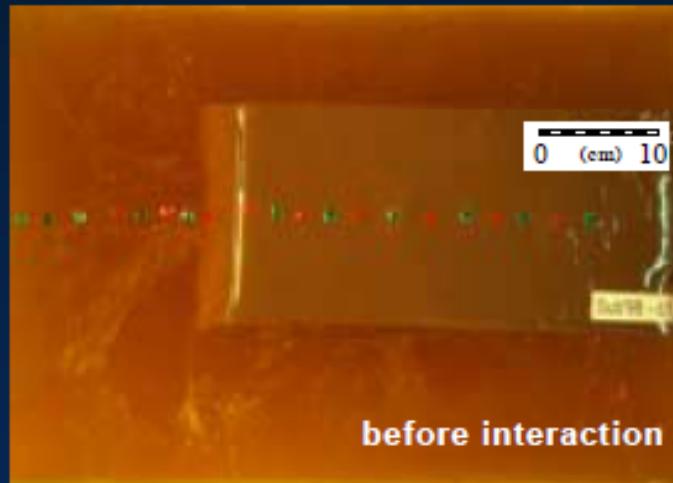
Karason (2002)

# 3D

# Interactions: rollback and episodicity in 3D

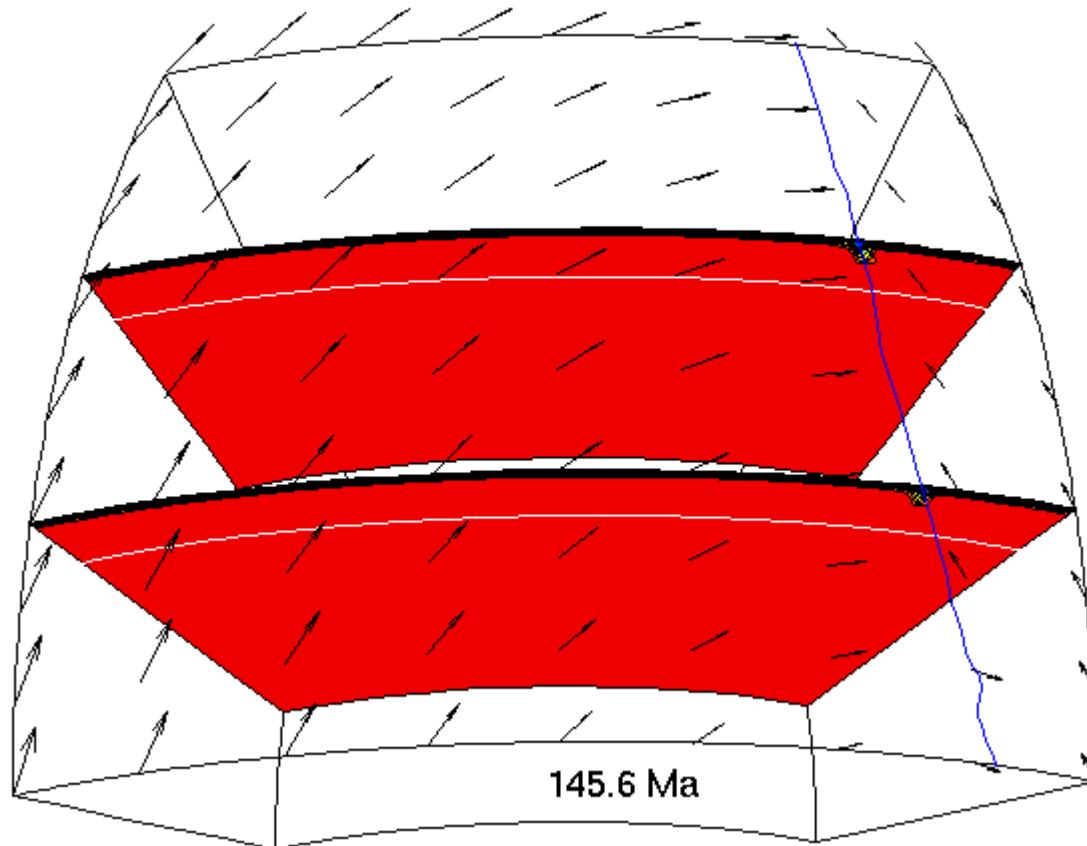
laterally unconfined

laterally confined



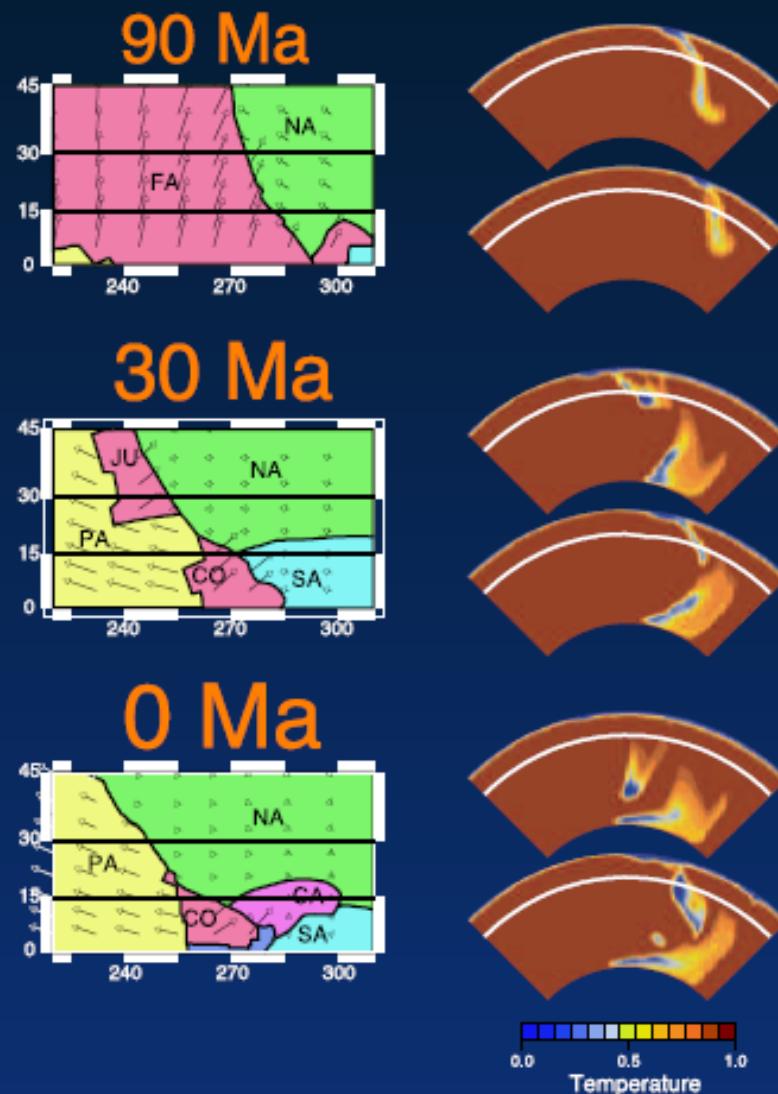
→ episodicity in case of lateral and vertical flow confinement

# Changes in plate motions



Tan and Gurnis (2002)

# What should slabs look like in tomography?



Complicated.

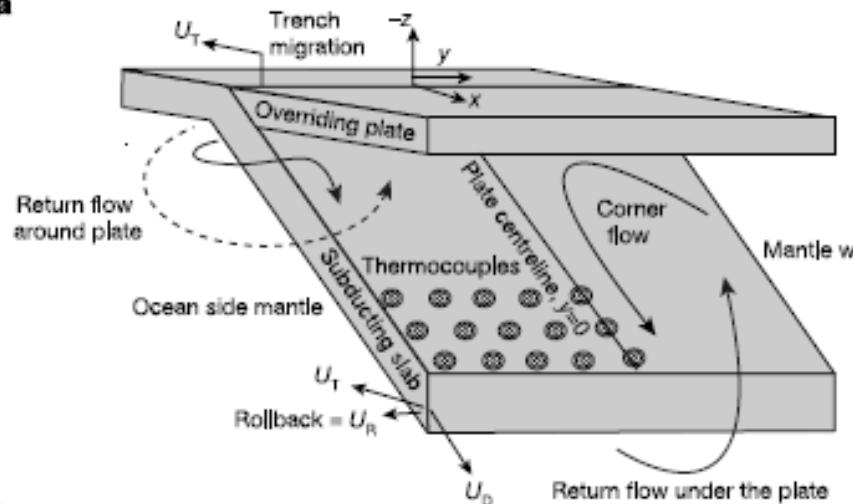
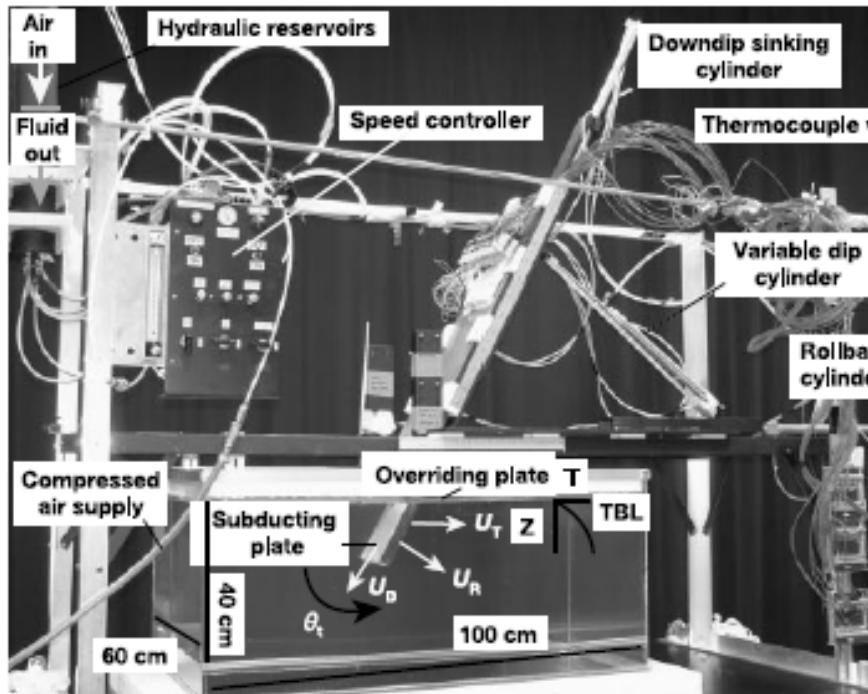
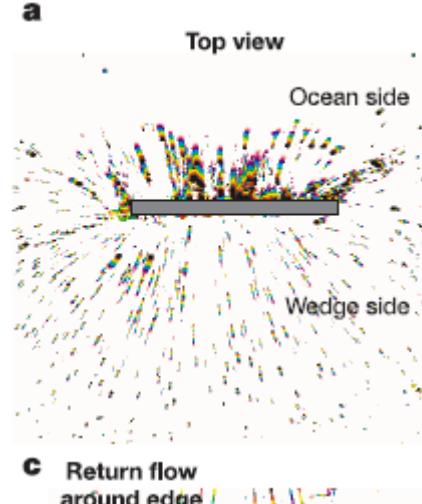
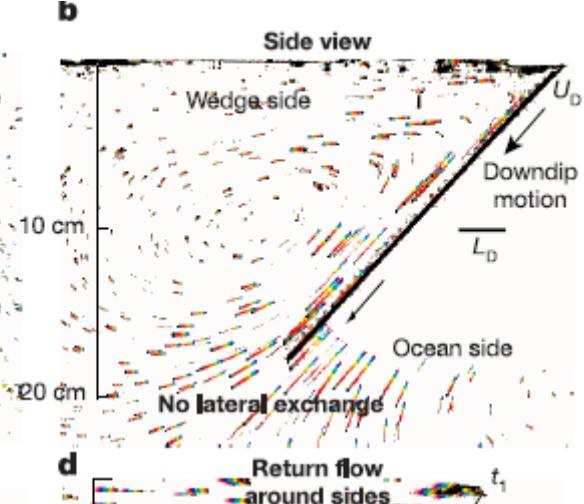
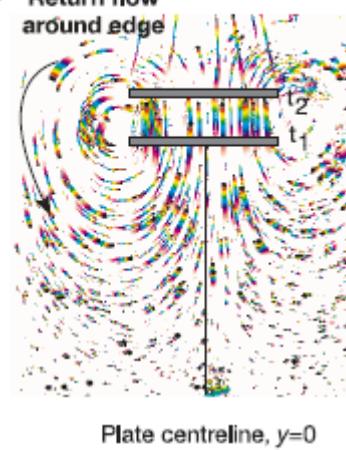
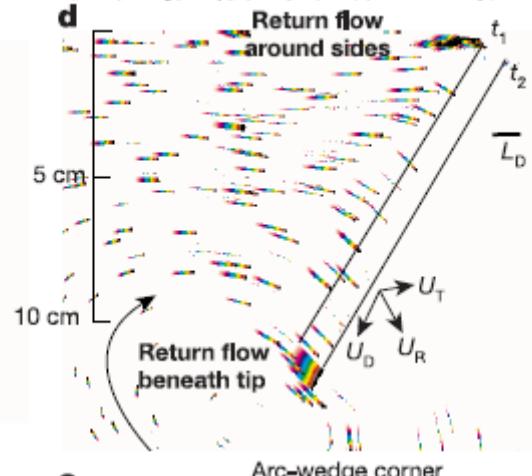
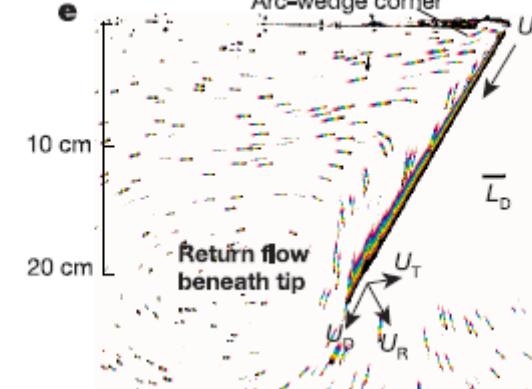
⇒ regional 3-D forward model

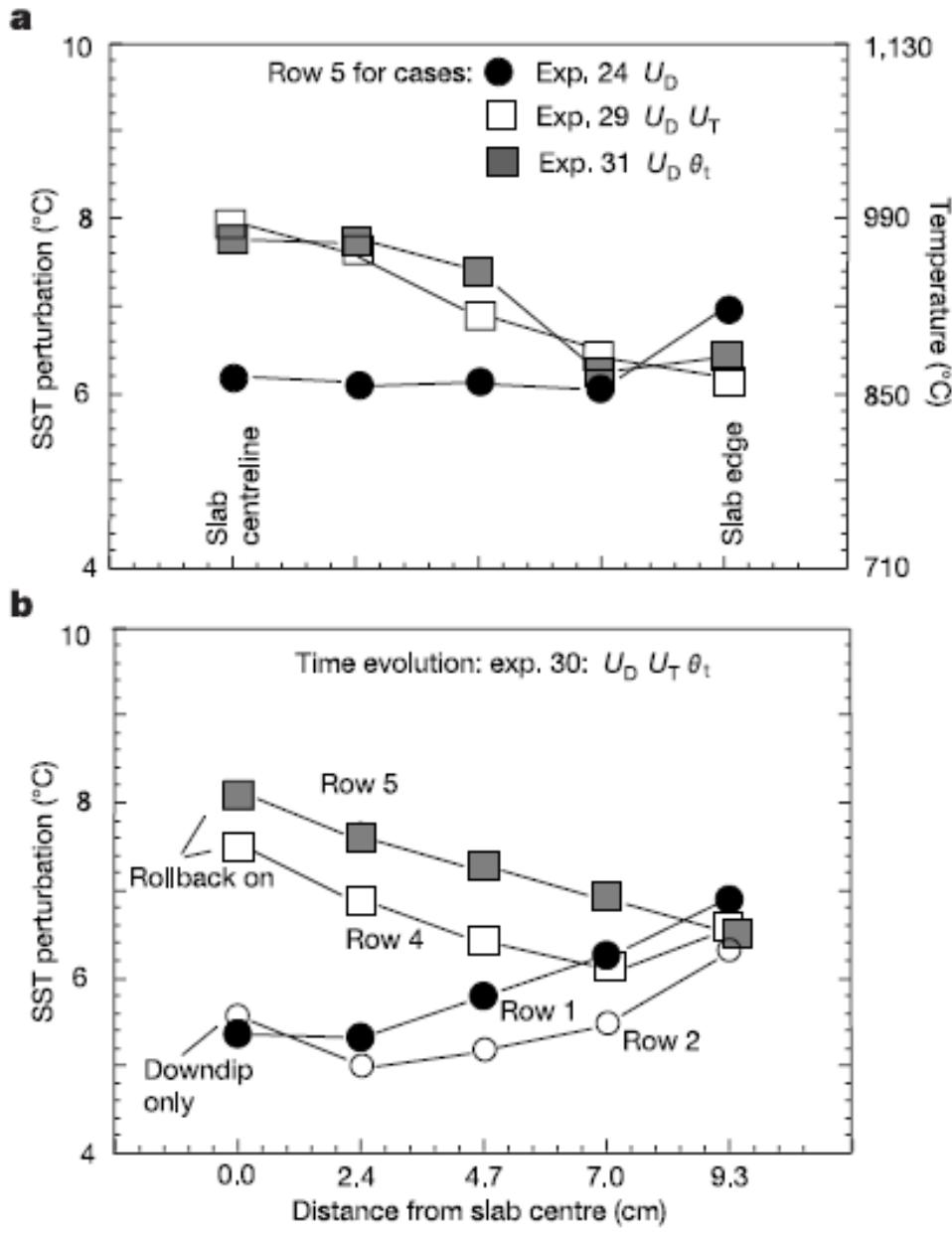
⇒ prescribed plate motions

⇒ slab segmentation expected

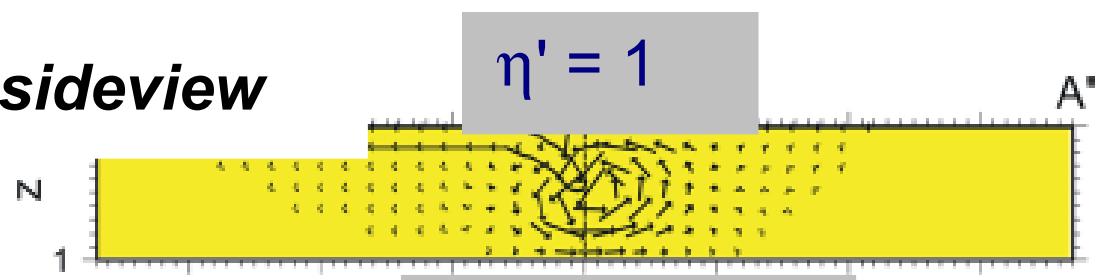
⇒ ambiguous cross-sections in tomography ⇒ convection is layered

Tan *et al.* (2002)

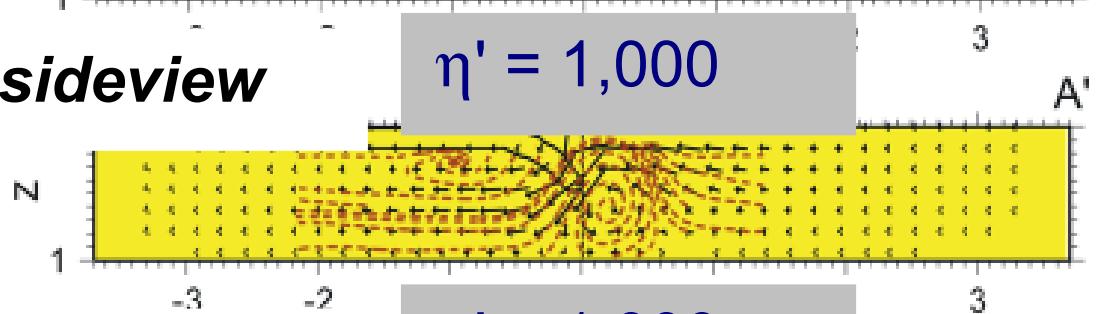
**a****b****a****b****c** Return flow around edge**d****e**



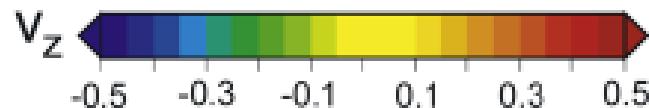
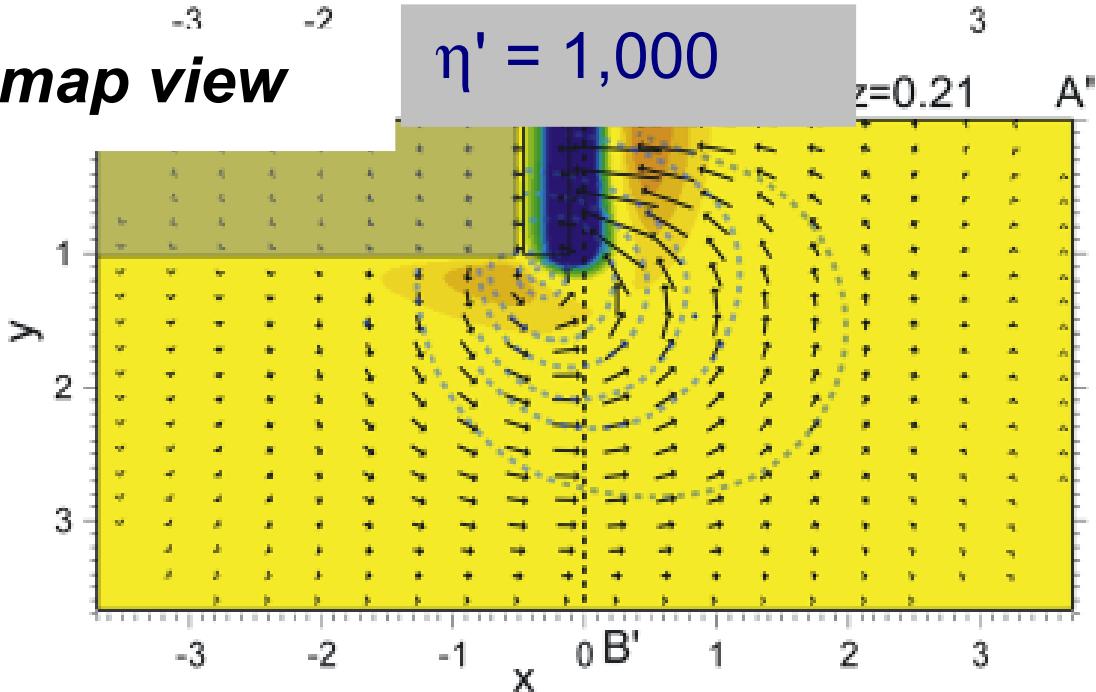
*sideview*



*sideview*

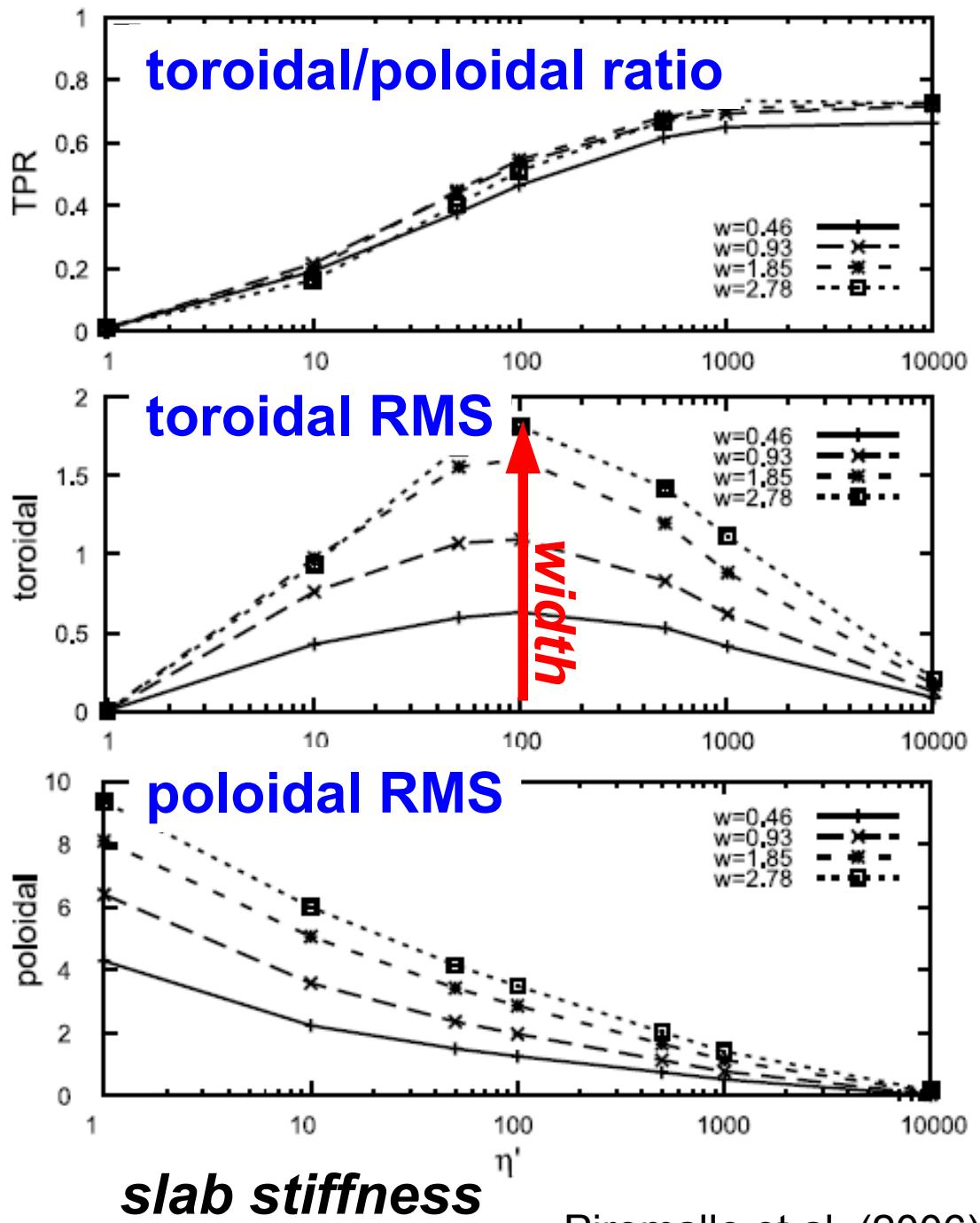


*map view*



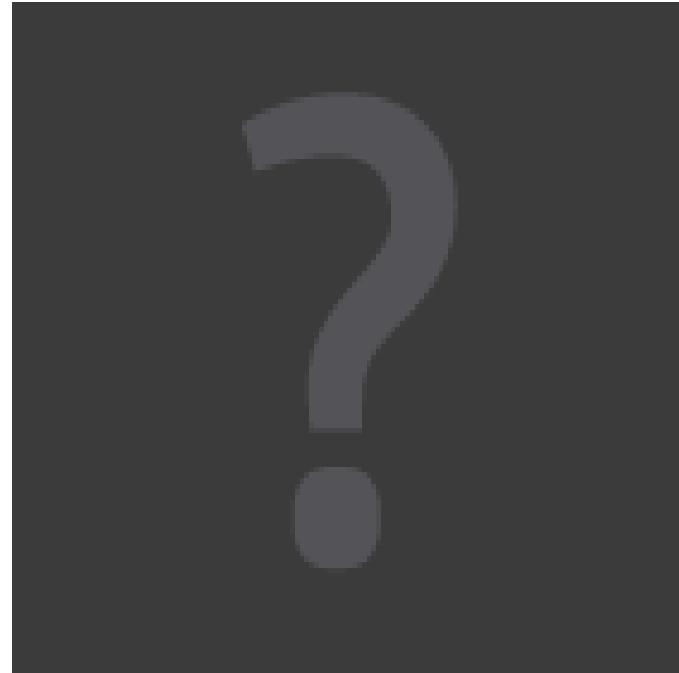
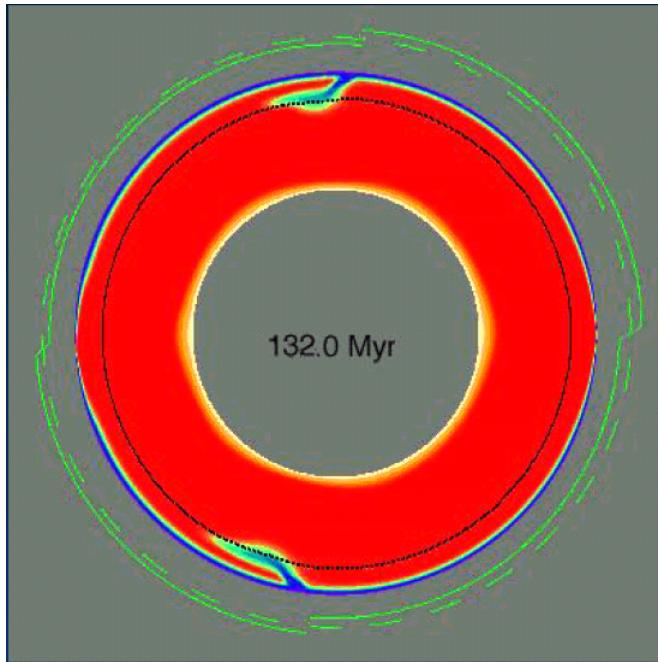
# Instantaneous toroidal partitioning

- Toroidal flow increases with slab width and peaks at moderate viscosity contrasts
- TPR increases with viscosity contrast

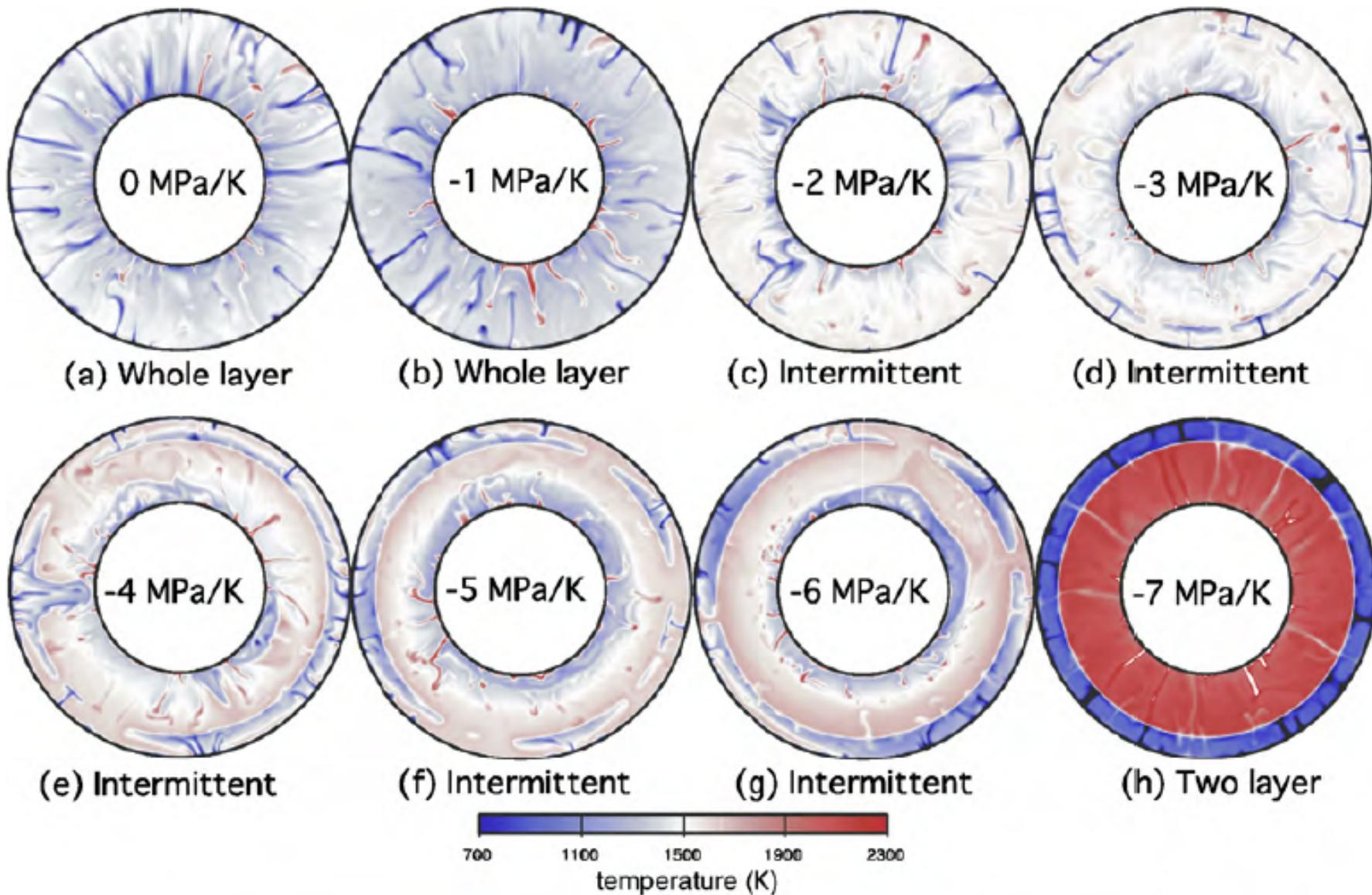


# Fully dynamic (free slab) models

# Trench rollback



Zhong and Gurnis (1995)

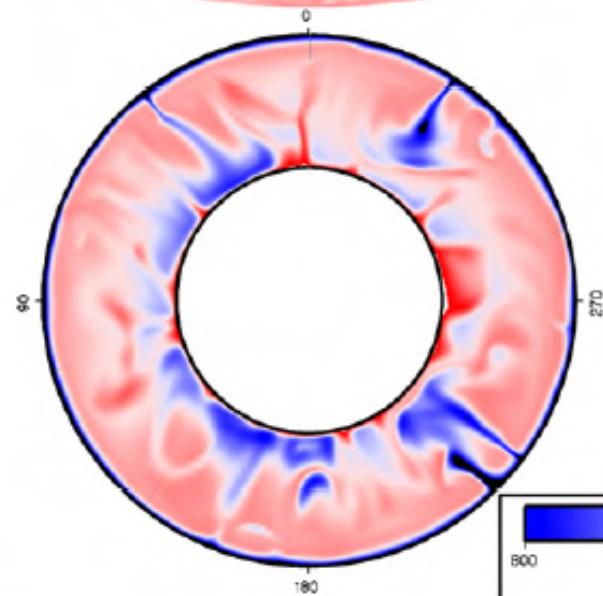
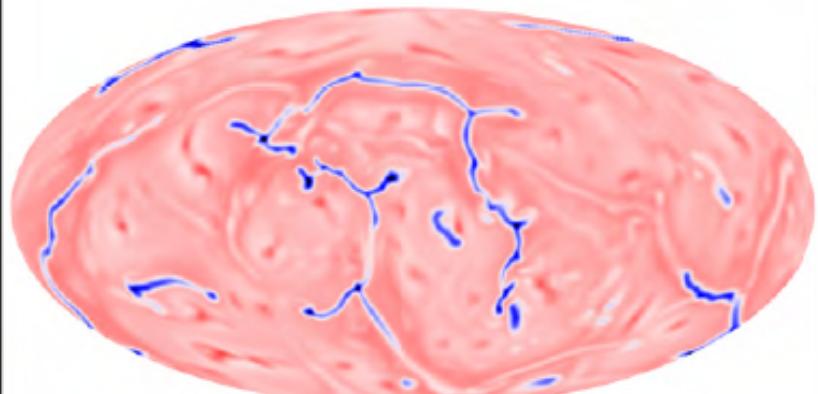


(a) case 1

temperature dependent viscosity, yielding

+

viscosity increase for the lower mantle



(b) case 2

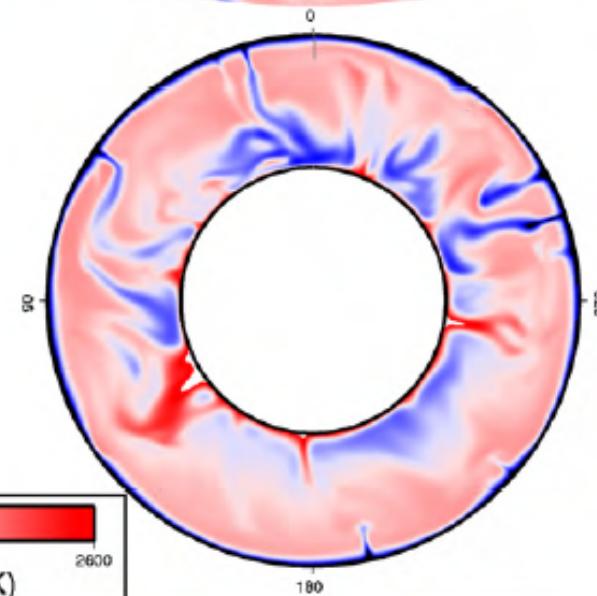
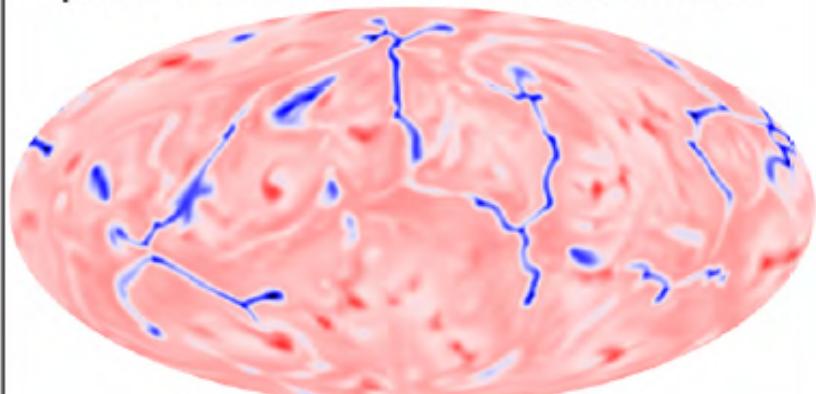
temperature dependent viscosity, yielding

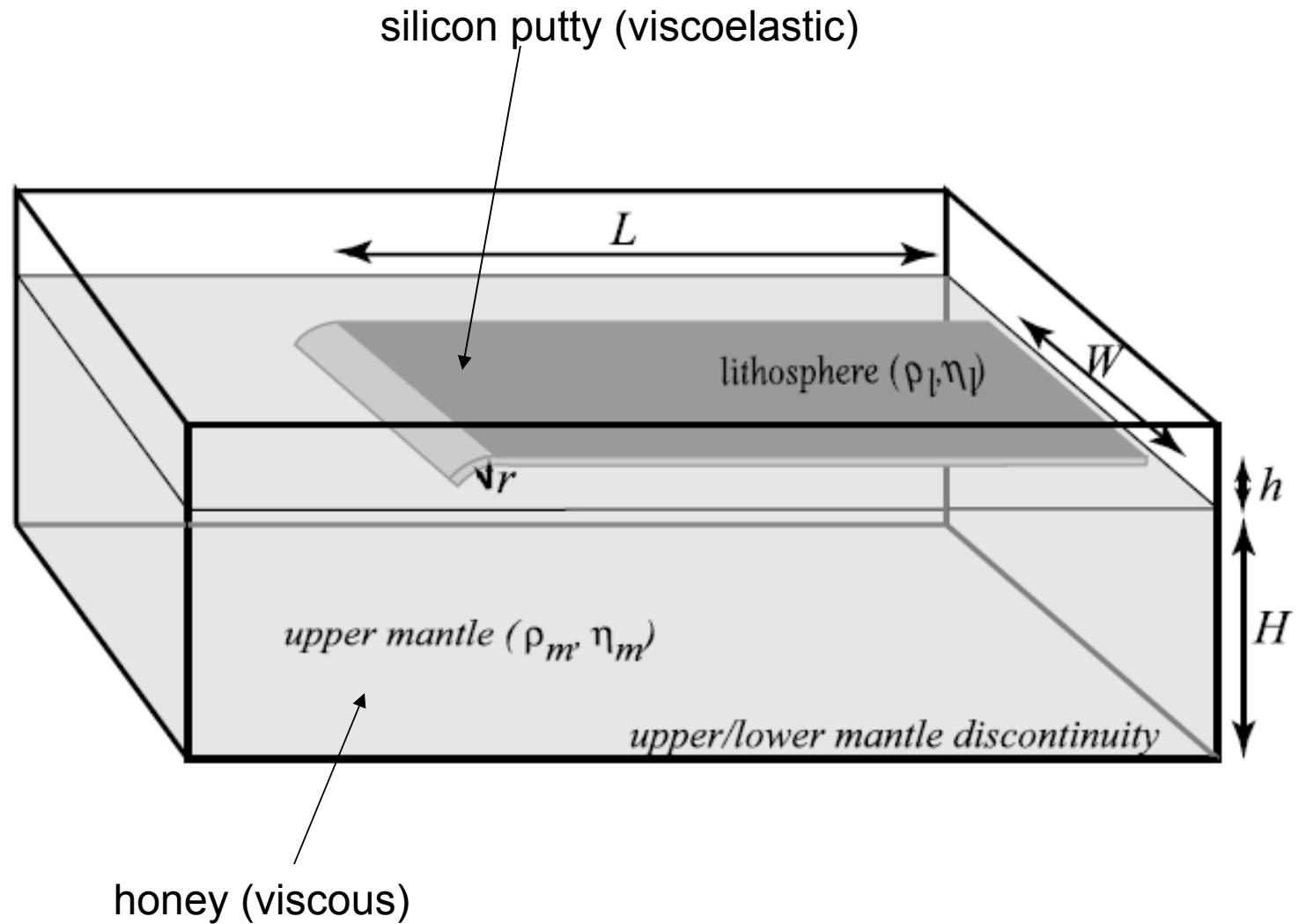
+

viscosity increase for the lower mantle

+

phase transition at 410 km and 660 km





a)

MODE I



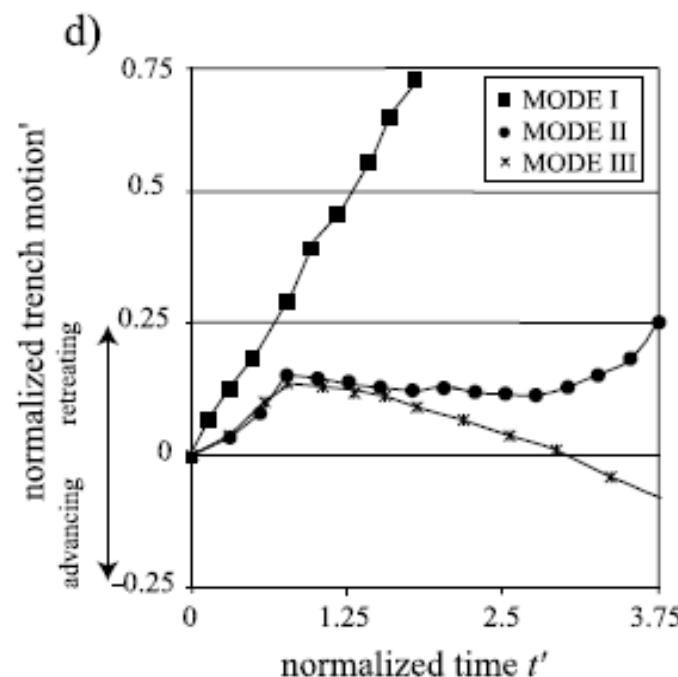
b)

MODE II



c)

MODE III

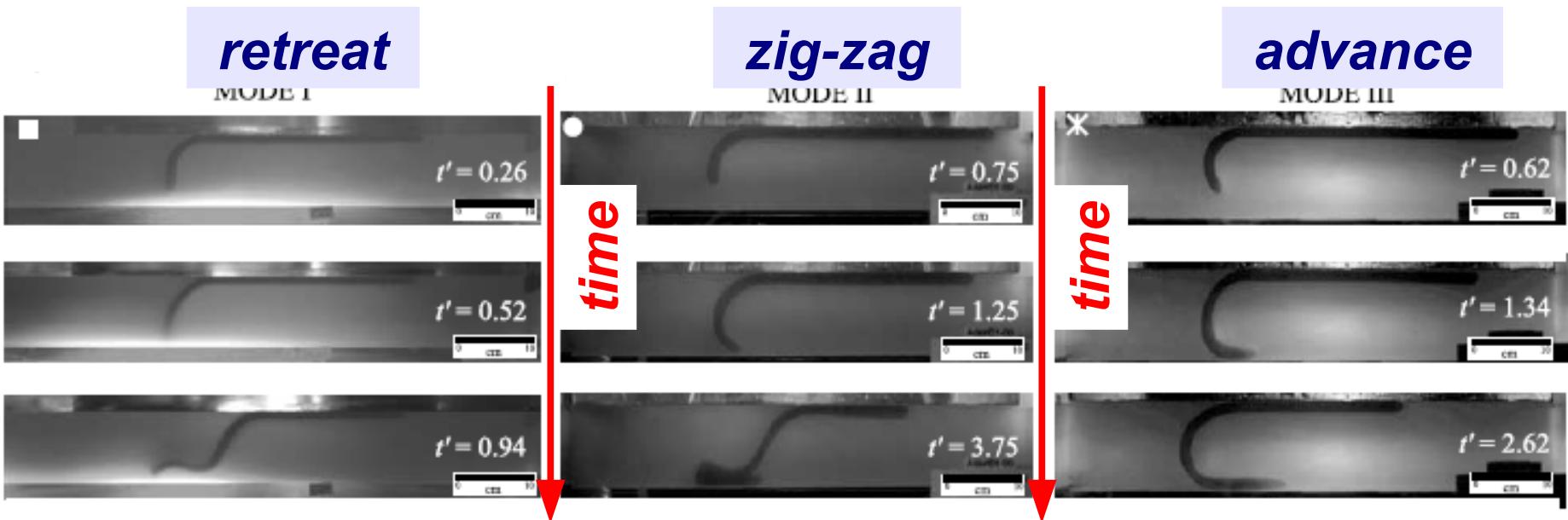
 $t' = 0.26$  $t' = 0.75$  $t' = 0.62$  $t' = 0.52$  $t' = 1.25$  $t' = 1.34$  $t' = 0.94$  $t' = 3.75$  $t' = 2.62$ 

'subduction = plate motion + trench motion'

Controls on modes:

- bending resistance
- curvature of subduction
- mantle depth
- strength of slab

# Strong slab trench dynamics



- For slabs with  $\eta' \sim 2,000 - 10,000$ , a mixed mode regime with advance and retreat exists for free slab models
- Analyze a wide set of experiments with different slab widths, viscosities, thickness, etc. (cf. Enns et al., 2005)

# Subduction velocity scaling

The diagram illustrates the components of subduction velocity. At the top, the words "slab bending" and "mantle drag" are written in bold black font. Orange arrows point from these words down to their respective terms in the equations below. The word "pull" is also present, with an orange arrow pointing to the first term in the equation for  $V'$ .

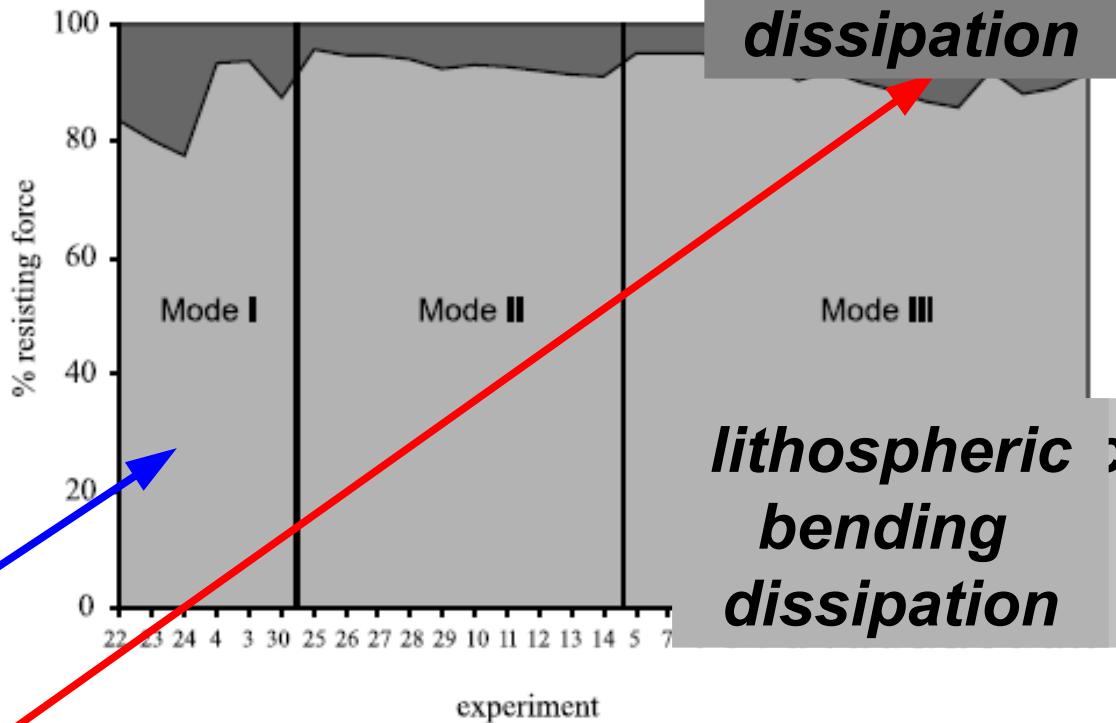
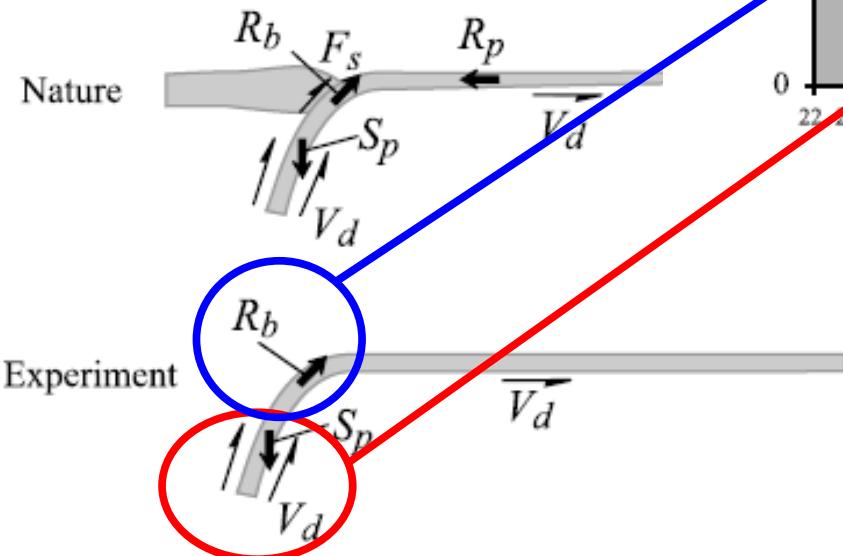
$$\begin{aligned} \text{slab } & \text{bending} & \text{mantle } & \text{drag} \\ \text{slab } & V' \approx \Delta\rho ghL/[2\eta_l(h/r)^3 + 3\eta_m A] & & \\ \text{pull} & & V^\circ = (\Delta\rho^\circ g H^\circ h^\circ)/\eta_m^\circ & \\ & V = V'/V^\circ & & \\ & = (hL/h^\circ H^\circ)[1/(2(\eta_l/\eta_m)(h/r)^3 + 3A)] & & \end{aligned}$$

- Subduction velocity = modified Stokes velocity accounting for bending
- Conrad & Hager (1999); Becker et al. (1999)

# Strong slab force balance

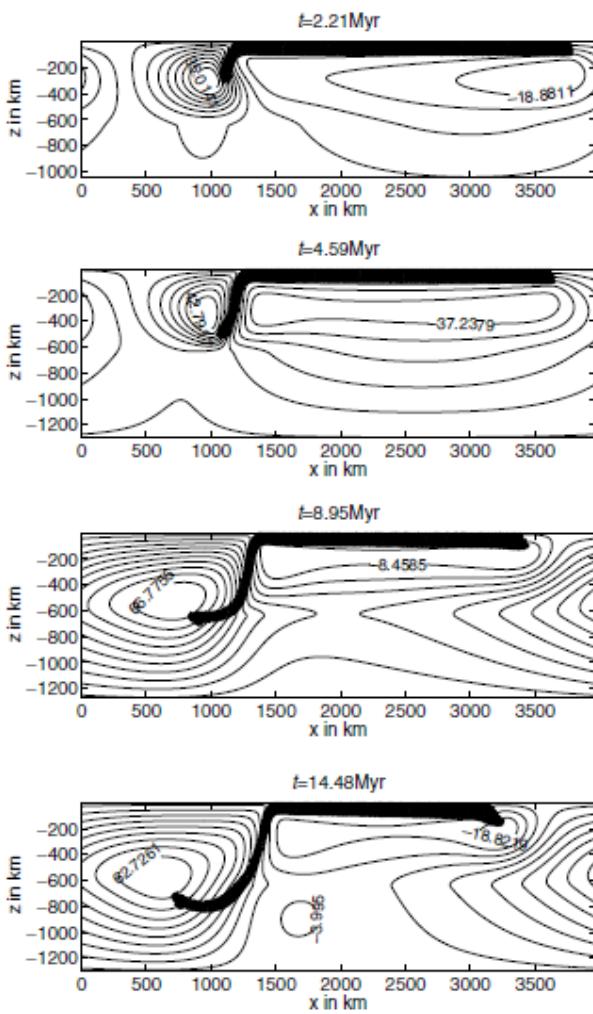
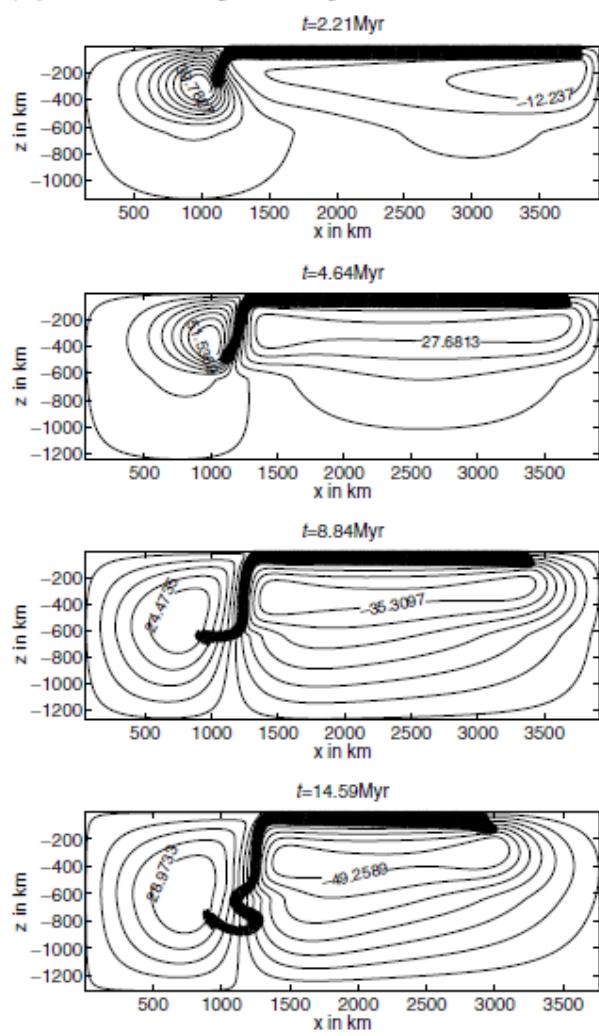
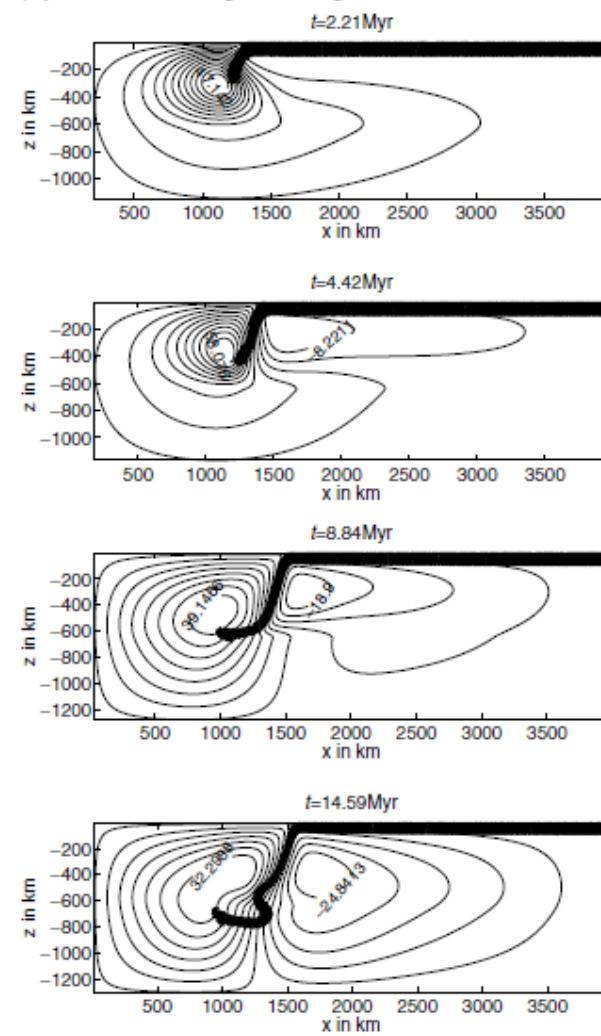
mantle flow  
dissipation

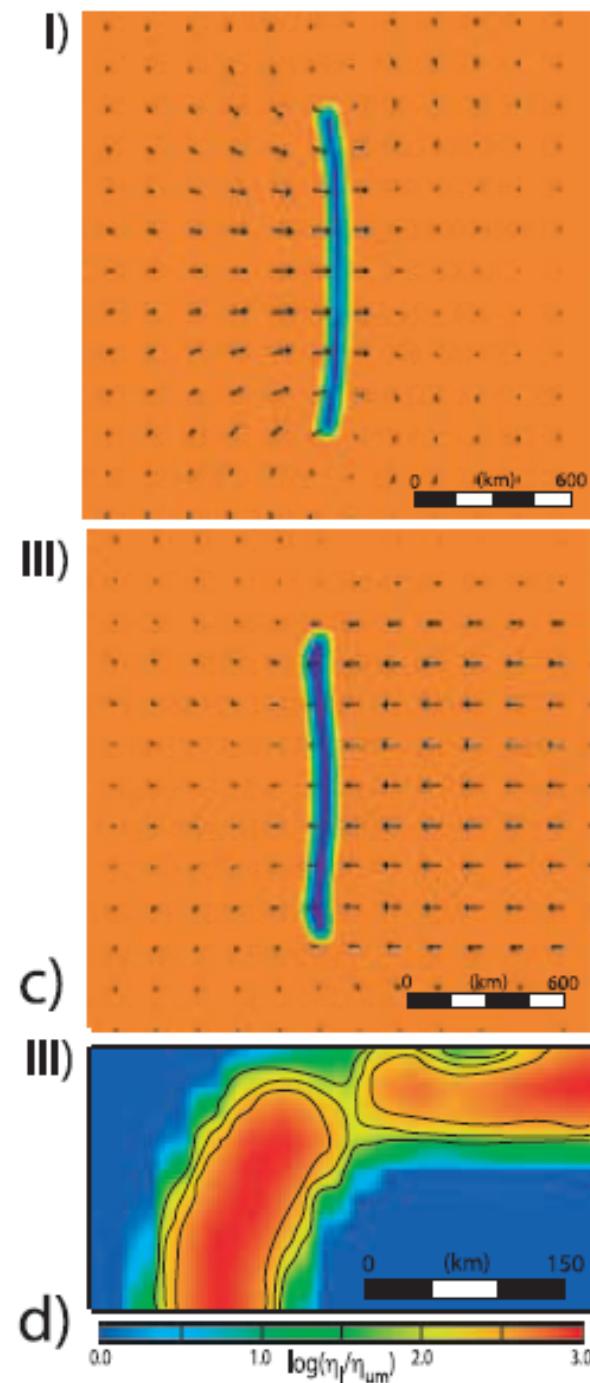
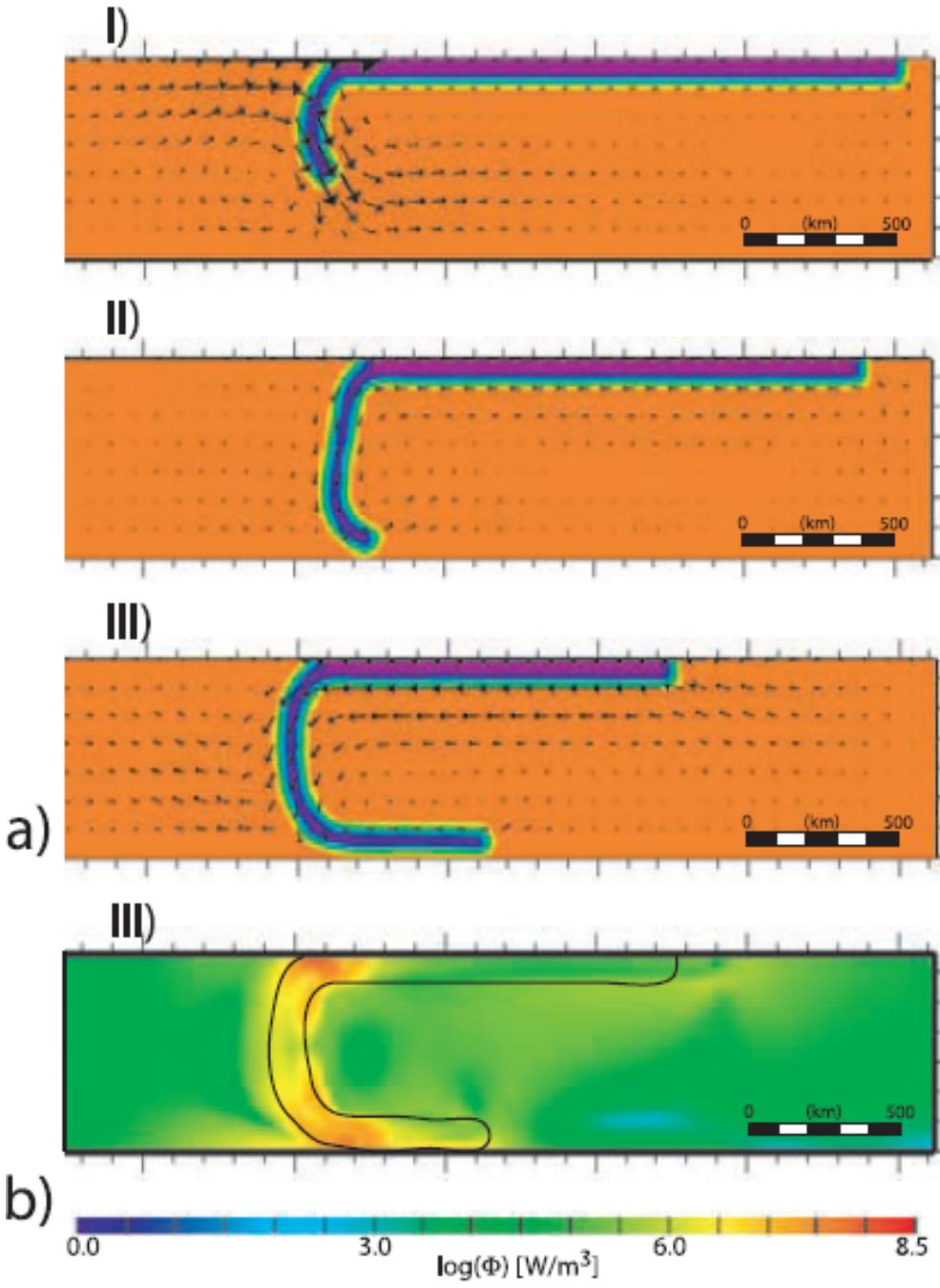
- Stiff slab experiments are dominated by bending vs. mantle drag
- cf. Buffett (2006) for proper force estimate (for  $r = \text{const.}$ )



- It's a percentage numbers game,  $f(\text{strength of slab})$ , which is not well known

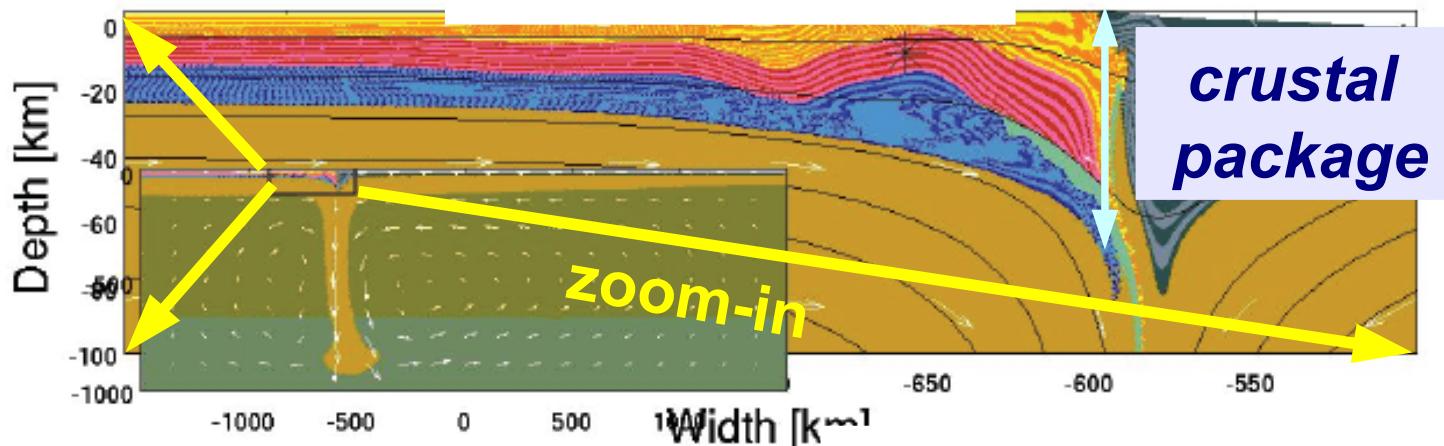
Bellahsen et al. (2005)

**(a)***periodic free slab***(b)***reflective free slab***(c)***reflective fixed slab*



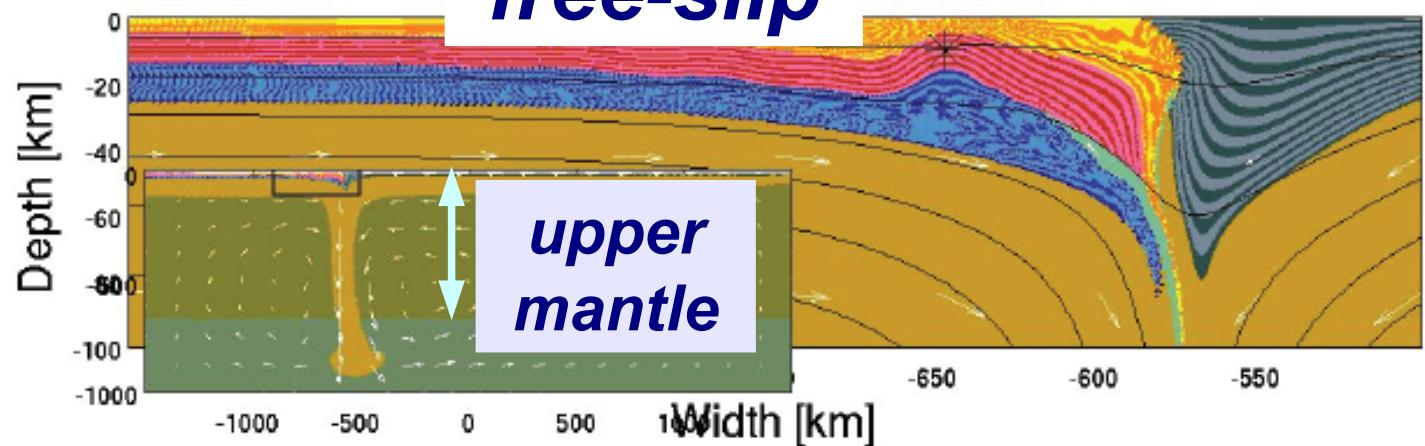
# Top boundary conditions I

*free surface*

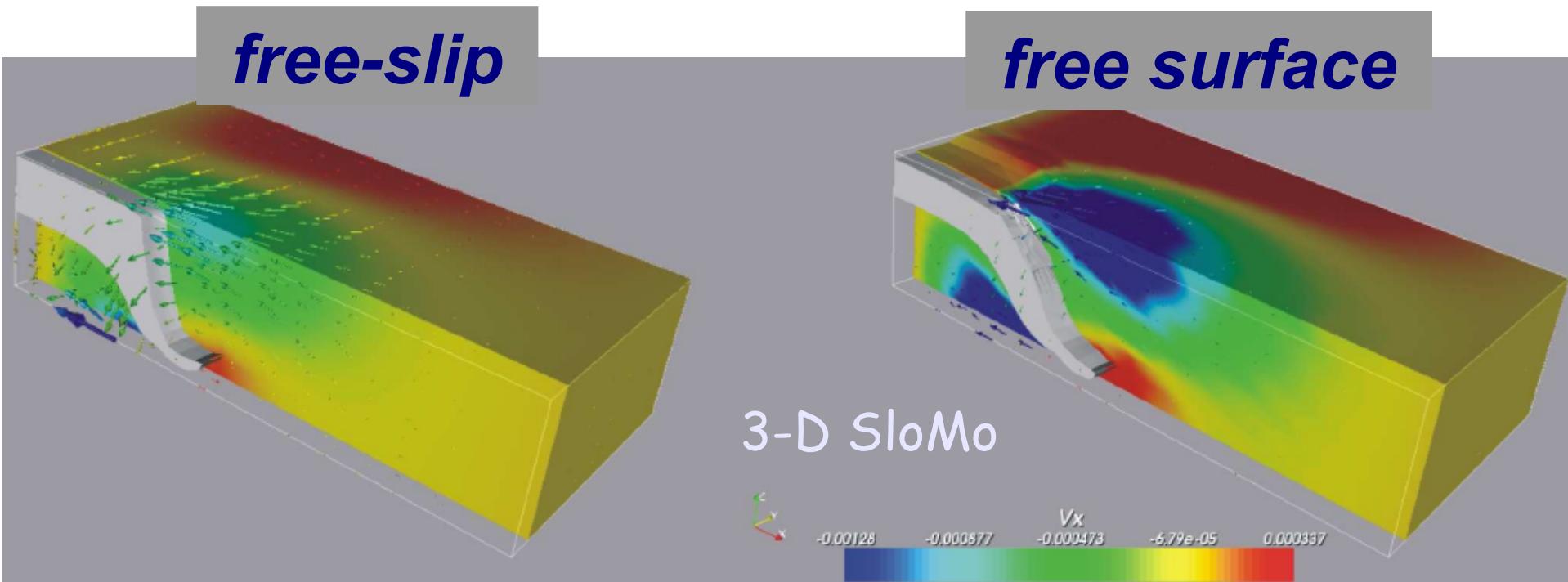


Elasto-visco-plastic rheology & erosion, finite elements (SloMo)

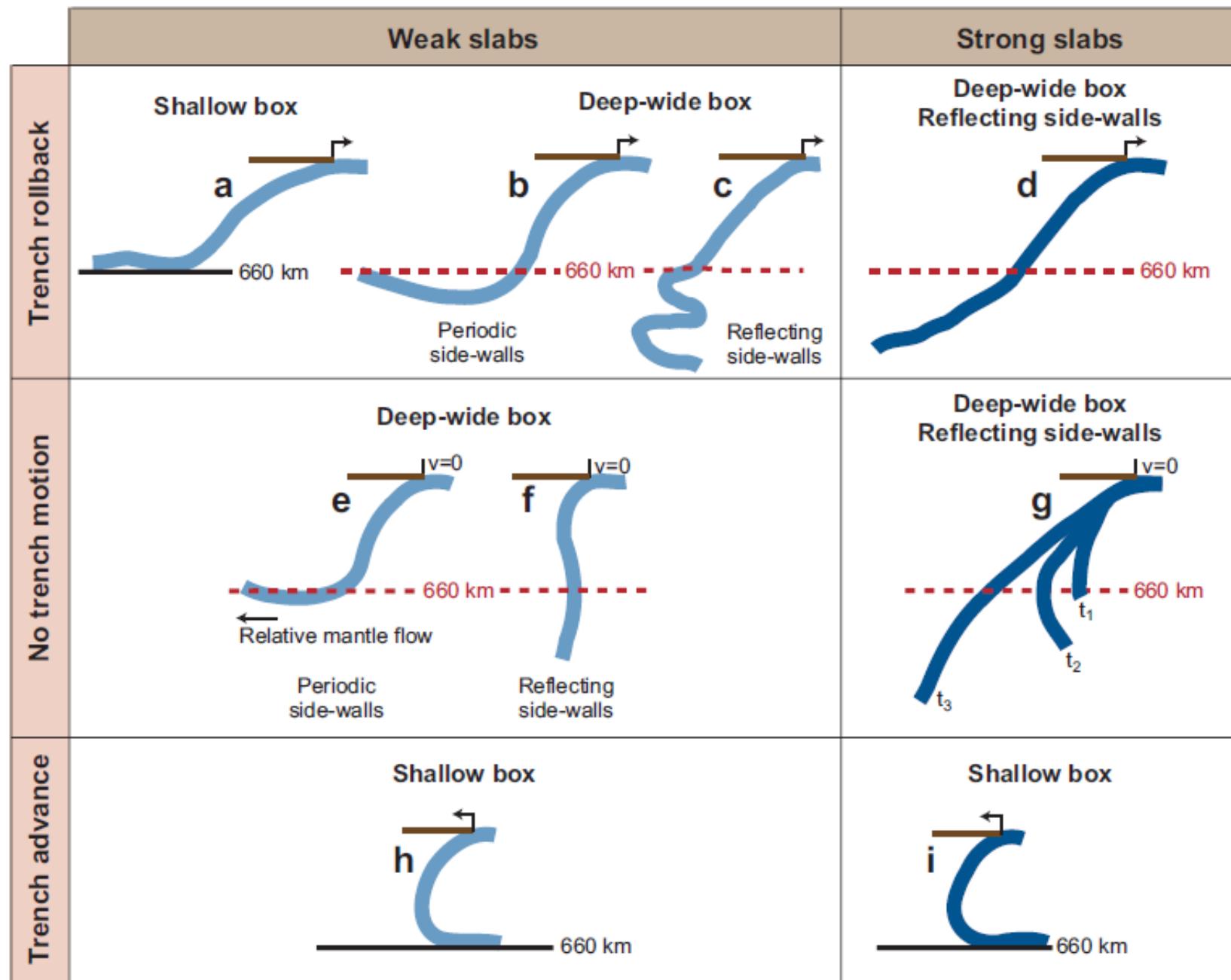
*free-slip*



# Top boundary conditions II



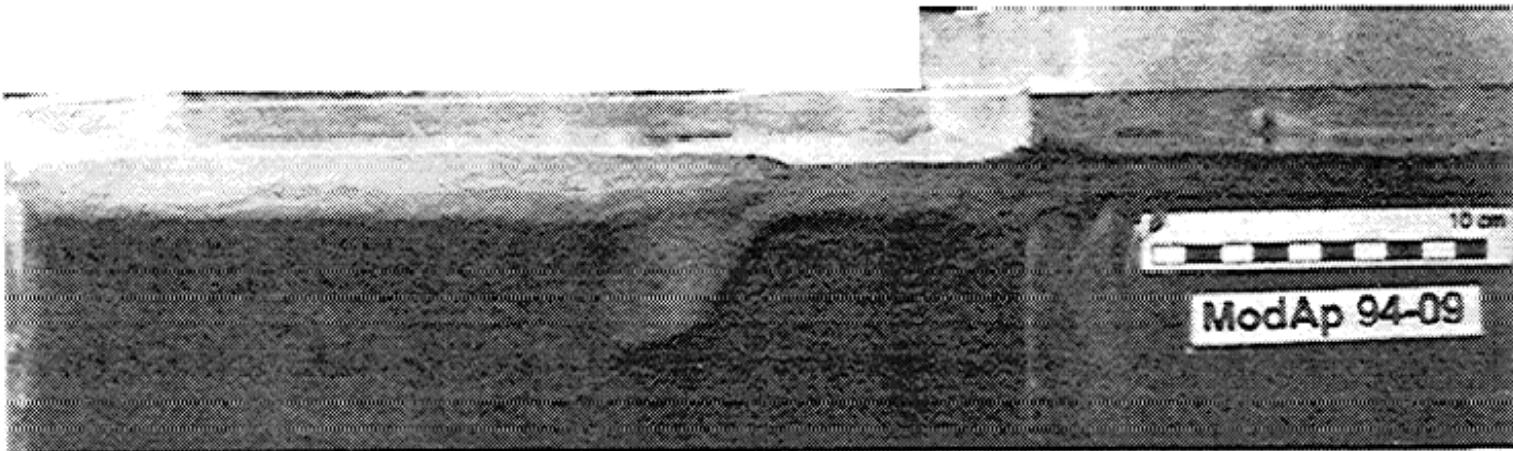
- Boundary condition important for isolated plate experiments  
(cf. Enns et al., 2005; Schmeling et al., 2006)
- Boundary condition not important for two-plate models (cf. Zhong, Moresi),  
and tests of Kaus et al. (20078)



# Effect of slab strength

- Toroidal power increases with viscosity contrast, i.e. flow becomes progressively less Stokes-sinker like (Piromallo et al., 2006)
- Subduction velocities (poloidal RMS) decrease with viscosity contrast, i.e. the slab strength has an important effect on mantle flow and subduction rates (Conrad & Hager, 1999; Becker et al., 1999; Bellahsen et al., 2005)
- Trench curvature is more convex for stiff slabs (cf. Finciello et al., 2004, Schellart et al., 2007)
- No elasticity needed to explain trench morphology (cf. Morra et al., 2006)

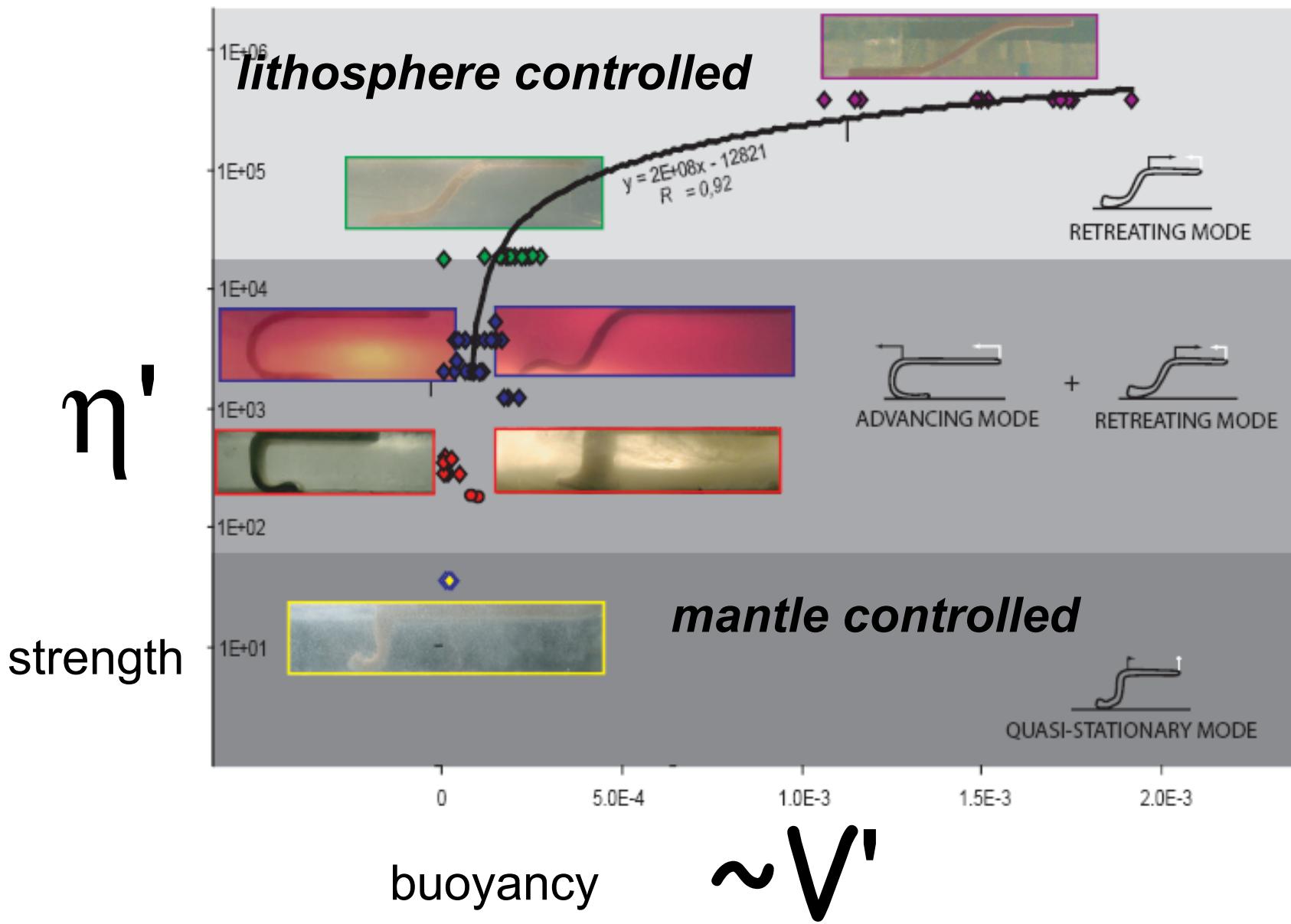
# The moderately weak slab



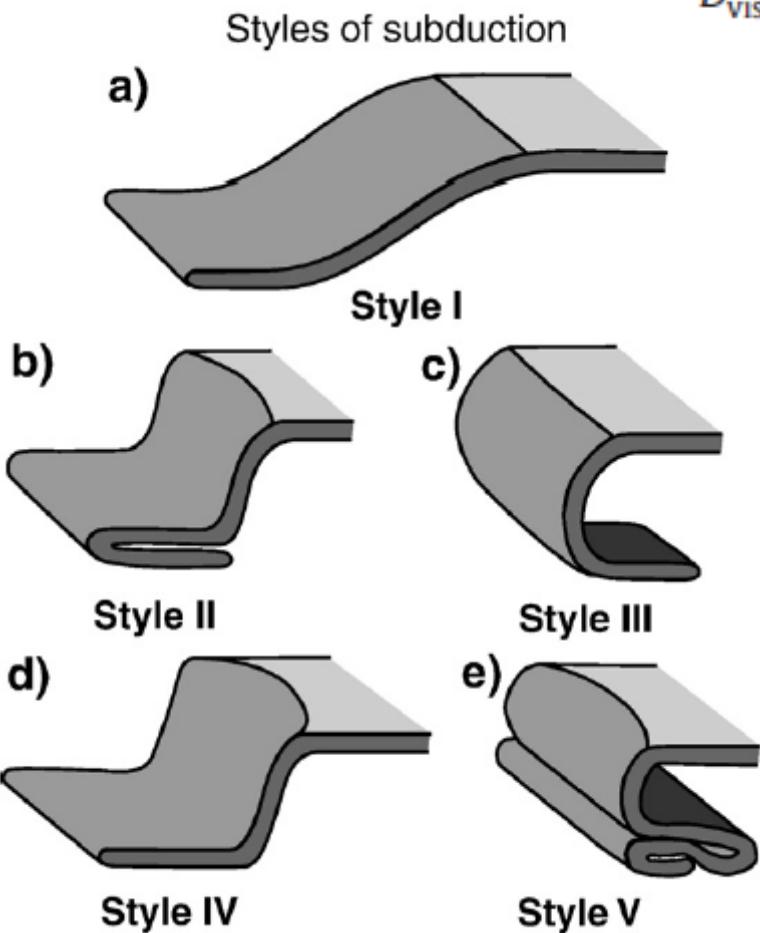
- Consistent with
  - Becker et al. (1999) and Conrad & Hager (1999) bending related estimates which yielded upper bound of  $\eta' \sim 500$
  - Moresi & Gurnis (1996) geopotential argument
  - Billen & Gurnis (2005) trench admittance work
  - ...

Becker *et al.* (1999)

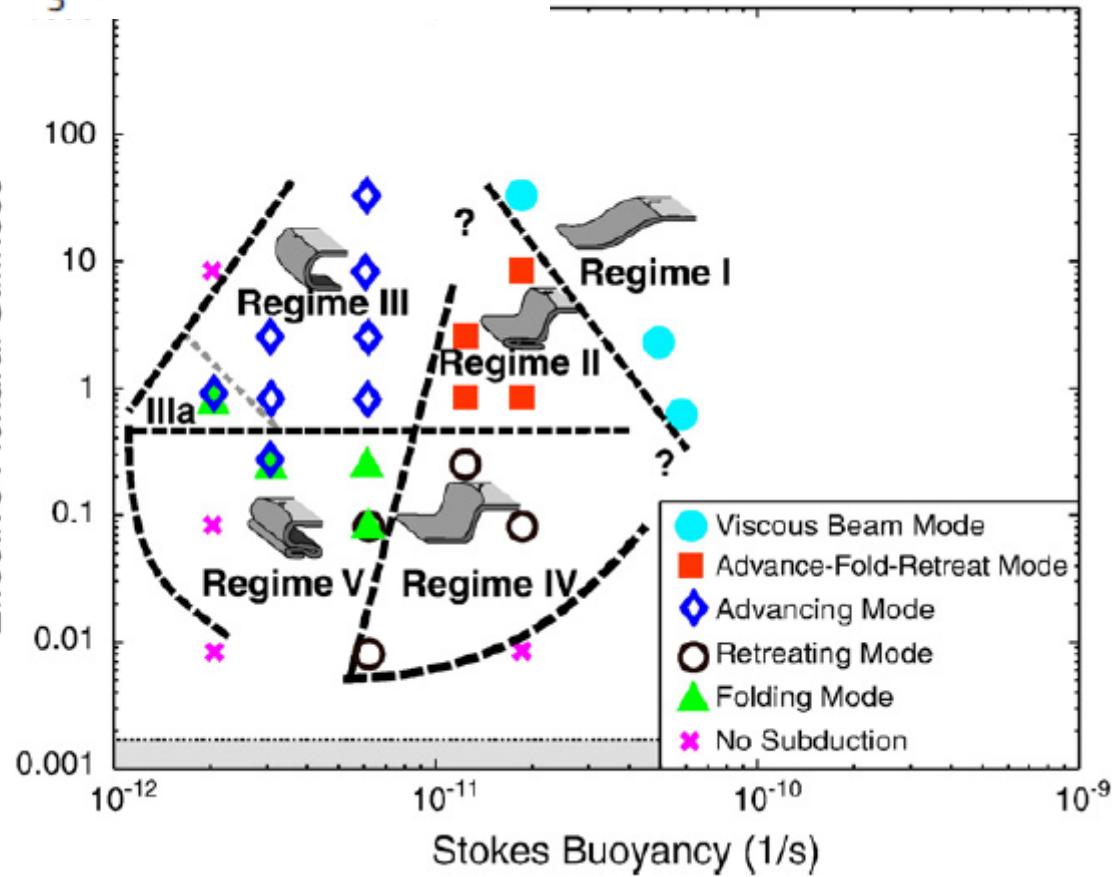
# Lab model behavior as $f(\eta')$



Funiciello et al. (2007) with  
data from Schellart (2004)



$$D_{\text{vis}}^* = \frac{D_{\text{vis}}}{\frac{1}{3}\eta_{\text{lum}} H^3} = \frac{\eta_{\text{plate}}}{\eta_{\text{lum}}} \left( \frac{h_{\text{plate}}}{H} \right)^3$$



Stegman et al. (2010)

$$B_S = \frac{\Delta \rho g h_{\text{plate}}}{\eta_{\text{lum}}}$$

# Thin sheet BEM models of free slabs

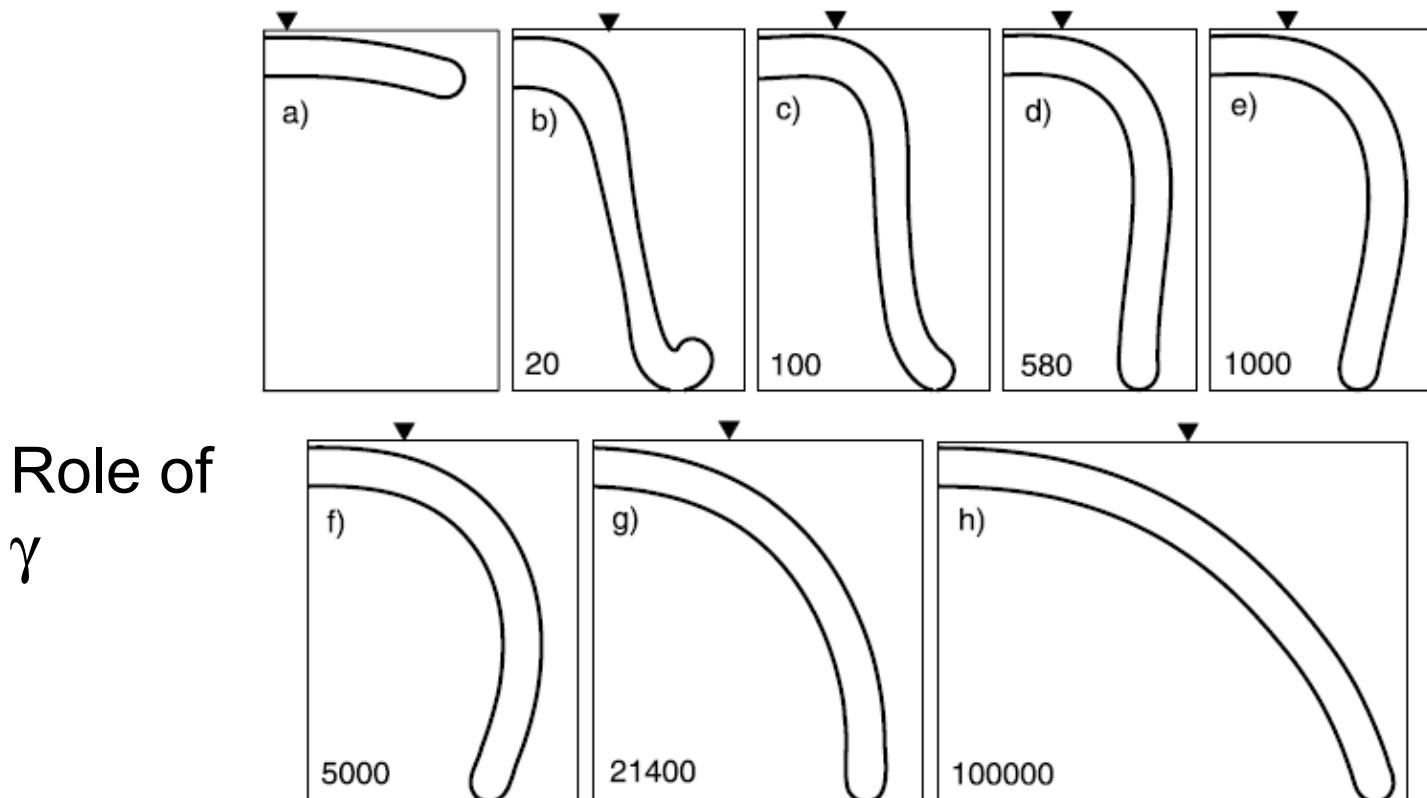
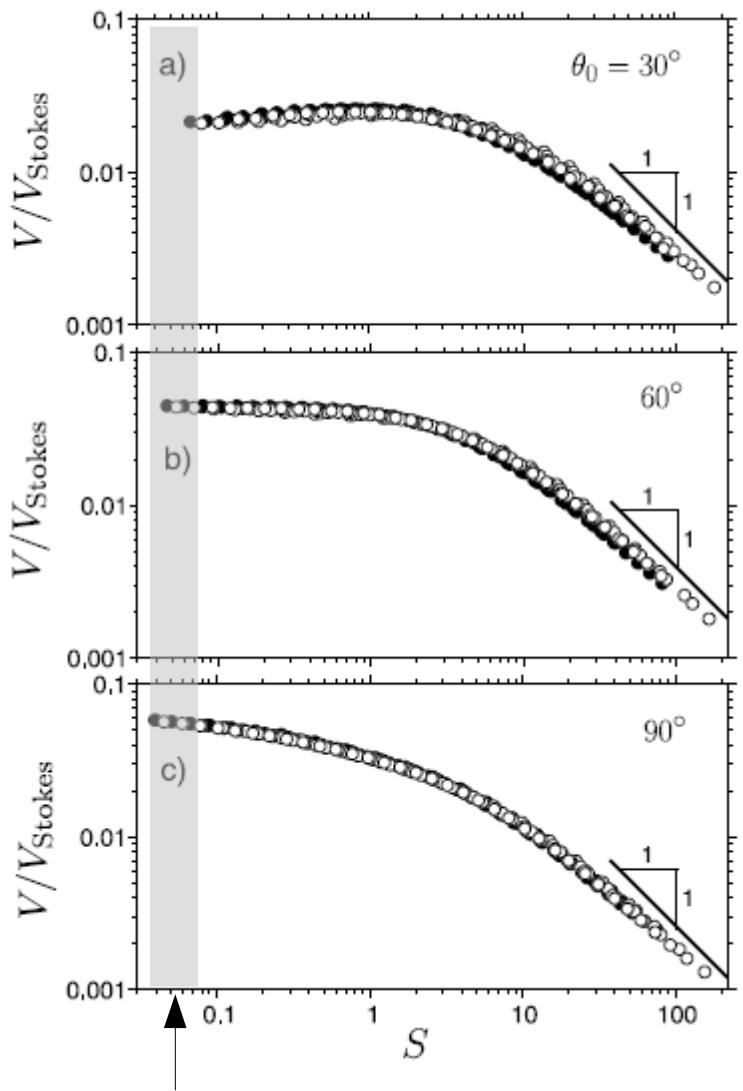


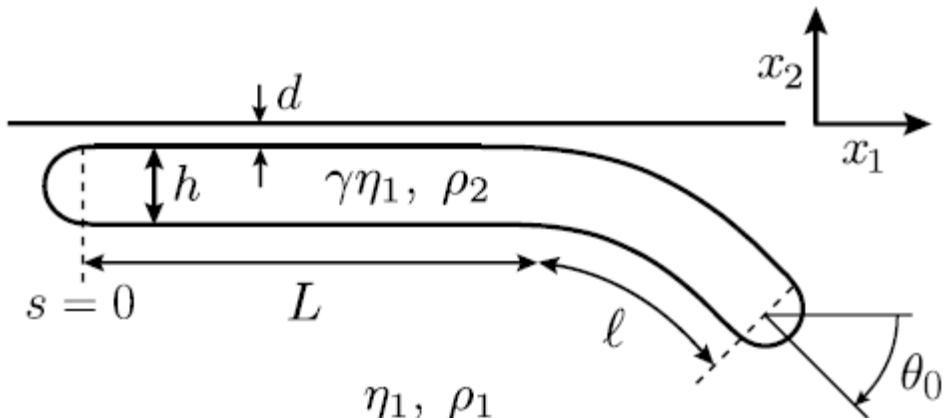
Figure 12. Shapes of subducting viscous sheets that have reached a depth  $D = 9.17h$ , starting from the initial conditions  $L(0) = 16h$ ,  $d/h = 0.2$ ,  $\ell(0) = 4h$  and  $\theta_0(0) = 15^\circ$  shown in panel a). The viscosity contrast  $\gamma$  is indicated at the lower left-hand corner of panels (b)–(h). The inverted triangles indicate the initial position of the trench.

# Thin sheet BEM models of free slabs



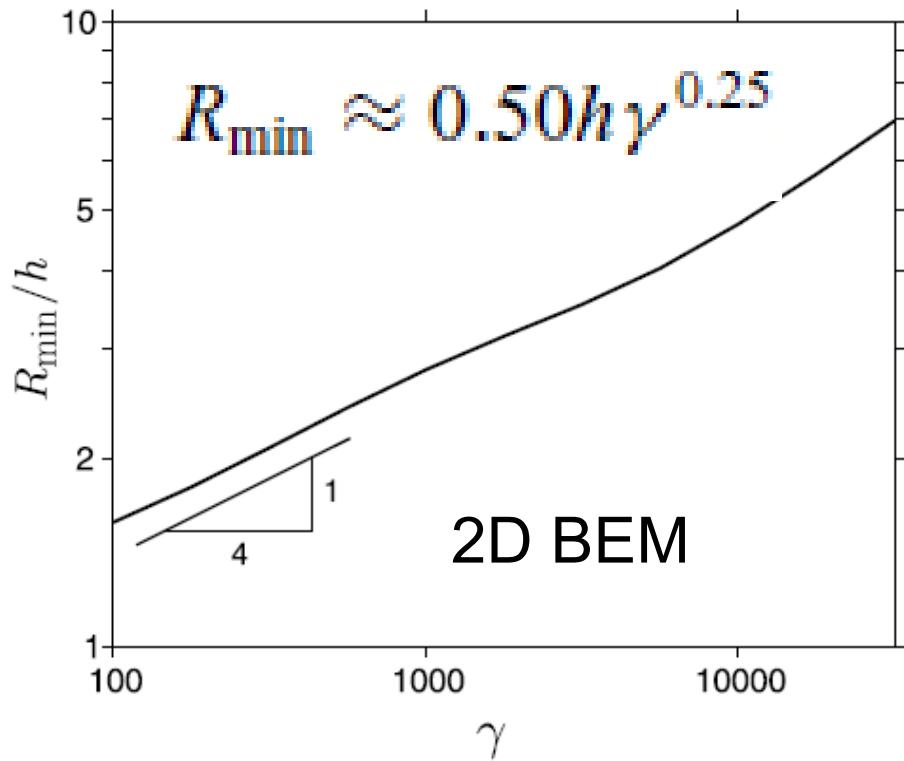
Capitanio et al. (2007) models

$$\gamma \left( \frac{h}{\ell_b} \right)^3 \equiv S,$$



Ribe (2010)

# Thin sheet BEM models of free slabs

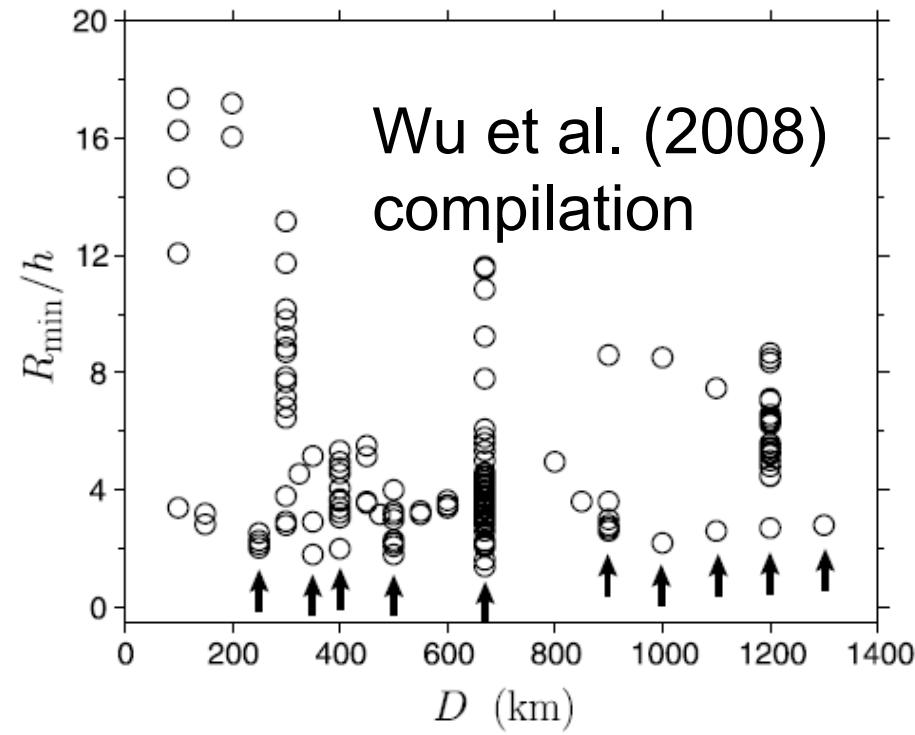


**Figure 13.** Minimum radius of curvature  $R_{\min}$  of a subducting sheet at the time when its tip reaches a depth  $D = 8.25h$ , as a function of the viscosity contrast  $\gamma$ . The initial condition is the same as in Fig. 12(a).

$$\gamma \in [140; 410]$$

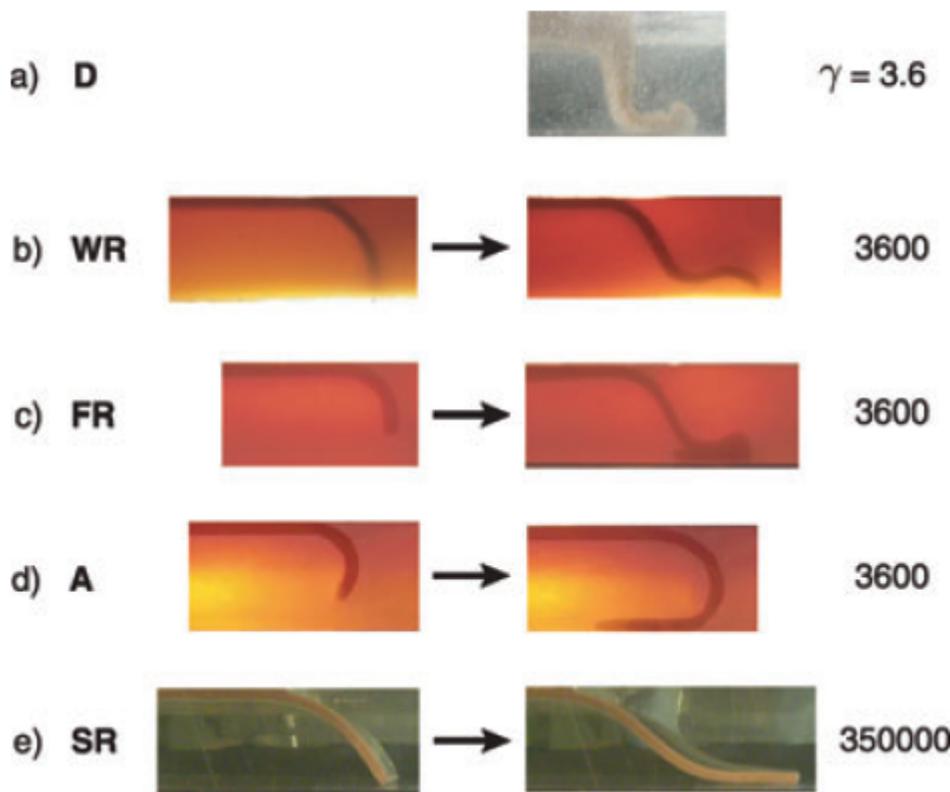
Consistent with Funiciello et al. (2009)

$$\gamma \in [150; 500]$$

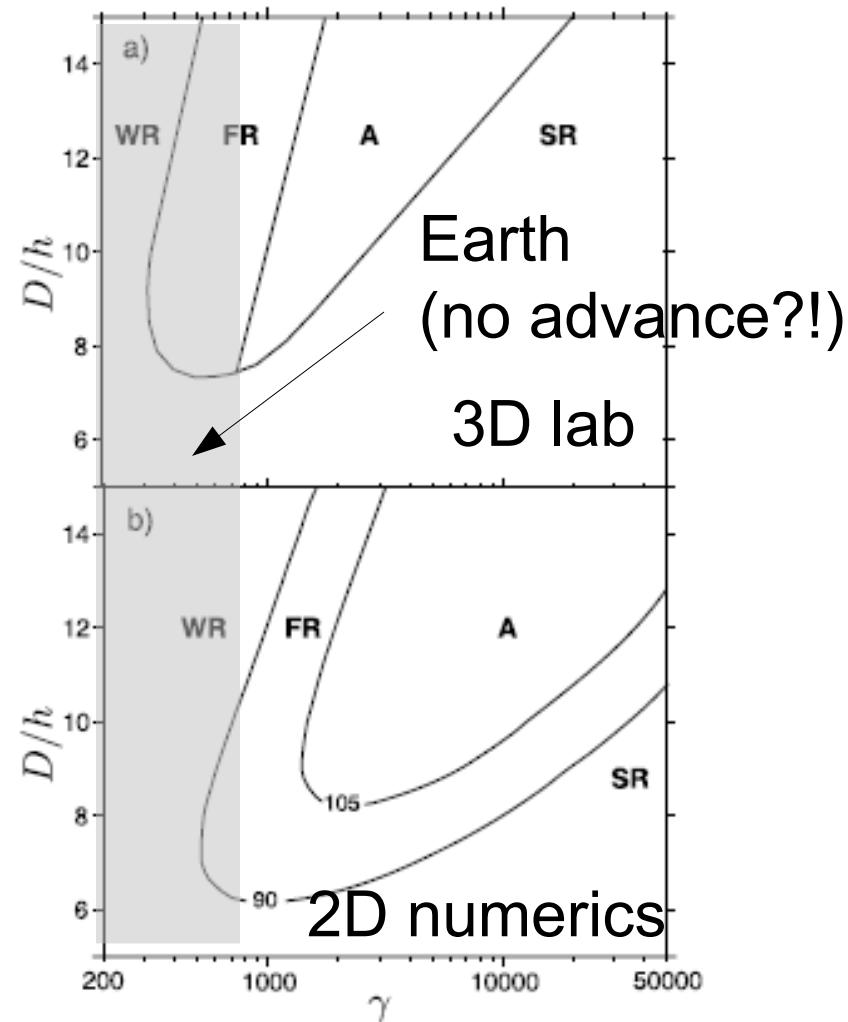


**Figure 14.** Normalized minimum radius of curvature  $R_{\min}/h$  of subducting slabs on Earth as a function of the slab's maximum depth  $D$  (data from Wu et al. 2008). Arrows indicate the data points used to estimate the global minimum value of  $R_{\min}/h$ .

# Role of the dip at touchdown

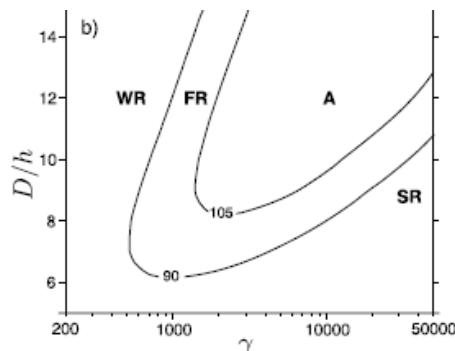


**Figure 10.** Modes of free subduction observed in analogue laboratory experiments. (a) ‘dripping’ (D) mode; (b) ‘weak retreating’ (WR) mode; (c) ‘folding retreating’ (FR) mode; (d) ‘advancing’ (A) mode and (e) ‘strong retreating’ (SR) mode. The photographs in the left-hand column were taken before the sheet’s leading end reached the bottom of the experimental tank, and those in the right-hand column some time after. The viscosity contrast  $\gamma$  for each experiment is indicated at far right-hand side. The depths of the fluid layers are 9.4 cm for (a), 11 cm for (b)–(d) and 9.7 cm for (d). Photographs courtesy of F. Funiciello.

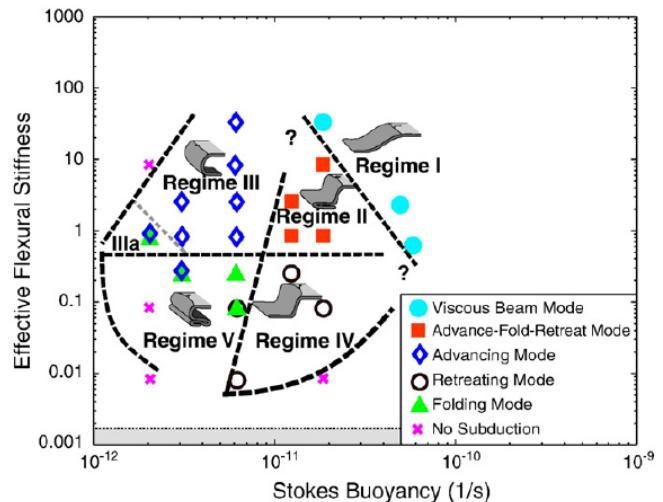


**Figure 11.** (a) Phase diagram showing the modes of free subduction observed in laboratory experiments as a function of the viscosity contrast  $\gamma$  and the ratio  $D/h$  of the layer depth to the sheet thickness (adapted from Fig. 13 of Schellart 2008). WR: weak retreating mode. FR: folding retreating mode. A: advancing mode. SR: strong retreating mode. (b) Contours of the dip  $\theta_D$  (in degrees) of the tip of the slab at the time when it reaches the depth  $D$ , predicted numerically using the BEM model. The initial condition for the calculations is  $\ell(0) = 0.455 D$ ,  $\theta_0(0) = 15^\circ$ ,  $L/h = 16$  and  $d/h = 0.2$ .

# Why not $f(\Delta\rho)$ ?



vs.



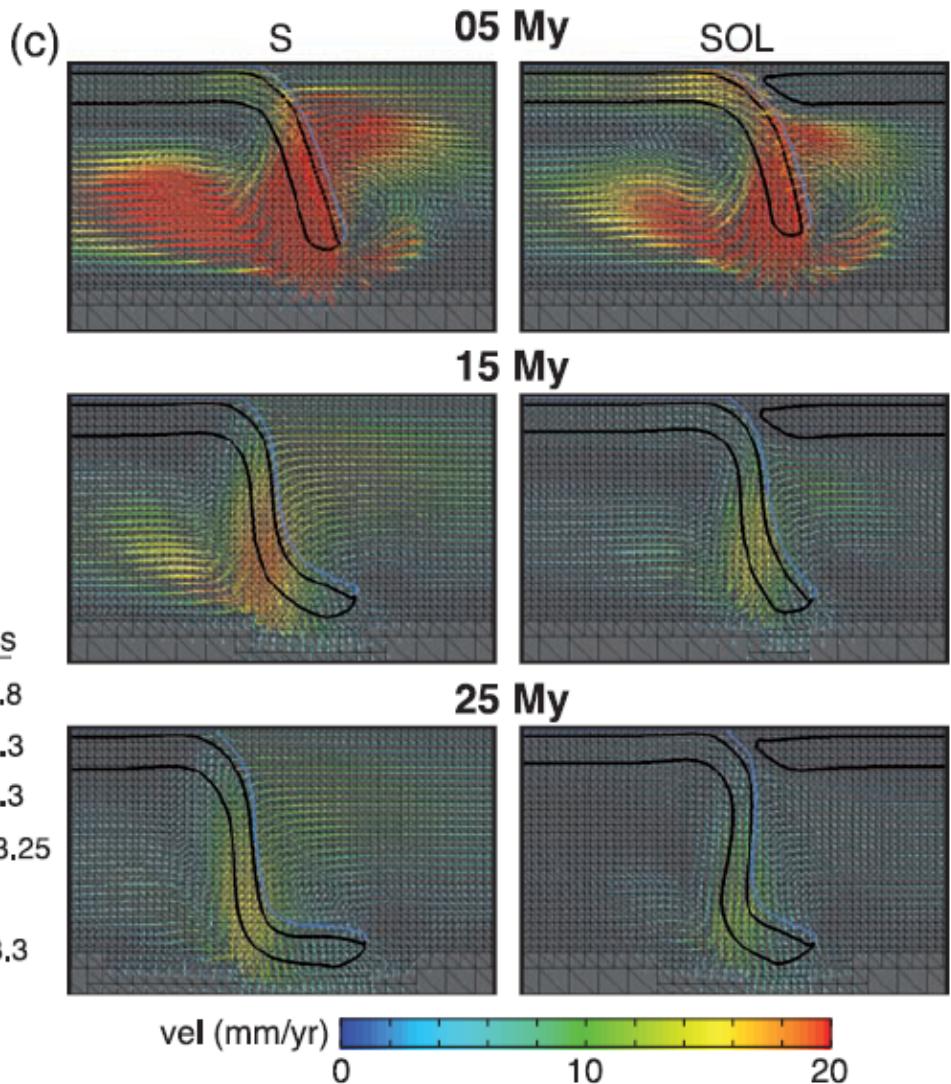
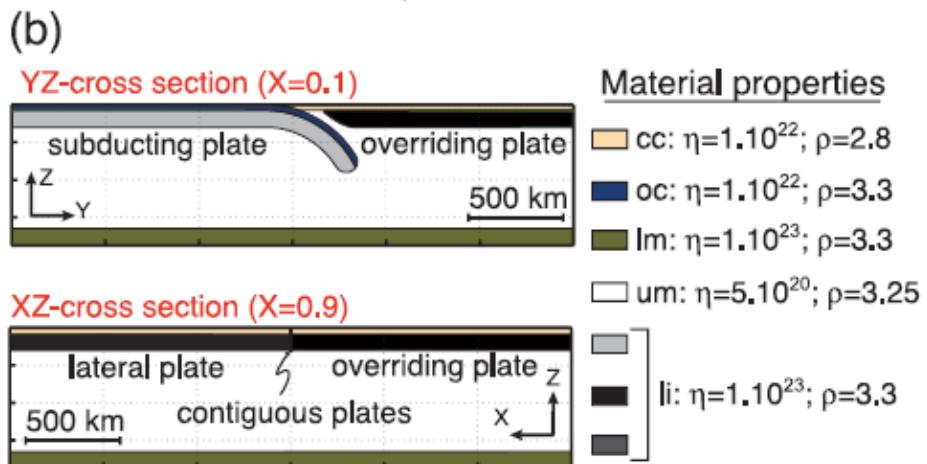
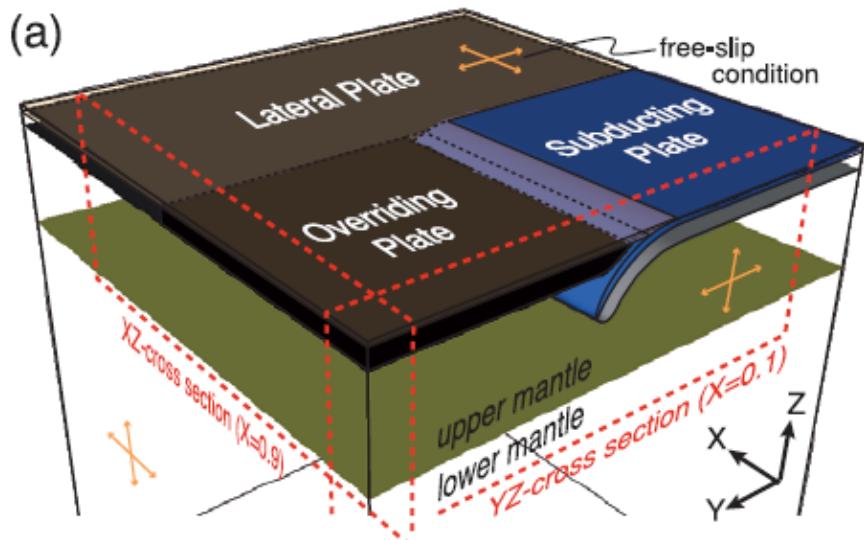
Lab: surface tension (Bellahsen et al., 2005)

$$Bo^{-1} = \frac{\sigma}{h^2 g \Delta \rho} \quad Bo^{-1} \in [0.37; 2.2]$$

Numerics: plastic yielding (Stegman et al., 2009)

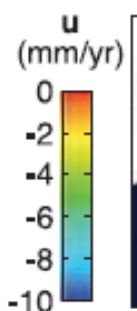
$$\Pi = \frac{\tau}{hg\Delta\rho} \quad \Pi \in [0.06; 1.85]$$

# Real slabs aren't free

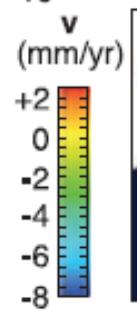


(15 My)

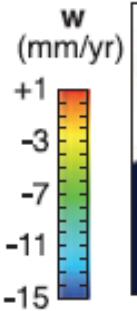
S



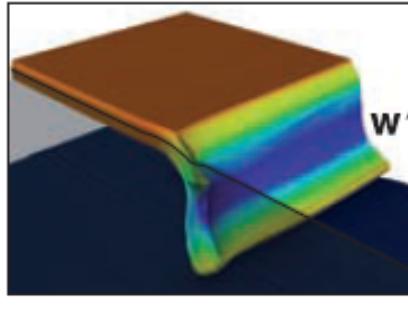
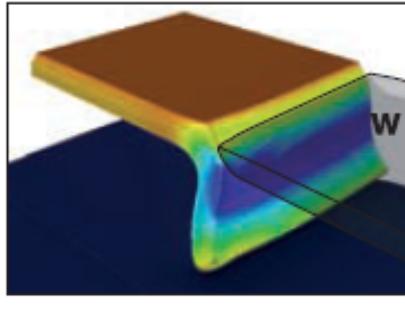
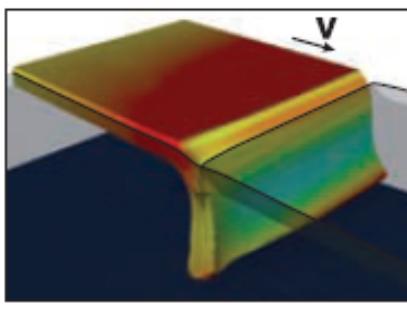
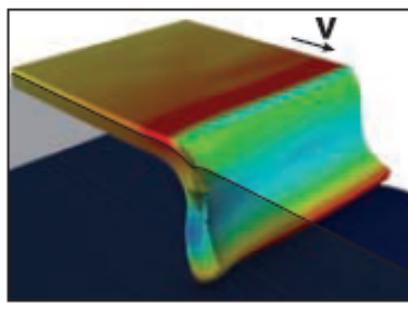
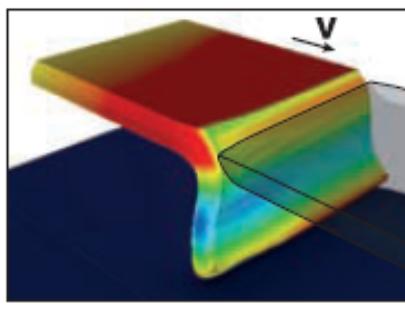
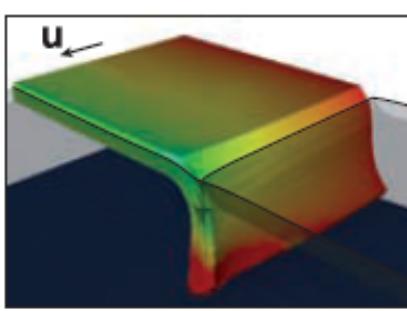
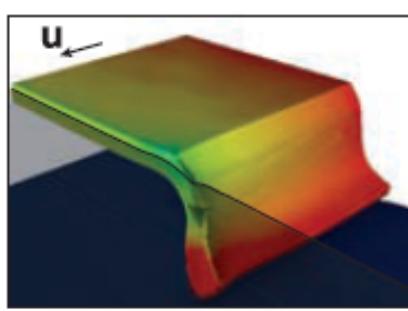
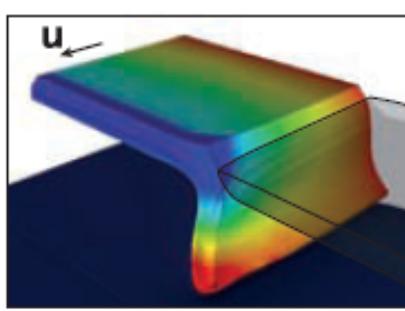
SO



SL



SOL



# From regional to global

